REMARKS

Applicants wish to express their appreciation for the Examiner's indication that claims 12-16 are allowed over the art of record and claims 7-11 would be allowable if rewritten to overcome the rejection under 35 U.S.C. 112, second paragraph.

Summary of the Office Action

In the Office Action, the title of the invention was objected to for being non-descriptive.

Claims 1-11 stand rejected under 35 U.S.C. § 112, second paragraph.

Claims 1-4 stand rejected under 35 U.S.C. § 103 (a) as being unpatentable over European Patent No. 09 595 42 to *Sugimoto, et al* in view of U.S. Patent No. 6,114,054 to *Klein, et al.*

Summary of the Response to the Office Action

By this Amendment, Applicant amends the title of the invention and claim 1. Accordingly, claims 1-16 are pending for further consideration.

All Claims are Allowable

Claims 1-11 were rejected under 35 U.S.C. § 112, second paragraph, as being indefinite for failing to particularly point out and distinctly claim the subject matter which Applicant regards as the invention. The Examiner is thanked for the helpful comments regarding the indefiniteness rejection of independent claim 1. This rejection is respectfully traversed.

Specifically, claim 1 includes reference to the 1993 Japanese Industrial Standard, JIS: Z8721, *Colour specification – Specification according to their three attributes*, hereinafter known as "1993 JIS: Z8721." The 1993 JIS: Z8721 document (an English-language version of Japanese Industrial Standard, 1993 JIS: Z8721 is attached for the Examiner's convenience and for entry into the record) is identified as a document for measuring hue, lightness value, and chroma. Because the claims include this specific 1993 standard, the metes and bounds of the

claim are known and will not vary over time. Accordingly, it is respectfully submitted that the claims are definite, and withdrawal of the rejections under 35 U.S.C. § 112, second is respectfully requested.

All Subject Matter Complies With 35 U.S.C. § 103(a)

Claims 1-4 were rejected under 35 U.S.C. § 103(a) as being unpatentable over European Patent No. 09 595 42 to *Sugimoto, et al* in view of U.S. Patent No. 6,114,054 to *Klein, et al.* This rejection is respectfully traversed. Applicant respectfully submits that neither *Sugimoto* nor *Klein* teach or suggest at least a brightness and chroma quality for a marking layer as recited in claim 1.

Sugimoto discloses a spark plug glaze layer formed on an alumina-based insulator constructed of materials with very little or no lead (Pb) constituents that demonstrate good resistance to cracking. The glaze can be fired at temperatures as low as 800-950°C, and has excellent flashover resistance. See the abstract of *Sugimoto.*

Klein discloses a method for coloring ceramic surfaces that includes the steps of providing a host lattice material composed of a colorless oxide compound that crystallizes into one of a spinel lattice or a rutile lattice and that may be water-soluble; providing an aqueous coloring solution, a first water-soluble compound including a metal ion that is one of a two-valent metal ion or a three-valent metal ion and that colors the host lattice material, and a second water-soluble compound including a metal ion that is one of a five-valent metal ion or six-valent metal ion and that provides a electrostatic balance; and generating a mixed-phase pigment in the surface of the ceramic mass. See the abstract of *Klein.*

To establish a *prima facie* case of obviousness, three basic criteria must be met (see MPEP §§ 2142-2143). First, there must be some suggestion or motivation, either in the references themselves or in the knowledge generally available to one of ordinary skill the art, to combine reference teachings. Second, there must be a reasonable expectation of success. Third, the prior art references must teach or suggest all the claim limitations.

In the present case, neither *Sugimoto* nor *Klein,* either alone or in combination teach or suggest at least the features of a "glaze layer [which] comprises 5 mol% or less of a Pb . . . the tint of the marking layer seen through the glaze layer is 3 or less in brightness as specified by 1993 JIS: Z8721 as well as 3 or less in chroma" as recited in claim 1. Thus, the Office Action fails to establish a *prima facie* case of obviousness because it does not teach all the recited claim features. Therefore, Applicant respectfully requests that the rejection of claims 1-4 under 35 U.S.C. § 103(a) be withdrawn.

The Office Action states that the "tint of the marking layer seen through the glaze layer...is...inherent provided the marking layer and the glaze layers comprise the same components in the same predetermined mass %." On the contrary, "[t]o establish inherency, the extrinsic evidence `must make clear that the missing descriptive matter is necessarily present in the thing described in the reference, and that it would be so recognized by persons of ordinary skill. Inherency, however, may not be established by probabilities or possibilities. The mere fact that a certain thing may result from a given set of circumstances is not sufficient.' " In re Robertson, 169 F.3d 743, 745, 49 USPQ2d 1949, 1950-51 (Fed. Cir. 1999) (citations omitted).

The Office Action does not establish that the brightness and chroma of a marking layer is greatly affected by its composition and that of the glaze layer. Accordingly, for at least this reason, the inherency argument is not supported or sustainable in the Office Action. In addition,

there is no suggestion in the art or extrinsic evidence of record that would indicate that the above recited features of claim 1 are necessarily present in either *Sugimoto* or *Klein et al.* Accordingly, the above recited features of Applicants' claim 1 cannot be considered inherently disclosed by *Sugimoto* or *Klein et al.*

CONCLUSION

In view of the foregoing, Applicant respectfully requests reconsideration and the timely allowance of the pending claims. Should the Examiner feel that there are any issues outstanding after consideration of the response, the Examiner is invited to contact the Applicant's undersigned representative to expedite prosecution.

If there are any other fees due in connection with the filing of this response, please charge the fees to our Deposit Account No. 50-0310. If a fee is required for an extension of time under 37 C.F.R. §1.136 not accounted for above, such an extension is requested and the fee should also be charged to our Deposit Account.

Attached hereto is a marked-up version of the changes made to the specification and/or claims by the current amendment. The attached page is captioned **"Version with markings to show changes made."**

Respectfully submitted,

MORGAN, LEWIS & BOCKIUS LLP

By: _____
David J. Kenealy
Reg. No. 40,411

Date: March 31, 2003
Customer No. 009629
MORGAN, LEWIS & BOCKIUS LLP
1111 Pennsylvania Avenue, NW
Washington, D.C. 20004
Tel.: (202) 739-3000

Version With Markings to Show Changes Made

IN THE TITLE:

The title has been amended to read as follows:

-- SPARK PLUG **WITH GLAZE AND MARKING** --

IN THE CLAIMS:

Claim 1 has been amended as follows:

1. (Amended) A spark plug comprising:

an insulator;

a marking layer formed on a surface of the insulator; and

a glaze layer covering the marking layer so that the marking layer can be seen through the glaze layer,

wherein the glaze layer comprises 5 mol% or less of a Pb component in terms of PbO, and the tint of the marking layer seen through the glaze layer is 3 or less in ~~[the]~~ brightness **as** specified by **1993** JIS: Z8721 as well as 3 or less in ~~[the]~~ chroma **as** specified by **1993** JIS: Z8721, or 4 or less in ~~[the]~~ brightness **as** specified by **1993** JIS: Z8721 as well as 2 or less in ~~[the]~~ chroma **as** specified by **1993** JIS: Z8721.

6. Fee Payment

☐ No fee is to be paid at this time.

☒ Please charge Deposit Amount No. 50-0310 the total amount of $ 930.00 for the three month extension fee due.. The Commissioner is hereby authorized to charge any additional extension of time fee or additional fee for claims due to Deposit Account No. 50-0310.

☒ The Commissioner is hereby authorized to charge any additional fees which may be required, including fees due under 37 C.F.R. §§ 1.16 and 1.17, or credit any overpayment to Deposit Account 50-0310.

Respectfully Submitted,

MORGAN, LEWIS & BOCKIUS LLP

Dated: March 31, 2003 By: _____
David J. Kenealy
Reg. No. 40,411

Customer No.: 009629
MORGAN, LEWIS & BOCKIUS LLP
1111 Pennsylvania Avenue, N.W.
Washington, D.C. 20004
Telephone: (202) 739-3000
Facsimile: (202) 739-3001

UDC 535.641

JIS

JAPANESE INDUSTRIAL STANDARD

Colour specification — Specification according to their three attributes

JIS Z 8721—1993

Translated and Published

by

Japanese Standards Association

Printed in Japan

39 S

In the event of any doubt arising,
the original Standard in Japanese is to be final authority.

JAPANESE INDUSTRIAL STANDARD

JIS Z 8721 :1993

Colour specification—Specification according to their three attributes

February, 1998

ERRATA

Page 17

Attached Table 2 (continued)

In column 3 (right-hand column y of 5.0 GY) in the 14th line from the bottom, replace "0.335 9" with "0.355 9".

Remarks: This errata is for correcting the first edition of this Standard.

Japanese Standards Association

UDC 535.641

JAPANESE INDUSTRIAL STANDARD J I S

Colour specification - Specification according to their three attributes

Z 8721-1993

1. Scope This Japanese Industrial Standard specifies the system to specify surface colours (hereafter referred to as "colours"), by indicating their three attributes, i.e. hue, lightness, and chroma of colour perception with notations on scales.

Remarks: The following standards are cited in this Standard:

JIS Z 8105 Glossary of colour terms

JIS Z 8701 Specification of colours according to the CIE 1931 standard colorimetric system and the CIE 1964 supplementary standard colorimetric system

JIS Z 8716 Fluorescent lamp as a simulator of CIE standard illuminant D_{65} for a visual comparison of surface colours - Type and characteristics

JIS Z 8719 Evaluation method of degree of metamerism for change in illuminants

JIS Z 8720 Standard illuminants and sources for colorimetry

JIS Z 8722 Methods of colour measurement - Reflecting or transmitting objects

JIS Z 8723 Methods of visual comparison for surface colours

JIS Z 8741 Method of measurement for specular glossiness

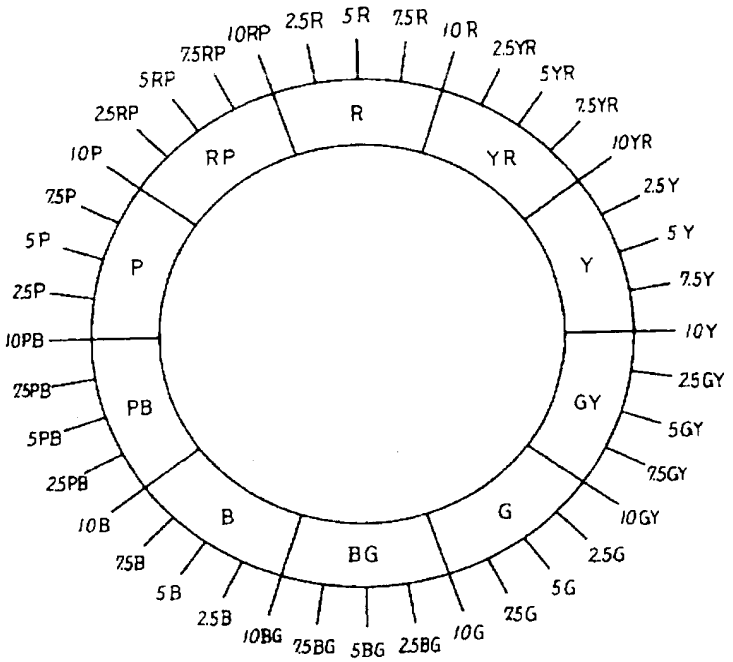
2. Definitions For the purposes of this Standard, the definitions given in JIS Z 8105 and the following definition apply.

Constant hue plane A plane where the colours of constant hue are arranged so as to position in the order of their lightness and chroma.

3. Notation to specify three attributes

3.1 Notation to specify hue Of the attributes of colour perception, the hue H, scaled perceived hue, as shown in hue circle of Fig. 1 on which lightness and chroma are fixed, shall be notated with symbols shown in the inner circle of Fig. 1 and numerals prefixed to them. The hue circle has been graduated in approximately equal steps of hue perception.

Fig. 1. Graduation of hue circle

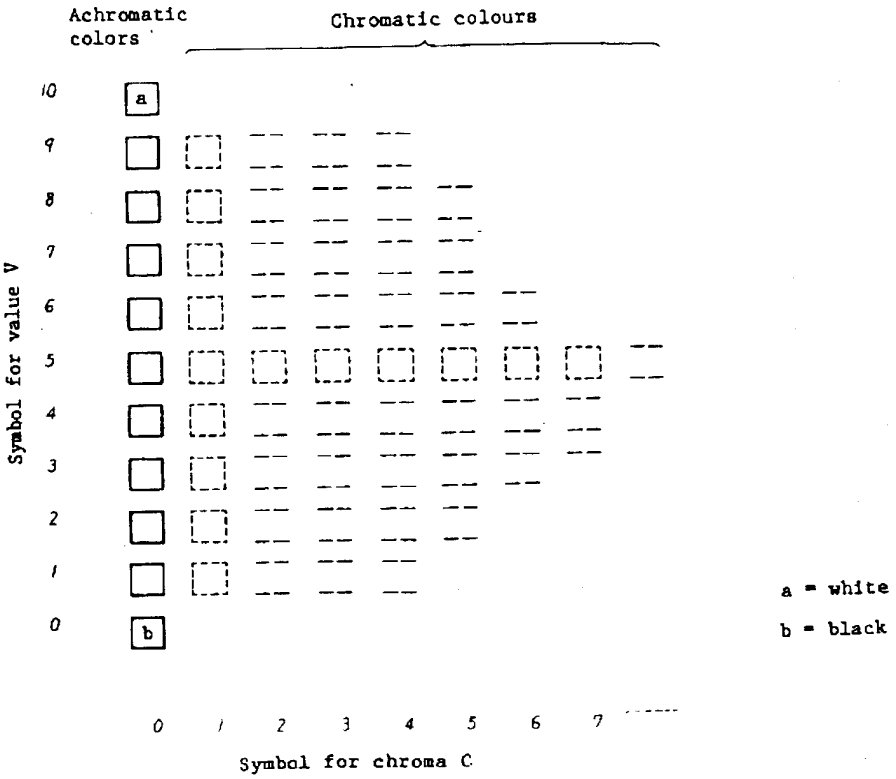


3.2 Notation to specify lightness Of the attributes of colour perception, the value V, scaled perceived lightness, shall be specified by a notation consisting of a numeral shown in Fig. 2. The numerals have been so obtained as shown in Fig. 2, that the entire lightness perception range from ideal black as 0 to ideal white as 10 may be divided on the basis of the achromatic colour into approximately equal steps of lightness perception.

To specify the value of a chromatic colour, the value of an achromatic colour of which luminance factor Y_c is equivalent to that of the chromatic colour shall be taken.

3.3 Notation to specify chroma Of the attributes of colour perception, the chroma C, scaled perceived chroma, shall be specified by a numeral shown in Fig. 2. The numerals have been so obtained, as shown in Fig. 2, that the colours of a fixed hue and, at the same time, of a fixed value may be arranged to equal step of chroma perception in the sequence of 1, 2, 3, ... of increasing order of chroma, which shall be started at 0 of the achromatic colour.

Fig. 2. Arrangement of values and chromas on a constant-hue plane



4. Notation to specify colours according to three attributes

4.1 Notation to specify colours The notation to specify colors shall be expressed, as shown below, by hue H, value V and chroma C for the chromatic colours and by value V for the achromatic colours in accordance with the methods shown in 3.1 to 3.3:

(1) Specification of chromatic colours A chromatic colour shall be specified as in Example 1. and Example 2. in accordance with the form of HV/C.

Example 1. 5R4/10 (read 5R, 4, and 10)

Example 2. 7.5P 2.5/2.5 (read 7.5P, 2.5 and 2.5).

(2) Specification of achromatic colour An achromatic colour shall be specified by giving the symbol N for achromatic before the value V and in the form of NV as shown in Example 3.

When an achromatic colour sensed slightly to be colored is required to be specified including hue and chroma, it shall be done so as written in Example 4 by bracketing with ( ) the main hue H and chroma C shown by the symbols in the inner circle of Fig. 1 and in the form of $NV/(HC)$.

Example 3. N8

Example 4. N5.5/(R0.3)

4.2 Numerals to be prefixed to notation to specify colours When determining the numerals to be prefixed to the notation to specify respective hue H, value V and chroma C, they shall be integer or down to decimal one place.

5. Basis of the colour system according to three attributes The basis of the colour system according to its three attributes shall be luminance factor Y_C shown in Attached Tables 1 and 2 and the values of chromaticity coordinates x_C and y_C ([1]).

The relations between the hue and chroma of equal lightness and the values of chromaticity coordinates x_C, y_C are shown in Attached Figs. 1 to 9.

Note ([1]) The values are based on the CIE 1931 standard colorimetric system under the standard illuminant C.

Remarks: The basic values of the CIE 1931 standard colorimetric system under the standard illuminant D_{65} are given in Annex.

6. Determination of notation to specify colours The notations to specify colours shall be determined by the method (1) or (2) below. For the accurate specifying, the method (1) shall be applied.

(1) Determination of notation using values Y_C, x_C, y_C The determination derived from the values, Y_C, x_C and y_C shall be made by interpolation or extrapolation([3]) from the values of chromaticity coordinates x_C, y_C and Y_C of tristimulus values obtained according to JIS Z 8722([2]) using Attached Tables 1 and 2.

The measurement shall be performed using values measured under the conditions that regular reflection components shall not be involved.

Notes ([2]) Tables of weighting functions in JIS Z 8719 may be used.

([3]) Example of calculation by interpolation is shown in Informative reference 1.

(2) Determination of notation by direct comparison with standard colour atlas The determination by direct comparison with standard colour atlas shall be made by visual comparison with standard colours atlas specified in 7.

The visual comparison shall be made by the method described in JIS Z 8723.

The light sources to be used for illumination shall be as follows:

(a) Standard source C specified in 4.2.2 of JIS Z 8720.

(b) Simulator source D_{65} specified in 4.1 of JIS Z 8723.

(c) Lamp specified in JIS Z 8716.

Remarks: The numerals of notation to specify colours determined by the visual comparison with the standard colour chips are expressed by the numerals corresponding to integer multiple of 0.5 step for hue H, that of 0.2 V step for value and that of 0.5 C step for chroma.

7. Standard colour atlas

7.1 Standard colour atlas The standard colour atlas shall consist of the colour chips according to the basis of the colour system specified in 5.

7.2 Types of standard colour atlas The types of standard colour atlas shall be as described below according to presence or absence of surface gloss in its colour chips.

(1) Standard colour atlas, mutte edition Relative specular glossiness(4) of the colour chips shall be 5 % or less.

(2) Standard colour atlas, grossary edition Relative specular glossiness (4) of the colour chips shall be 60 % or more.

Note (4) It shall be in accordance with the method 3 in JIS Z 8741.

7.3 Tolerance on colour of standard colour chips The tolerance on colour of standard colour chips shall be as shown in Table 1.

Table 1. Tolerance on colour of standard colour chips

Colour	Attribute	Tolerance
Achromatic colour	Value	For colour chips exceeding $V = 3.5$, value ΔY corresponding to $\Delta V = \pm 0.1$. For colour chips of which Value is not more than $V = 3.5$, value ΔY corresponding to $\Delta V = \pm 0.2$.
	Chroma	Values Δx and Δy corresponding to $\Delta C = 0.2$.
Chromatic colour	Hue	For colour at $C = 6$ or more, values Δx and Δy corresponding to $\Delta H = \pm 1$. For colour chips of which Chroma is less than $C = 6$, values Δx and Δy corresponding to $\Delta H = \pm 4/C$.
	Value	For colour chips exceeding $V = 3.5$, value ΔY corresponding to $\Delta V = \pm 0.1$. For colour chips of which Value is not more than $V = 3.5$, value ΔY corresponding to $\Delta V = \pm 0.2$.
	Chroma	Values Δx and Δy corresponding to $\Delta C = \pm 0.4$.

Remarks: The tolerances specified in Table 1 apply to standard colour chips whether matte or glossy.

7.4 Construction of standard colour atlas The standard colour atlas shall consist of the standard colour charts and the accessories for colour comparison use, as follows:

(1) Masks of three types: for high, medium, and low value use

(2) A colour chart of value scale consisting of 18 colour chips N1 to N9.5 (with 0.5 V steps)

(3) A colour chart of hue circle consisting of 10 hues 5R to 5RP (with 10 H steps)

(4) Colour charts of every constant hue, (colour chart based on value and chroma of constant hue). The hue shall be 40 in number as shown in outercircle of Fig. 1; the value of achromatic colour shall be graduated into 8 steps V = 2, 3, 4, 5, 6, 7, 8, 9; and the chroma shall be stepped as C = 0 (achromatic), 1, 2, 3, 4, 6, 8, 10, 12 ... to the highest chroma possible.

(5) Explanatory book

(6) Other necessary matters

7.5 Inspection The standard colours atlas shall be subjected to the tests in accordance with JIS Z 8722 for colour of the standard colour chips. The results shall meet the requirements of 7.3. In addition, the construction of the book of standard colour atlas shall be inspected, and the results shall comply with the requirements of 7.4.

Attached Table 1. Relation between value V and Y_c of luminance factor

V	Y_c	V	Y_c	V	Y_c	V	Y_c	V	Y_c
0.00	0.000	0.50	0.567	1.00	1.180	1.50	1.971	2.00	3.048
0.01	0.012	0.51	0.579	1.01	1.193	1.51	1.989	2.01	3.073
0.02	0.024	0.52	0.590	1.02	1.207	1.52	2.008	2.02	3.098
0.03	0.036	0.53	0.601	1.03	1.221	1.53	2.026	2.03	3.124
0.04	0.047	0.54	0.613	1.04	1.235	1.54	2.045	2.04	3.149
0.05	0.059	0.55	0.624	1.05	1.249	1.55	2.064	2.05	3.175
0.06	0.071	0.56	0.636	1.06	1.263	1.56	2.083	2.06	3.201
0.07	0.082	0.57	0.647	1.07	1.277	1.57	2.102	2.07	3.227
0.08	0.094	0.58	0.658	1.08	1.291	1.58	2.121	2.08	3.253
0.09	0.106	0.59	0.670	1.09	1.306	1.59	2.141	2.09	3.279
0.10	0.117	0.60	0.682	1.10	1.320	1.60	2.160	2.10	3.306
0.11	0.129	0.61	0.693	1.11	1.334	1.61	2.180	2.11	3.332
0.12	0.140	0.62	0.705	1.12	1.349	1.62	2.199	2.12	3.359
0.13	0.152	0.63	0.716	1.13	1.364	1.63	2.219	2.13	3.386
0.14	0.163	0.64	0.728	1.14	1.378	1.64	2.239	2.14	3.413
0.15	0.174	0.65	0.740	1.15	1.393	1.65	2.259	2.15	3.440
0.16	0.186	0.66	0.751	1.16	1.408	1.66	2.280	2.16	3.468
0.17	0.197	0.67	0.763	1.17	1.423	1.67	2.300	2.17	3.495
0.18	0.208	0.68	0.775	1.18	1.438	1.68	2.320	2.18	3.523
0.19	0.220	0.69	0.787	1.19	1.453	1.69	2.341	2.19	3.551
0.20	0.231	0.70	0.799	1.20	1.468	1.70	2.362	2.20	3.579
0.21	0.242	0.71	0.811	1.21	1.483	1.71	2.383	2.21	3.607
0.22	0.254	0.72	0.823	1.22	1.499	1.72	2.404	2.22	3.636
0.23	0.265	0.73	0.835	1.23	1.514	1.73	2.425	2.23	3.664
0.24	0.276	0.74	0.847	1.24	1.530	1.74	2.446	2.24	3.693
0.25	0.287	0.75	0.859	1.25	1.546	1.75	2.468	2.25	3.722
0.26	0.299	0.76	0.871	1.26	1.561	1.76	2.489	2.26	3.751
0.27	0.310	0.77	0.883	1.27	1.577	1.77	2.511	2.27	3.780
0.28	0.321	0.78	0.896	1.28	1.593	1.78	2.533	2.28	3.809
0.29	0.332	0.79	0.908	1.29	1.609	1.79	2.555	2.29	3.839
0.30	0.343	0.80	0.920	1.30	1.625	1.80	2.577	2.30	3.869
0.31	0.354	0.81	0.933	1.31	1.642	1.81	2.599	2.31	3.899
0.32	0.366	0.82	0.945	1.32	1.658	1.82	2.621	2.32	3.929
0.33	0.377	0.83	0.958	1.33	1.675	1.83	2.644	2.33	3.959
0.34	0.388	0.84	0.970	1.34	1.691	1.84	2.666	2.34	3.989
0.35	0.399	0.85	0.983	1.35	1.708	1.85	2.689	2.35	4.020
0.36	0.410	0.86	0.996	1.36	1.725	1.86	2.712	2.36	4.050
0.37	0.421	0.87	1.008	1.37	1.741	1.87	2.735	2.37	4.081
0.38	0.433	0.88	1.021	1.38	1.758	1.88	2.758	2.38	4.112
0.39	0.444	0.89	1.034	1.39	1.775	1.89	2.782	2.39	4.144
0.40	0.455	0.90	1.047	1.40	1.793	1.90	2.805	2.40	4.175
0.41	0.466	0.91	1.060	1.41	1.810	1.91	2.829	2.41	4.207
0.42	0.477	0.92	1.073	1.42	1.827	1.92	2.852	2.42	4.238
0.43	0.488	0.93	1.086	1.43	1.845	1.93	2.876	2.43	4.270
0.44	0.500	0.94	1.099	1.44	1.863	1.94	2.900	2.44	4.302
0.45	0.511	0.95	1.113	1.45	1.880	1.95	2.925	2.45	4.335
0.46	0.522	0.96	1.126	1.46	1.898	1.96	2.949	2.46	4.367
0.47	0.533	0.97	1.139	1.47	1.916	1.97	2.973	2.47	4.400
0.48	0.545	0.98	1.153	1.48	1.934	1.98	2.998	2.48	4.432
0.49	0.556	0.99	1.166	1.49	1.952	1.99	3.023	2.49	4.465

Attached Table 1. (continued)

V	Y_c	V	Y_c	V	Y_c	V	Y_c	V	Y_c
2.50	4.498	3.00	6.391	3.50	8.778	4.00	11.70	4.50	15.19
2.51	4.532	3.01	6.434	3.51	8.831	4.01	11.76	4.51	15.27
2.52	4.565	3.02	6.476	3.52	8.884	4.02	11.83	4.52	15.34
2.53	4.599	3.03	6.520	3.53	8.938	4.03	11.89	4.53	15.42
2.54	4.633	3.04	6.563	3.54	8.991	4.04	11.96	4.54	15.49
2.55	4.667	3.05	6.606	3.55	9.045	4.05	12.02	4.55	15.57
2.56	4.701	3.06	6.650	3.56	9.099	4.06	12.09	4.56	15.65
2.57	4.735	3.07	6.694	3.57	9.154	4.07	12.15	4.57	15.72
2.58	4.770	3.08	6.738	3.58	9.208	4.08	12.22	4.58	15.80
2.59	4.805	3.09	6.783	3.59	9.263	4.09	12.29	4.59	15.88
2.60	4.840	3.10	6.827	3.60	9.318	4.10	12.35	4.60	15.96
2.61	4.875	3.11	6.872	3.61	9.373	4.11	12.42	4.61	16.04
2.62	4.910	3.12	6.917	3.62	9.429	4.12	12.48	4.62	16.11
2.63	4.946	3.13	6.962	3.63	9.485	4.13	12.55	4.63	16.19
2.64	4.981	3.14	7.007	3.64	9.541	4.14	12.62	4.64	16.27
2.65	5.017	3.15	7.053	3.65	9.597	4.15	12.69	4.65	16.35
2.66	5.053	3.16	7.099	3.66	9.653	4.16	12.75	4.66	16.43
2.67	5.089	3.17	7.145	3.67	9.710	4.17	12.82	4.67	16.51
2.68	5.126	3.18	7.191	3.68	9.766	4.18	12.89	4.68	16.59
2.69	5.162	3.19	7.237	3.69	9.823	4.19	12.96	4.69	16.67
2.70	5.199	3.20	7.284	3.70	9.880	4.20	13.03	4.70	16.75
2.71	5.236	3.21	7.330	3.71	9.938	4.21	13.09	4.71	16.83
2.72	5.273	3.22	7.377	3.72	9.996	4.22	13.16	4.72	16.91
2.73	5.311	3.23	7.425	3.73	10.053	4.23	13.23	4.73	16.99
2.74	5.348	3.24	7.472	3.74	10.112	4.24	13.30	4.74	17.07
2.75	5.386	3.25	7.520	3.75	10.170	4.25	13.37	4.75	17.15
2.76	5.424	3.26	7.567	3.76	10.228	4.26	13.44	4.76	17.24
2.77	5.462	3.27	7.615	3.77	10.287	4.27	13.51	4.77	17.32
2.78	5.500	3.28	7.664	3.78	10.346	4.28	13.58	4.78	17.40
2.79	5.539	3.29	7.712	3.79	10.405	4.29	13.65	4.79	17.48
2.80	5.577	3.30	7.761	3.80	10.465	4.30	13.72	4.80	17.57
2.81	5.616	3.31	7.810	3.81	10.524	4.31	13.79	4.81	17.65
2.82	5.655	3.32	7.859	3.82	10.584	4.32	13.87	4.82	17.73
2.83	5.694	3.33	7.908	3.83	10.644	4.33	13.94	4.83	17.82
2.84	5.734	3.34	7.957	3.84	10.705	4.34	14.01	4.84	17.90
2.85	5.773	3.35	8.007	3.85	10.765	4.35	14.08	4.85	17.98
2.86	5.813	3.36	8.057	3.86	10.826	4.36	14.15	4.86	18.07
2.87	5.853	3.37	8.107	3.87	10.887	4.37	14.23	4.87	18.15
2.88	5.893	3.38	8.157	3.88	10.948	4.38	14.30	4.88	18.24
2.89	5.934	3.39	8.208	3.89	11.010	4.39	14.37	4.89	18.32
2.90	5.974	3.40	8.259	3.90	11.071	4.40	14.44	4.90	18.41
2.91	6.015	3.41	8.310	3.91	11.133	4.41	14.52	4.91	18.49
2.92	6.056	3.42	8.361	3.92	11.195	4.42	14.59	4.92	18.58
2.93	6.097	3.43	8.412	3.93	11.257	4.43	14.67	4.93	18.66
2.94	6.138	3.44	8.464	3.94	11.320	4.44	14.74	4.94	18.75
2.95	6.180	3.45	8.516	3.95	11.383	4.45	14.81	4.95	18.84
2.96	6.222	3.46	8.568	3.96	11.446	4.46	14.89	4.96	18.92
2.97	6.264	3.47	8.620	3.97	11.509	4.47	14.96	4.97	19.01
2.98	6.306	3.48	8.672	3.98	11.573	4.48	15.04	4.98	19.10
2.99	6.348	3.49	8.725	3.99	11.636	4.49	15.11	4.99	19.18

Attached Table 1. (continued)

V	Y_c	V	Y_c	V	Y_c	V	Y_c	V	Y_c
5.00	19.27	5.50	23.97	6.00	29.30	6.50	35.29	7.00	41.98
5.01	19.36	5.51	24.07	6.01	29.41	6.51	35.42	7.01	42.12
5.02	19.45	5.52	24.17	6.02	29.53	6.52	35.55	7.02	42.27
5.03	19.54	5.53	24.27	6.03	29.64	6.53	35.68	7.03	42.41
5.04	19.62	5.54	24.37	6.04	29.75	6.54	35.80	7.04	42.55
5.05	19.71	5.55	24.47	6.05	29.87	6.55	35.93	7.05	42.69
5.06	19.80	5.56	24.57	6.06	29.98	6.56	36.06	7.06	42.83
5.07	19.89	5.57	24.67	6.07	30.10	6.57	36.19	7.07	42.98
5.08	19.98	5.58	24.78	6.08	30.21	6.58	36.32	7.08	43.12
5.09	20.07	5.59	24.88	6.09	30.33	6.59	36.45	7.09	43.26
5.10	20.16	5.60	24.98	6.10	30.44	6.60	36.58	7.10	43.41
5.11	20.25	5.61	25.08	6.11	30.56	6.61	36.71	7.11	43.55
5.12	20.34	5.62	25.19	6.12	30.68	6.62	36.84	7.12	43.70
5.13	20.43	5.63	25.29	6.13	30.79	6.63	36.97	7.13	43.84
5.14	20.52	5.64	25.39	6.14	30.91	6.64	37.10	7.14	43.99
5.15	20.61	5.65	25.50	6.15	31.03	6.65	37.23	7.15	44.13
5.16	20.71	5.66	25.60	6.16	31.14	6.66	37.36	7.16	44.28
5.17	20.80	5.67	25.71	6.17	31.26	6.67	37.49	7.17	44.42
5.18	20.89	5.68	25.81	6.18	31.38	6.68	37.62	7.18	44.57
5.19	20.98	5.69	25.92	6.19	31.50	6.69	37.75	7.19	44.72
5.20	21.07	5.70	26.02	6.20	31.62	6.70	37.89	7.20	44.86
5.21	21.17	5.71	26.13	6.21	31.74	6.71	38.02	7.21	45.01
5.22	21.26	5.72	26.23	6.22	31.85	6.72	38.15	7.22	45.16
5.23	21.35	5.73	26.34	6.23	31.97	6.73	38.28	7.23	45.30
5.24	21.45	5.74	26.45	6.24	32.09	6.74	38.42	7.24	45.45
5.25	21.54	5.75	26.55	6.25	32.21	6.75	38.55	7.25	45.60
5.26	21.63	5.76	26.66	6.26	32.33	6.76	38.68	7.26	45.75
5.27	21.73	5.77	26.77	6.27	32.45	6.77	38.82	7.27	45.90
5.28	21.82	5.78	26.87	6.28	32.57	6.78	38.95	7.28	46.05
5.29	21.92	5.79	26.98	6.29	32.69	6.79	39.09	7.29	46.20
5.30	22.01	5.80	27.09	6.30	32.82	6.80	39.22	7.30	46.35
5.31	22.11	5.81	27.20	6.31	32.94	6.81	39.36	7.31	46.50
5.32	22.20	5.82	27.31	6.32	33.06	6.82	39.49	7.32	46.65
5.33	22.30	5.83	27.41	6.33	33.18	6.83	39.63	7.33	46.80
5.34	22.40	5.84	27.52	6.34	33.30	6.84	39.77	7.34	46.95
5.35	22.49	5.85	27.63	6.35	33.43	6.85	39.90	7.35	47.10
5.36	22.59	5.86	27.74	6.36	33.55	6.86	40.04	7.36	47.25
5.37	22.69	5.87	27.85	6.37	33.67	6.87	40.18	7.37	47.40
5.38	22.78	5.88	27.96	6.38	33.79	6.88	40.31	7.38	47.56
5.39	22.88	5.89	28.07	6.39	33.92	6.89	40.45	7.39	47.71
5.40	22.98	5.90	28.18	6.40	34.04	6.90	40.59	7.40	47.86
5.41	23.08	5.91	28.29	6.41	34.17	6.91	40.73	7.41	48.01
5.42	23.17	5.92	28.40	6.42	34.29	6.92	40.87	7.42	48.17
5.43	23.27	5.93	28.51	6.43	34.41	6.93	41.00	7.43	48.32
5.44	23.37	5.94	28.63	6.44	34.54	6.94	41.14	7.44	48.48
5.45	23.47	5.95	28.74	6.45	34.66	6.95	41.28	7.45	48.63
5.46	23.57	5.96	28.85	6.46	34.79	6.96	41.42	7.46	48.78
5.47	23.67	5.97	28.96	6.47	34.92	6.97	41.56	7.47	48.94
5.48	23.77	5.98	29.07	6.48	35.04	6.98	41.70	7.48	49.10
5.49	23.87	5.99	29.19	6.49	35.17	6.99	41.84	7.49	49.25

Attached Table 1. (continued)

V	Y_c	V	Y_c	V	Y_c	V	Y_c	V	Y_c
7.50	49.41	8.00	57.62	8.50	66.68	9.00	76.69	9.50	87.75
7.51	49.56	8.01	57.79	8.51	66.87	9.01	76.90	9.51	87.99
7.52	49.72	8.02	57.96	8.52	67.07	9.02	77.11	9.52	88.22
7.53	49.88	8.03	58.14	8.53	67.26	9.03	77.33	9.53	88.45
7.54	50.03	8.04	58.31	8.54	67.45	9.04	77.54	9.54	88.69
7.55	50.19	8.05	58.48	8.55	67.64	9.05	77.75	9.55	88.92
7.56	50.35	8.06	58.66	8.56	67.83	9.06	77.96	9.56	89.16
7.57	50.51	8.07	58.83	8.57	68.03	9.07	78.18	9.57	89.39
7.58	50.67	8.08	59.01	8.58	68.22	9.08	78.39	9.58	89.63
7.59	50.82	8.09	59.18	8.59	68.41	9.09	78.60	9.59	89.87
7.60	50.98	8.10	59.36	8.60	68.61	9.10	78.82	9.60	90.10
7.61	51.14	8.11	59.54	8.61	68.80	9.11	79.03	9.61	90.34
7.62	51.30	8.12	59.71	8.62	69.00	9.12	79.25	9.62	90.58
7.63	51.46	8.13	59.89	8.63	69.19	9.13	79.46	9.63	90.82
7.64	51.62	8.14	60.07	8.64	69.39	9.14	79.68	9.64	91.06
7.65	51.78	8.15	60.24	8.65	69.58	9.15	79.90	9.65	91.30
7.66	51.95	8.16	60.42	8.66	69.78	9.16	80.11	9.66	91.54
7.67	52.11	8.17	60.60	8.67	69.98	9.17	80.33	9.67	91.78
7.68	52.27	8.18	60.78	8.68	70.17	9.18	80.55	9.68	92.02
7.69	52.43	8.19	60.96	8.69	70.37	9.19	80.77	9.69	92.26
7.70	52.59	8.20	61.14	8.70	70.57	9.20	80.98	9.70	92.50
7.71	52.76	8.21	61.32	8.71	70.77	9.21	81.20	9.71	92.74
7.72	52.92	8.22	61.50	8.72	70.97	9.22	81.42	9.72	92.99
7.73	53.08	8.23	61.68	8.73	71.16	9.23	81.64	9.73	93.23
7.74	53.25	8.24	61.86	8.74	71.36	9.24	81.86	9.74	93.47
7.75	53.41	8.25	62.04	8.75	71.56	9.25	82.08	9.75	93.72
7.76	53.57	8.26	62.22	8.76	71.76	9.26	82.31	9.76	93.96
7.77	53.74	8.27	62.40	8.77	71.97	9.27	82.53	9.77	94.21
7.78	53.90	8.28	62.58	8.78	72.17	9.28	82.75	9.78	94.45
7.79	54.07	8.29	62.77	8.79	72.37	9.29	82.97	9.79	94.70
7.80	54.23	8.30	62.95	8.80	72.57	9.30	83.19	9.80	94.95
7.81	54.40	8.31	63.13	8.81	72.77	9.31	83.42	9.81	95.20
7.82	54.57	8.32	63.32	8.82	72.97	9.32	83.64	9.82	95.44
7.83	54.73	8.33	63.50	8.83	73.18	9.33	83.87	9.83	95.69
7.84	54.90	8.34	63.68	8.84	73.38	9.34	84.09	9.84	95.94
7.85	55.07	8.35	63.87	8.85	73.59	9.35	84.32	9.85	96.19
7.86	55.24	8.36	64.05	8.86	73.79	9.36	84.54	9.86	96.44
7.87	55.40	8.37	64.24	8.87	73.99	9.37	84.77	9.87	96.69
7.88	55.57	8.38	64.43	8.88	74.20	9.38	85.00	9.88	96.94
7.89	55.74	8.39	64.61	8.89	74.40	9.39	85.22	9.89	97.19
7.90	55.91	8.40	64.80	8.90	74.61	9.40	85.45	9.90	97.45
7.91	56.08	8.41	64.99	8.91	74.82	9.41	85.68	9.91	97.70
7.92	56.25	8.42	65.17	8.92	75.02	9.42	85.91	9.92	97.95
7.93	56.42	8.43	65.36	8.93	75.23	9.43	86.14	9.93	98.21
7.94	56.59	8.44	65.55	8.94	75.44	9.44	86.37	9.94	98.46
7.95	56.76	8.45	65.74	8.95	75.65	9.45	86.60	9.95	98.71
7.96	56.93	8.46	65.93	8.96	75.86	9.46	86.83	9.96	98.97
7.97	57.10	8.47	66.11	8.97	76.06	9.47	87.06	9.97	99.23
7.98	57.27	8.48	66.30	8.98	76.27	9.48	87.29	9.98	99.48
7.99	57.45	8.49	66.49	8.99	76.48	9.49	87.52	9.99	99.74
								10.00	100.00

Remarks: The function between the value V and the Y_c of luminance factor is calculated by the following formula:

In this case it is mode under the condition of perfect diffuse surface, two degree visual field and standard illuminant C.

$$Y_c = 1.191\,3\ V - 0.225\,32\ V^2 + 0.233\,51\ V^3 - 0.020\,483\ V^4 + 0.000\,819\,36\ V^5$$

Attached Table 2. Basis of colour system according to three attributes (chromatic colours)

V/C	Y_C(%)	R							
		2.5 R		5.0 R		7.5 R		10.0 R	
		x	y	x	y	x	y	x	y
9/ 6	76.69	0.366 5	0.318 3	0.373 4	0.325 6	0.381 2	0.334 8	0.388 0	0.343 9
4		0.344 5	0.317 9	0.349 5	0.322 6	0.355 1	0.328 5	0.360 0	0.334 8.
3		0.332 6*	0.317 4*	0.336 1*	0.320 7*	0.340 1*	0.324 5*	0.343 6*	0.328 9*
2		0.321 0	0.316 8	0.324 0	0.318 8	0.326 3	0.321 0	0.328 4	0.323 3
1		0.313 1*	0.316 4*	0.314 8*	0.317 3*	0.315 7*	0.318 1*	0.316 5*	0.318 8*
8/10	57.62	0.412 5	0.316 0	0.424 9	0.327 0	0.438 8	0.341 9	0.449 0	0.358 9
8		0.390 0	0.317 1	0.400 1	0.326 3	0.411 8	0.338 5	0.421 2	0.352 6
6		0.367 1	0.317 5	0.374 3	0.324 8	0.383 0	0.333 5	0.391 0	0.344 2
4		0.346 0	0.317 7	0.351 0	0.322 4	0.356 4	0.327 9	0.362 1	0.334 9
3		0.334 3*	0.317 4*	0.337 7*	0.320 5*	0.341 5*	0.324 4*	0.345 5*	0.329 2*
2		0.323 6	0.316 9	0.325 4	0.318 6	0.327 7	0.321 1	0.330 1	0.323 7
1		0.315 1*	0.316 5*	0.315 7*	0.317 1*	0.316 7*	0.318 3*	0.317 7*	0.319 2*
7/16	41.98	0.488 5	0.303 9	—	—	0.534 1	0.345 2	0.551 9	0.372 9
14		0.466 0	0.308 2	0.484 8	0.323 8	0.505 9	0.345 0	0.523 4	0.370 0
12		0.443 5	0.311 9	0.459 5	0.325 2	0.477 7	0.343 5	0.493 0	0.365 9
10		0.418 3	0.314 4	0.432 0	0.326 0	0.447 0	0.341 3	0.460 0	0.359 6
8		0.396 1	0.316 0	0.406 7	0.325 6	0.419 6	0.338 2	0.430 8	0.353 3
6		0.372 8	0.317 0	0.380 5	0.324 4	0.388 8	0.333 6	0.398 4	0.345 2
4		0.349 9	0.317 1	0.355 2	0.322 2	0.361 1	0.328 2	0.367 1	0.336 0
3		0.338 9*	0.317 1*	0.342 6*	0.320 6*	0.347 0*	0.325 1*	0.351 2*	0.330 6*
2		0.328 4	0.317 0	0.330 6	0.319 0	0.333 5	0.322 0	0.336 0	0.325 3
1		0.318 7*	0.316 8*	0.319 6*	0.317 5*	0.321 0*	0.319 0*	0 322 1*	0.320 4*
6/18	29 30	0.526 2	0.292 8	0.555 2	0.313 8	0.582 9	0.339 6	0.600 9	0.372 0
16		0.504 1	0.298 3	0.529 7	0.317 9	0.556 0	0.342 0	0.574 1	0.371 3
14		0.479 0	0.304 1	0.502 0	0.321 2	0.526 5	0.343 1	0.546 8	0.369 7
12		0.456 8	0.308 2	0.476 0	0.323 4	0.496 1	0.342 8	0.515 0	0.366 7
10		0.432 0	0.311 8	0.448 0	0 325 0	0.465 5	0.341 2	0.481 2	0.361 9
8		0,406 5	0.314 4	0.418 7	0.325 1	0.431 8	0.338 3	0.444 9	0.355 0
6		0.383 2	0.315 8	0.392 1	0.324 4	0.400 0	0.334 0	0.410 3	0.347 3
4		0.356 6	0.316 3	0.362 8	0 322 1	0.369 2	0.329 1	0.376 8	0.338 1
3		0,343 9*	0.316 5*	0.348 2*	0.320 6*	0.353 5*	0.326 1*	0.359 1*	0.332 5*
2		0.331 8	0.316 6	0.334 3	0.319 0	0.338 1	0.322 8	0.341 7	0.326 8
1		0.320 5*	0.316 6*	0.321 4*	0.317 5*	0.323 5*	0.319 5*	0.325 1*	0.321 3*
5/20	19.27	0.578 4	0.271 9	0.614 2	0.297 0	0.638 8	0.321 6	—	—
18		0.554 0	0 280 4	0.591 8	0.303 8	0.616 1	0.327 7	0.629 7	0.364 2
16		0.530 0	0.288 0	0 563 7	0 310 2	0.590 1	0.333 1	0.603 7	0 365 7
14		0.504 7	0.295 0	0.534 1	0.315 8	0.559 0	0.337 0	0.577 1	0.366 4
12		0.482 0	0.300 2	0.507 1	0.319 4	0.528 0	0.338 9	0.548 1	0.366 0
10		0.453 3	0.305 8	0.474 7	0.322 7	0.492 7	0.339 9	0.511 3	0 363 0
8		0.425 2	0.310 1	0.441 3	0.324 0	0.456 3	0.338 7	0.471 3	0 357 5
6		0.396 0	0.313 0	0.407 8	0.323 8	0.418 0	0.334 8	0 429 9	0 349 9
4		0.366 0	0.314 8	0.374 0	0.322 0	0.380 6	0.329 4	0.387 9	0.339 8
3		0.350 7*	0.315 4*	0.356 3*	0.320 7*	0.361 2*	0.326 2*	0.366 8*	0.333 9*
2		0.336 0	0.315 8	0.339 2	0.319 2	0.342 5	0.322 9	0.346 5	0.327 8
1		0.322 3*	0.316 1*	0.323 5*	0 317 7*	0.325 2*	0.319 6*	0 327 4*	0.321 8*
4/20	11.70	—	—	—	—	0.680 6	0.298 8	—	—
18		0.589 8	0 262 2	0.632 9	0 288 1	0 653 8	0 310 0	—	—
16		0.562 0	0.272 4	0.603 9	0.297 8	0.626 0	0.319 2	0 640 9	0.353 3
14		0.536 9	0.281 0	0.573 4	0.305 7	0.595 9	0.326 9	0.615 4	0.356 8
12		0.507 2	0.289 7	0.538 5	0.312 9	0.560 3	0.332 1	0.580 1	0 353 8
10		0.477 4	0.296 9	0.504 3	0.317 6	0.523 5	0.335 1	0 541 8	0.358 0
8		0 447 2	0.303 1	0.469 0	0.320 9	0.485 0	0.335 9	0.499 5	0.355 7
6		0.414 1	0.308 5	0.429 9	0.322 6	0.441 5	0.334 0	0.453 5	0.350 0
4		0.380 6	0.312 5	0.391 6	0.322 3	0.399 0	0.330 0	0.407 8	0.341 2
3		0.363 5*	0.313 9*	0.371 3*	0.321 4*	0.376 5*	0.327 0*	0.383 2*	0.335 6*
2		0.346 1	0.315 0	0.350 8	0.320 0	0.353 8	0.323 6	0.358 2	0.329 4
1		0.328 3*	0.315 8*	0.330 3*	0.318 3*	0.331 5*	0.320 0*	0.333 6*	0.322 9*

Attached Table 2. (continued)

V/C	Y_C(%)	R							
		2.5 R		5.0 R		7.5 R		10.0 R	
		x	y	x	y	x	y	x	y
3/16	6.391	0.611 6	0.245 6	0.652 0	0.266 0	0.681 7	0.287 2	—	—
14		0.582 8	0.257 9	0.620 4	0.278 9	0.649 2	0.301 2	0.670 3	0.324 9
12		0.553 6	0.269 1	0.588 4	0.290 4	0.615 8	0.312 9	0.632 2	0.336 1
10		0.519 1	0.281 1	0.550 0	0.302 4	0.573 0	0.324 0	0.587 1	0.344 0
8		0.482 1	0.291 8	0.506 4	0.311 4	0.525 1	0.329 7	0.539 3	0.347 7
6		0.440 9	0.300 9	0.459 2	0.316 8	0.473 8	0.331 6	0.485 4	0.346 7
4		0.402 1	0.307 6	0.414 8	0.319 0	0.424 0	0.330 2	0.430 8	0.341 2
3		0.381 2*	0.310 5*	0.390 3*	0.319 3*	0.397 1*	0.327 9*	0.402 3*	0.336 9*
2		0.359 1	0.313 0	0.364 5	0.319 0	0.369 0	0.324 8	0.372 8	0.331 4
1		0.335 5*	0.315 0*	0.337 7*	0.318 0*	0.340 0*	0.320 9*	0.342 1*	0.324 6*
2/14	3.048	0.573 4	0.208 3	0.630 2	0.228 7	0.679 1	0.252 0	0.716 5	0.273 4
12		0.543 8	0.225 4	0.593 0	0.246 5	0.639 2	0.270 4	0.673 2	0.293 7
10		0.512 2	0.242 8	0.555 7	0.263 3	0.595 2	0.287 4	0.624 7	0.312 0
8		0.477 6	0.259 3	0.514 3	0.280 0	0.543 3	0.302 7	0.571 3	0.325 9
6		0.439 0	0.276 0	0.464 2	0.293 4	0.487 5	0.312 3	0.509 5	0.333 1
4		0.402 1	0.290 0	0.418 4	0.303 2	0.433 5	0.316 9	0.448 1	0.333 0
3		0.382 7*	0.296 7*	0.394 6*	0.307 4*	0.405 0*	0.317 9*	0.415 2*	0.330 9*
2		0.361 4	0.303 3	0.369 2	0.311 1	0.375 1	0.318 1	0.381 1	0.327 4
1		0.337 5*	0.309 8*	0.341 3*	0.314 1*	0.343 6*	0.317 6*	0.346 0*	0.322 5*
1/10	1.180	0.505 8	0.190 0	0.560 4	0.210 0	0.611 1	0.229 0	0.666 1	0.249 9
8		0.481 2	0.210 3	0.528 2	0.229 7	0.572 2	0.248 7	0.617 8	0.271 3
6		0.451 5	0.232 9	0.488 5	0.251 5	0.523 5	0.269 8	0.558 4	0.292 1
4		0.416 6	0.256 9	0.442 0	0.272 8	0.466 0	0 288 8	0 493 3	0 306 8
3		0.398 7*	0.268 6*	0 418 5*	0.282 7*	0.436 2*	0.296 5*	0 455 4*	0 312 0*
2		0.376 8	0.281 6	0.390 8	0.292 9	0.402 0	0.303 4	0.412 8	0.315 4
1		0.348 2*	0.297 1*	0.355 7*	0.303 9*	0.360 9*	0.309 9*	0.364 7*	0.316 9*

Attached Table 2. (continued)

V/C	Y_c(%)	YR							
		2.5 YR		5.0 YR		7.5 YR		10.0 YR	
		x	y	x	y	x	y	x	y
9/ 8	76.69	—	—	—	—	0.422 0	0.393 0	0.419 9	0.406 9
6		0.392 7	0.355 0	0.394 8	0.365 9	0.395 0	0.376 3	0.394 1	0.387 7
4		0.364 1	0.342 2	0.366 8	0.350 9	0.367 9	0.358 5	0.367 7	0.366 8
3		0.347 6*	0.334 6*	0.350 9*	0.341 8*	0.353 0*	0.348 3*	0.353 6*	0.355 3*
2		0.332 0	0.327 3	0.335 3	0.332 5	0.338 0	0.337 7	0.339 2	0.343 0
1		0.318 9*	0.320 9*	0.321 3*	0.323 8*	0.323 5*	0.326 9*	0.324 6*	0.330 0*
8/20	57.62	—	—	—	—	0.539 1	0.451 8	0.524 5	0.470 9
18		—	—	—	—	0.531 6	0.448 0	0.517 9	0.467 0
16		—	—	—	—	0.519 5	0.442 4	0.507 9	0.461 3
14		—	—	0.508 8	0.414 5	0.502 5	0.433 8	0.494 0	0.453 0
12		0.485 2	0.384 7	0.484 9	0.405 0	0.481 6	0.423 2	0.475 3	0.441 4
10		0.455 2	0.376 1	0.457 6	0.393 8	0.456 8	0.410 0	0.452 7	0.426 8
8		0.427 5	0.366 2	0.431 0	0.382 0	0.430 6	0.395 2	0.428 0	0.410 2
6		0.396 0	0.354 7	0.398 8	0.366 3	0.400 0	0.377 0	0.399 4	0.389 6
4		0.366 7	0.342 9	0.369 0	0.351 0	0.369 9	0.358 6	0.370 1	0.367 4
3		0.349 7*	0.335 2*	0.353 0*	0.342 1*	0.354 7*	0.348 4*	0.355 5*	0.355 7*
2		0.333 4	0.327 6	0.337 3	0.333 0	0.339 5	0.337 9	0.340 7	0.343 4
1		0.319 6*	0.321 0*	0.322 7*	0.324 2*	0.324 6*	0.327 1*	0.325 6*	0.330 3*
7/20	41.98	0.582 4	0.404 6	0.565 7	0.429 8	—	—	—	—
18		0.569 5	0.402 4	0.556 4	0.426 7	0.541 7	0.449 2	0.527 6	0.470 0
16		0.552 2	0.398 9	0.543 7	0.422 8	0.531 9	0.444 9	0.518 8	0.465 0
14		0.529 7	0.393 8	0.525 2	0.416 8	0.517 4	0.438 1	0.507 4	0.458 1
12		0.500 1	0.386 1	0.500 7	0.408 1	0.497 0	0.428 2	0.490 0	0.448 0
10		0.467 1	0.376 8	0.471 1	0.397 2	0.470 4	0.415 1	0.466 7	0.433 5
8		0.437 1	0.367 9	0.440 2	0.384 2	0.441 5	0.399 6	0.439 9	0.416 4
6		0.405 3	0.357 0	0.409 1	0.370 1	0.410 7	0.382 0	0.410 2	0.396 0
4		0.371 5	0.343 9	0.375 0	0.353 0	0.377 2	0.361 3	0.377 8	0.371 9
3		0.355 1*	0.336 9*	0.358 4*	0.344 0*	0.360 5*	0.350 7*	0.361 2*	0.359 0*
2		0.339 2	0.329 8	0.342 1	0.334 9	0.343 7	0.339 7	0.344 3	0.345 4
1		0.324 1*	0.322 9*	0.326 0*	0.325 6*	0.326 9*	0.328 3*	0.327 3*	0.331 2*
6/18	29.30	0.587 9	0.402 1	0.571 5	0.427 0	—	—	—	—
16		0.569 8	0.399 0	0.559 7	0.423 9	0.546 8	0.447 8	—	—
14		0.548 8	0.394 7	0.542 3	0.418 8	0.532 0	0.441 2	0.520 0	0.462 3
12		0.521 5	0.388 7	0.519 9	0.411 9	0.514 5	0.433 1	0.505 0	0.453 6
10		0.489 1	0.380 6	0.492 1	0.402 2	0.490 4	0.422 0	0.484 3	0.441 6
8		0.453 3	0.370 8	0.459 2	0.390 0	0.459 6	0.406 4	0.457 0	0.424 9
6		0.418 0	0.360 0	0.422 9	0.375 0	0.424 2	0.387 6	0.424 0	0.403 0
4		0.380 6	0.346 7	0.384 0	0.356 4	0.386 0	0.365 2	0.386 1	0.376 7
3		0.362 8*	0.339 6*	0.365 6*	0.347 0*	0.367 4*	0.353 9*	0.367 7*	0.362 9*
2		0.345 3	0.332 1	0.347 4	0.337 3	0.348 7	0.342 1	0.349 1	0.348 3
1		0.327 8*	0.324 3*	0.329 0*	0.327 1*	0.329 7*	0.329 7*	0.330 0*	0.332 8*
5/16	19.27	0.593 3	0.398 9	—	—	—	—	—	—
14		0.573 1	0.395 3	0.564 2	0.420 1	0.550 6	0.445 0	—	—
12		0.548 2	0.390 9	0.542 2	0.414 1	0.533 5	0.437 8	0.521 1	0.460 0
10		0.517 5	0.384 4	0.516 1	0.406 4	0.510 8	0.427 6	0.502 5	0.448 9
8		0.479 5	0.375 8	0.483 0	0.396 0	0.482 0	0.414 1	0.477 0	0.433 8
6		0.436 5	0.364 0	0.442 0	0.380 8	0.444 0	0.395 4	0.442 8	0.412 8
4		0.392 5	0.349 4	0.396 8	0.361 4	0.399 1	0.371 4	0.399 5	0.384 0
3		0.371 3*	0.341 7*	0.374 8*	0.350 7*	0.376 5*	0.358 2*	0.377 1*	0.368 1*
2		0.350 6	0.333 7	0.353 0	0.339 5	0.354 0	0.344 5	0.354 6	0.351 4
1		0.330 2*	0.325 2*	0.331 5*	0.328 0*	0.331 8*	0.330 5*	0.332 2*	0.334 1*

Attached Table 2. (continued)

V/C	Y_c(%)	YR							
		2.5 YR		5.0 YR		7.5 YR		10.0 YR	
		x	y	x	y	x	y	x	y
4/12	11.70	0.580 9	0.391 0	0.572 9	0.416 9	—	—	—	—
10		0.547 5	0.385 6	0.543 2	0.409 7	0.535 6	0.434 2	0.525 0	0.457 3
8		0.507 1	0.377 7	0.507 0	0.399 4	0.503 8	0.420 4	0.496 5	0.441 4
6		0.461 2	0.367 4	0.465 1	0.385 9	0.465 5	0.402 9	0.461 8	0.421 3
4		0.414 1	0.353 9	0.418 7	0.367 9	0.420 8	0.380 9	0.418 9	0.394 8
3		0.388 6*	0.345 7*	0.392 4*	0.356 7*	0.394 2*	0.366 4*	0.393 3*	0.377 9*
2		0.362 4	0.336 7	0.365 1	0.344 2	0.366 2	0.350 4	0.366 0	0.359 0
1		0.336 1*	0.326 9*	0.337 4*	0.330 7*	0.337 8*	0.333 5*	0.338 0*	0.338 4*
3/10	6.391	0.594 1	0.381 8	—	—	—	—	—	—
8		0.547 5	0.377 1	0.545 6	0.404 0	0.539 0	0.430 6	0.530 5	0.455 9
6		0.495 4	0.369 2	0.496 6	0.390 8	0.493 0	0.411 6	0.487 2	0.432 6
4		0.436 0	0.356 3	0.437 6	0.371 5	0.437 8	0.386 5	0.434 1	0.401 8
3		0.406 2*	0.348 3*	0.407 9*	0.360 3*	0.408 2*	0.371 5*	0.405 1*	0.383 4*
2		0.375 7	0.339 1	0.377 1	0.347 6	0.377 1	0.354 9	0.374 7	0.363 0
1		0.343 8*	0.328 5*	0.344 7*	0.333 0*	0.344 4*	0.336 5*	0.343 0*	0.340 6*
2/ 8	3.048	0.599 5	0.359 0	—	—	—	—	—	—
6		0.528 0	0.358 1	0.542 6	0.392 5	0.547 5	0.427 1	—	—
4		0.459 8	0.350 8	0.467 4	0.373 8	0.469 0	0.396 4	0.467 6	0.416 8
3		0.422 9*	0.344 5*	0.427 9*	0.361 5*	0.429 0*	0.378 5*	0.427 0*	0.393 4*
2		0.385 2	0.336 5	0.388 0	0.347 6	0.388 9	0.359 0	0.387 2	0.368 8
1		0.347 3*	0.327 1*	0.348 5*	0.332 4*	0.349 2*	0.338 2*	0.348 2*	0.343 1*
1/ 8	1.180	0.672 1	0.305 8	—	—	—	—	—	—
6		0.604 8	0.327 0	—	—	—	—	—	—
4		0.531 1	0.337 1	0.566 0	0.379 5	—	—	—	—
3		0.481 1*	0.337 5*	0.501 8*	0.371 3*	—	—	—	—
2		0.425 8	0.334 4	0.437 7	0.358 0	0.443 0	0.377 5	0.444 6	0.398 2
1		0.367 9*	0.327 4*	0.369 6*	0.338 0*	0.366 5*	0.344 0*	0.362 5*	0.349 0*

Attached Table 2. (continued)

V/C	Y_c(%)	Y							
		2.5 Y		5.0 Y		7.5 Y		10.0 Y	
		x	y	x	y	x	y	x	y
9/20	76.69	—	—	0.483 0	0.509 2	—	—	—	—
18		—	—	0.478 2	0.504 9	0.466 3	0.518 8	0.454 0	0.532 0
16		—	—	0.471 1	0.497 7	0.459 5	0.510 4	0.447 7	0.522 5
14		—	—	0.460 2	0.486 9	0.450 3	0.499 3	0.439 3	0.510 1
12		0.456 9	0.452 7	0.445 5	0.471 9	0.436 9	0.482 9	0.427 1	0.492 0
10		0.437 0	0.436 9	0.427 5	0.452 9	0.420 1	0.462 2	0.412 0	0.469 4
8		0.415 4	0.418 6	0.408 0	0.431 9	0.401 9	0.439 2	0.395 7	0.445 0
6		0.391 0	0.397 2	0.385 8	0.407 1	0.381 1	0.412 3	0.376 1	0.415 5
4		0.365 5	0.373 8	0.362 1	0.379 9	0.359 1	0.383 2	0.355 8	0.385 2
3		0.352 5*	0.361 0*	0.350 2*	0.365 6*	0.348 1*	0.368 4*	0.345 6*	0.369 9*
2		0.339 0	0.347 2	0.337 8	0.350 4	0.336 5	0.352 7	0.334 9	0.353 7
1		0.324 9*	0.332 4*	0.324 5*	0.334 1*	0.324 0*	0.335 5*	0.323 2*	0.336 0*
8/20	57.62	0.509 1	0.490 0	—	—	—	—	—	—
18		0.503 3	0.485 5	0.484 7	0.506 9	0.470 9	0.522 0	0.457 0	0.536 6
16		0.495 7	0.480 0	0.479 1	0.501 2	0.465 3	0.515 8	0.452 5	0.529 5
14		0.484 2	0.471 2	0.469 9	0.492 0	0.457 4	0.506 2	0.445 0	0.518 1
12		0.467 8	0.458 9	0.456 2	0.478 8	0.445 5	0.491 7	0.434 1	0.502 0
10		0.446 9	0.442 3	0.437 6	0.460 1	0.428 3	0.471 2	0.419 0	0.479 1
8		0.423 1	0.423 1	0.415 8	0.437 8	0.408 8	0.446 6	0.400 8	0.452 0
6		0.396 9	0.400 9	0.391 3	0.411 7	0.386 2	0.417 5	0.380 3	0.421 6
4		0.368 4	0.375 1	0.365 0	0.382 6	0.362 2	0.386 1	0.358 1	0.388 3
3		0.354 6*	0.362 1*	0.352 4*	0.367 6*	0.350 3*	0.370 4*	0.347 2*	0.372 1*
2		0.340 6	0.348 4	0.339 4	0.351 8	0.337 9	0.354 0	0.335 9	0.355 2
1		0.325 9*	0.333 3*	0.325 5*	0.334 8*	0.324 6*	0.336 2*	0.323 7*	0.336 9*
7/16	41.98	0.504 9	0.484 3	0.487 5	0.504 7	0.472 8	0.521 5	0.458 2	0.537 5
14		0.495 0	0.477 3	0.479 1	0.496 5	0.465 2	0.512 8	0.451 6	0.527 7
12		0.480 6	0.466 6	0.467 7	0.485 7	0.454 7	0.500 5	0.442 0	0.513 1
10		0.460 6	0.451 6	0.450 9	0.469 6	0.440 0	0.483 0	0.428 9	0.493 7
8		0.435 3	0.431 2	0.427 1	0.446 2	0.418 4	0.456 8	0.409 0	0.464 1
6		0.407 3	0.407 3	0.400 9	0.419 8	0.394 3	0.426 4	0.386 4	0.430 5
4		0.376 1	0.380 0	0.371 8	0.388 5	0.367 7	0.392 5	0.362 4	0.395 1
3		0.360 0*	0.365 8*	0.357 0*	0.371 7*	0.353 8*	0.374 5*	0.349 8*	0.376 3*
2		0.343 6	0.350 7	0.341 9	0.354 0	0.339 6	0.355 8	0.336 9	0.356 9
1		0.327 0*	0.334 3*	0.326 3*	0.335 6*	0.325 0*	0.336 4*	0.323 7*	0.336 9*
6/14	29.30	0.506 1	0.482 9	0.490 5	0 503 8	0.475 4	0.522 0	0.459 3	0.539 2
12		0.492 8	0.473 0	0.478 0	0 492 0	0.463 8	0.508 7	0.448 8	0.523 7
10		0.476 0	0.460 7	0.463 9	0 479 0	0.451 2	0.494 3	0.437 2	0.506 8
8		0.451 7	0.442 1	0.442 6	0 458 8	0.432 1	0.471 9	0 420 1	0.481 2
6		0.420 3	0.417 6	0.414 0	0 430 5	0.406 0	0.440 0	0.396 0	0.445 2
4		0.384 0	0.386 7	0.379 4	0.395 5	0.374 5	0.400 4	0.367 9	0.403 3
3		0.366 1*	0 370 8*	0.362 6*	0 377 2*	0.358 9*	0.380 5*	0.354 0*	0.382 4*
2		0.348 0	0.354 0	0 345 7	0 358 0	0.343 1	0.360 1	0.339 8	0.361 1
1		0.329 4*	0.336 0*	0.328 3*	0 337 8*	0.326 9*	0.338 8*	0.325 2*	0.339 2*
5/12	19.27	0.508 2	0 481 2	0.493 2	0 501 9	0.476 7	0.520 8	0.459 0	0.539 0
10		0.490 5	0.468 3	0.477 7	0.487 6	0.463 2	0.505 7	0.446 8	0.520 9
8		0 468 5	0.452 4	0.457 9	0.469 2	0.445 0	0.485 0	0.430 7	0.496 7
6		0.438 0	0 429 2	0 430 2	0.443 5	0.419 9	0.455 1	0.407 2	0.468 3
4		0.396 8	0.395 4	0.391 5	0.405 7	0.385 0	0.412 0	0.376 2	0.415 8
3		0 375 2*	0 376 6*	0 370 8*	0 384 3*	0 366 1*	0 388 3*	0 359 3*	0 390 4*
2		0.353 4	0.357 0	0.350 0	0.362 0	0 347 0	0.364 0	0.342 2	0.364 8
1		0.331 6*	0.336 8*	0.329 6*	0.339 2*	0.328 2*	0.339 8*	0.325 6*	0.339 8*

Attached Table 2. (continued)

V/C	Y_c(%)	Y							
		2.5 Y		5.0 Y		7.5 Y		10.0 Y	
		x	y	x	y	x	y	x	y
4/10	11.70	0.512 0	0.480 0	—	—	—	—	—	—
8		0.486 5	0.462 5	0.474 5	0.481 0	0.459 5	0.499 0	0.443 0	0.515 3
6		0.454 2	0.439 1	0.445 1	0.455 0	0.433 1	0.468 8	0.419 0	0.479 5
4		0.413 8	0.407 6	0.406 9	0.418 8	0.398 2	0.427 2	0.387 1	0.432 1
3		0.389 3*	0.387 6*	0.383 6*	0.395 5*	0.376 8*	0.400 9*	0.367 7*	0.403 2*
2		0.363 3	0.365 4	0.359 0	0.370 1	0.354 2	0.372 7	0.347 6	0.373 2
1		0.336 6*	0.341 5*	0.334 1*	0.343 4*	0.331 6*	0.344 1*	0.328 0*	0.343 7*
3/ 6	6.391	0.478 4	0.453 1	0.467 0	0.471 1	0.452 6	0.488 9	0.434 5	0.502 6
4		0.427 7	0.416 6	0.419 1	0.428 3	0.408 6	0.437 9	0.396 1	0.445 2
3		0.399 6*	0.394 4*	0.392 3*	0.402 5*	0.384 1*	0.408 5*	0.373 9*	0.412 4*
2		0.370 3	0.370 0	0.364 6	0.374 8	0.358 9	0.377 8	0.351 3	0.378 9
1		0.340 3*	0.343 9*	0.336 9*	0.345 8*	0.334 0*	0.346 7*	0.329 6*	0.346 4*
2/ 4	3.048	0.462 7	0.439 2	0.454 3	0.457 3	0.440 1	0.472 3	0.418 8	0.478 9
3		0.421 6*	0.409 0*	0.413 4*	0.419 9*	0.400 8*	0.426 9*	0.385 0*	0.428 7*
2		0.382 5	0.378 5	0.375 7	0.383 9	0.366 0	0.385 8	0.355 6	0.384 8
1		0.345 3*	0.347 6*	0.341 3*	0.349 4*	0.335 8*	0.348 9*	0.330 6*	0.347 4*
1/ 2	1.180	0.436 2	0.417 7	0.423 0	0.426 5	0.404 2	0.428 7	0.380 2	0.421 2
1		0.355 3*	0.353 0*	0.347 9*	0.353 3*	0.340 6*	0.352 4*	0.333 2*	0.350 3*

Attached Table 2. (continued)

V/C	Y_c(%)	GY							
		2.5 GY		5.0 GY		7.5 GY		10.0 GY	
		x	y	x	y	x	y	x	y
9/18	76.69	0.435 4	0.550 8	0.410 8	0.569 9	0.360 2	0.592 0	0.303 2	0.574 8
16		0.428 8	0.538 3	0.405 8	0.554 1	0.358 1	0.565 4	0.307 9	0.544 0
14		0.421 2	0.523 7	0.399 3	0.532 9	0.355 1	0.533 9	0.311 5	0.512 9
12		0.410 8	0.502 8	0.391 1	0.508 2	0.351 8	0.504 2	0.313 9	0.482 9
10		0.397 3	0.476 1	0.381 0	0.479 1	0.347 1	0.473 5	0.315 5	0.455 8
8		0.383 4	0.449 0	0.369 8	0.449 7	0.341 4	0.441 5	0.315 7	0.425 9
6		0.367 0	0.417 8	0.357 2	0.417 9	0.335 1	0.411 1	0.315 3	0.400 8
4		0.349 9	0.386 6	0.343 7	0.386 1	0.327 4	0.379 3	0.314 4	0.371 1
3		0.341 3*	0.370 7*	0.336 4*	0.370 1*	0.323 7*	0.364 8*	0.313 5*	0.358 2*
2		0.332 1	0.353 9	0.328 4	0.353 4	0.319 8	0.350 0	0.312 4	0.345 4
1		0.321 8*	0.335 9*	0.319 7*	0.335 6*	0.315 4*	0.334 1*	0.311 2*	0.331 7*
8/24	57.62	—	—	—	—	—	—	0.278 1	0.684 0
22		—	—	—	—	—	—	0.284 6	0.656 4
20		—	—	0.412 7	0.585 5	0.359 2	0.623 5	0.291 8	0.625 5
18		0.437 1	0.555 7	0.410 4	0.578 5	0.358 5	0.606 3	0.298 7	0.591 9
16		0.432 7	0.547 5	0.406 1	0.564 1	0.356 9	0.579 8	0.304 3	0.557 8
14		0.426 1	0.534 4	0.401 1	0.546 8	0.354 6	0.549 0	0.309 1	0.524 7
12		0.415 4	0.513 3	0.392 4	0.519 9	0.351 1	0.514 4	0.312 4	0.492 6
10		0.402 1	0.486 9	0.381 6	0.487 9	0.346 3	0.479 1	0.314 0	0.460 1
8		0.385 8	0.455 0	0.369 6	0.454 2	0.340 8	0.445 2	0.314 9	0.428 4
6		0.369 0	0.423 0	0.357 3	0.421 4	0.333 9	0.412 9	0.315 0	0.401 4
4		0.350 4	0.388 7	0.343 3	0.387 2	0.326 6	0.380 9	0.314 0	0.372 7
3		0.341 8*	0.372 4*	0.336 1*	0.370 9*	0.323 1*	0.365 7*	0.313 1*	0.359 4*
2		0.332 7	0.355 5	0.328 4	0.354 2	0.319 4	0.350 2	0.312 1	0.345 9
1		0.322 4*	0.337 1*	0.319 8*	0.336 2*	0.315 2*	0.333 9*	0.311 1*	0.331 7*
7/22	41.98	—	—	—	—	—	—	0.272 8	0.689 3
20		—	—	—	—	—	—	0.281 6	0.656 3
18		—	—	—	—	0.355 5	0.624 2	0.290 5	0.618 6
16		0.436 6	0.557 8	0.407 6	0.578 3	0.354 9	0.600 0	0.298 1	0.583 5
14		0.430 9	0.545 9	0.402 7	0.561 5	0.353 2	0.570 0	0.304 7	0.545 8
12		0.421 3	0.527 0	0.394 9	0.536 7	0.350 2	0.532 8	0.309 2	0.509 5
10		0.409 1	0.503 0	0.385 2	0.505 1	0.346 1	0.495 0	0.312 3	0.473 2
8		0.391 9	0.468 4	0.372 2	0.466 9	0.340 6	0.455 8	0.314 0	0.438 7
6		0.372 8	0.431 6	0.358 1	0.429 1	0.334 1	0.419 1	0.314 2	0.405 8
4		0.353 4	0.395 3	0.343 7	0.392 9	0.326 7	0.384 8	0.313 3	0.376 4
3		0.343 3*	0.376 4*	0.336 3*	0.374 6*	0.322 9*	0.368 3*	0.312 5*	0.361 7*
2		0.332 8	0.356 9	0.328 4	0.335 9	0.319 0	0.351 6	0.311 7	0.346 9
1		0.321 8*	0.336 9*	0.319 8*	0.336 5*	0.314 8*	0.334 4*	0.310 9*	0.331 8*
6/20	29.30	—	—	—	—	—	—	0.264 8	0.700 4
18		—	—	—	—	—	—	0.276 3	0.661 6
16		—	—	—	—	0.349 8	0.628 2	0.287 2	0.619 9
14		0.435 4	0.559 4	0.404 2	0.578 8	0.349 8	0.598 5	0.296 2	0.580 2
12		0.426 9	0.541 4	0.398 0	0.556 4	0.348 8	0.559 6	0.303 7	0.535 8
10		0.415 9	0.519 0	0.389 1	0.526 4	0.346 3	0.519 6	0.308 6	0.494 9
8		0.400 6	0.488 5	0.377 2	0.488 0	0.341 8	0.476 8	0.311 6	0.456 3
6		0.379 9	0.447 0	0.362 2	0.443 8	0.335 1	0.432 1	0.312 8	0.417 5
4		0.357 2	0.403 8	0.346 1	0.400 8	0.327 5	0.392 2	0.312 4	0.382 2
3		0.345 8*	0.382 3*	0.337 6*	0.380 0*	0.323 5*	0.373 5*	0.311 8*	0.365 8*
2		0.334 2	0.360 7	0.328 8	0.359 2	0.319 3	0.355 0	0.311 2	0.349 6
1		0.322 3*	0.338 8*	0.319 6*	0.338 1*	0.314 9*	0.336 1*	0.310 6*	0.333 2*

Attached Table 2. (continued)

V/C	Y_c(%)	GY							
		2.5 GY		5.0 GY		7.5 GY		10.0 GY	
		x	y	x	y	x	y	x	y
5/18	19.27	—	—	—	—	—	—	0.254 9	0.717 9
16		—	—	—	—	—	—	0.270 2	0.670 0
14		—	—	—	—	0.342 9	0.633 5	0.283 8	0.620 8
12		0.433 3	0.560 2	0.401 1	0.580 2	0.345 0	0.594 9	0.294 0	0.575 1
10		0.422 4	0.536 9	0.392 8	0.548 5	0.345 1	0.549 0	0.302 8	0.523 7
8		0.408 8	0.506 8	0.381 5	0.509 3	0.341 2	0.497 6	0.308 0	0.475 9
6		0.387 9	0.464 6	0.366 3	0.461 4	0.335 4	0.448 3	0.310 8	0.430 1
4		0.362 1	0.414 3	0.348 2	0.409 7	0.327 4	0.399 4	0.311 1	0.388 1
3		0.348 6*	0.388 8*	0.338 6*	0.385 0*	0.323 1*	0.377 1*	0.311 1*	0.369 0*
2		0.335 2	0.363 6	0.328 9	0.361 2	0.318 8	0.356 0	0.311 0	0.350 8
1		0.322 2*	0.339 3*	0.319 3*	0.338 3*	0.314 4*	0.335 8*	0.310 7*	0.333 3*
4/16	11.70	—	—	—	—	—	—	0.242 2	0.736 0
14		—	—	—	—	—	—	0.259 0	0.685 8
12		—	—	—	—	0.334 8	0.646 8	0.275 8	0.628 2
10		—	—	0.398 3	0.585 0	0.339 5	0.591 3	0.290 8	0.567 2
8		0.417 4	0.530 0	0.386 8	0.538 4	0.340 0	0.5348	0.300 8	0.509 5
6		0.396 8	0.485 7	0.371 8	0.485 2	0.335 5	0.473 9	0.306 9	0.455 0
4		0.370 8	0.432 9	0.353 8	0.428 4	0.328 1	0.415 7	0.310 0	0.401 8
3		0.354 6*	0.401 8*	0.342 7*	0.397 8*	0.323 4*	0.387 2*	0.310 7*	0.377 5*
2		0.338 2	0.370 6	0.331 2	0.367 8	0.318 5	0.360 4	0.310 9	0.355 0
1		0.322 9*	0.341 4*	0.320 1*	0.340 1*	0.313 9*	0.336 4*	0.310 7*	0.334 5*
3/14	6.391	—	—	—	—	—	—	0.228 3	0.742 3
12		—	—	—	—	—	—	0.253 1	0.670 0
10		—	—	—	—	0.326 6	0.644 8	0.272 4	0.602 6
8		—	—	0.392 4	0.583 2	0.334 1	0.570 0	0.288 7	0.536 1
6		0.406 9	0.511 0	0.375 0	0.510 9	0.333 3	0.496 7	0.299 2	0.471 7
4		0.377 2	0.448 4	0.355 4	0.442 9	0.327 0	0.428 8	0.305 3	0.412 3
3		0.359 3*	0.412 5*	0.343 8*	0.407 2*	0.322 6*	0.395 4*	0.307 3*	0.383 9*
2		0.341 2	0.376 8	0.331 9	0.372 9	0.318 0	0.364 4	0.308 8	0.357 8
1		0.324 3*	0.343 9*	0.320 4*	0.342 0*	0.313 7*	0.337 5*	0.309 7*	0.334 9*
2/12	3.048	—	—	—	—	—	—	0.190 7	0.779 8
10		—	—	—	—	—	—	0.230 7	0.681 4
8		—	—	—	—	0.316 0	0.650 9	0.262 8	0.583 7
6		—	—	0.383 9	0.574 8	0.326 0	0.537 9	0.285 2	0.497 2
4		0.388 1	0.475 2	0.358 2	0.465 0	0.324 8	0.445 7	0.298 6	0.424 0
3		0.363 4*	0.423 9*	0.344 2*	0.416 4*	0.321 0*	0.402 6*	0.303 4*	0.389 0*
2		0.342 1	0.380 3	0.330 9	0.374 3	0.316 5	0.365 0	0.306 9	0.358 0
1		0.324 4*	0.344 4*	0.319 2*	0.340 4*	0.312 5*	0.335 4*	0.309 1*	0.333 0*
1/ 6	1.180	—	—	—	—	—	—	0.223 2	0.639 2
4		—	—	0.376 5	0.594 2	0.313 3	0.538 0	0.272 2	0.490 3
3		—	—	0.354 4*	0.481 9*	0.315 3*	0.450 2*	0.288 9*	0.425 3*
2		0.354 0	0.408 8	0.335 9	0.398 2	0.315 4	0.384 0	0.300 6	0.372 0
1		0.327 0*	0.347 0*	0.321 2*	0.343 8*	0.313 7*	0.339 4*	0.308 3*	0.337 0*

Attached Table 2. (continued)

V/C	Y_c(%)	G							
		2.5 G		5.0 G		7.5 G		10.0 G	
		x	y	x	y	x	y	x	y
9/16	76.69	0.263 0	0.496 6	—	—	—	—	—	—
14		0.271 1	0.472 6	—	—	—	—	—	—
12		0.278 6	0.449 1	0.252 8	0.416 0	0.241 9	0.398 5	0.232 5	0.379 6
10		0.285 1	0.427 5	0.263 9	0.400 1	0.254 5	0.385 5	0.245 7	0.370 2
8		0.291 2	0.405 4	0.273 5	0.385 4	0.265 2	0.373 8	0.257 4	0.361 8
6		0.296 6	0.384 6	0.283 2	0.369 7	0.276 3	0.360 7	0.270 3	0.351 3
4		0.301 8	0.360 6	0.293 3	0.351 9	0.288 2	0.346 1	0.284 0	0.340 2
3		0.303 9*	0.350 3*	0.297 6*	0.343 9*	0.293 5*	0.339 3*	0.290 3*	0.334 9*
2		0.305 8	0.340 0	0.301 7	0.335 7	0.298 7	0.332 3	0.296 5	0.329 3
1		0.307 8*	0.328 9*	0.305 8*	0.326 7*	0.304 1*	0.324 8*	0.303 0*	0.323 2*
8/24	57.62	0.209 1	0.603 3	—	—	—	—	—	—
22		0.222 1	0.579 9	0.182 1	0.494 0	—	—	—	—
20		0.233 9	0.556 1	0.195 6	0.480 6	0.184 5	0.449 2	0.173 4	0.416 4
18		0.245 1	0.530 9	0.210 3	0.465 2	0.198 0	0.437 2	0.186 6	0.408 6
16		0.256 3	0.504 5	0.224 0	0.450 0	0.212 0	0.425 2	0.201 2	0.399 2
14		0.266 1	0.478 0	0.236 8	0.434 8	0.225 4	0.412 5	0.214 8	0.390 3
12		0.274 3	0.455 4	0.248 9	0.419 1	0.238 0	0.400 2	0.228 2	0.381 1
10		0.282 9	0.430 1	0.261 3	0.402 6	0.251 5	0.386 7	0.243 0	0.371 0
8		0.289 6	0.406 5	0.272 3	0.386 5	0.263 9	0.373 3	0.256 4	0.361 1
6		0.295 2	0.385 1	0.282 2	0.370 2	0.275 4	0.360 8	0.269 3	0.351 2
4		0.300 9	0.361 4	0.292 4	0.352 3	0.287 4	0.346 4	0.282 8	0.340 3
3		0.303 2*	0.350 9*	0.296 7*	0.344 2*	0.292 7*	0.339 6*	0.289 2*	0.334 9*
2		0.305 3	0.340 4	0.300 9	0.335 9	0.298 1	0.332 6	0.295 7	0.329 3
1		0.307 5*	0.329 1*	0.305 3*	0.326 8*	0.303 8*	0.325 0*	0.302 6*	0.323 2*
7/26	41.98	0.168 9	0.654 9	0.139 7	0.531 2	0.130 3	0.485 8	—	—
24		0.187 5	0.626 5	0.152 1	0.520 0	0.141 5	0.477 8	0.131 0	0.437 7
22		0.202 9	0.601 7	0.165 9	0.507 4	0.153 9	0.468 3	0.143 4	0.430 6
20		0.218 1	0.574 4	0.180 5	0.493 3	0.168 8	0.457 0	0.158 9	0.422 0
18		0.232 8	0.546 7	0.196 7	0.477 1	0.184 1	0.444 8	0.173 4	0.413 5
16		0.244 8	0.520 3	0.211 1	0.461 6	0.198 2	0.433 0	0.188 1	0.404 9
14		0.256 8	0.493 1	0.226 2	0.445 0	0.213 9	0.419 9	0.203 3	0.395 6
12		0.267 2	0.466 7	0.241 6	0.426 7	0.229 5	0.405 8	0.219 5	0.385 4
10		0.277 5	0.439 5	0.255 4	0.408 7	0.244 5	0.391 4	0.235 2	0.374 8
8		0.286 1	0.412 9	0.268 7	0.390 1	0.259 5	0.376 4	0.251 3	0.363 5
6		0.293 3	0.387 3	0.280 1	0.372 1	0.272 8	0.362 2	0.266 2	0.352 6
4		0.299 2	0.364 4	0.290 2	0.354 8	0.285 0	0.348 2	0.280 3	0.341 5
3		0.302 0*	0.353 0*	0.295 2*	0.345 9*	0.291 1*	0.340 9*	0.287 3*	0.335 7*
2		0.304 7	0.341 3	0.300 1	0.336 6	0.297 2	0.333 3	0.294 5	0.329 7
1		0.307 4*	0.329 1*	0.305 1*	0.326 8*	0.303 5*	0.325 1*	0.302 0*	0.323 3*
6/28	29.30	0.114 5	0.712 2	0.090 8	0.569 5	0.085 8	0.512 7	—	—
26		0.134 0	0.687 1	0.107 9	0.556 0	0.101 0	0.501 8	0.094 1	0.452 0
24		0.153 6	0.660 5	0.125 2	0.540 8	0.115 9	0.491 0	0.107 0	0.445 8
22		0.173 9	0.631 8	0.143 2	0.525 2	0.132 5	0.479 5	0.123 0	0.437 8
20		0.192 2	0.603 5	0.160 9	0.509 1	0.148 5	0.467 7	0.138 2	0.429 9
18		0.210 2	0.573 7	0.178 5	0.492 4	0.165 4	0.455 1	0.155 1	0.420 8
16		0.227 8	0.543 0	0.196 0	0.475 1	0.183 2	0.441 4	0.172 2	0.411 3
14		0.242 6	0.513 3	0.213 0	0.457 1	0.200 1	0.427 8	0.189 5	0.401 5
12		0.257 4	0.481 4	0.229 3	0.439 0	0.217 1	0.413 8	0.206 0	0.391 4
10		0.269 0	0.453 0	0.246 6	0.418 1	0.235 0	0.397 9	0.224 7	0.379 6
8		0.279 9	0.423 9	0.261 2	0.399 0	0.251 0	0.382 9	0.242 0	0.367 9
6		0.289 2	0.396 3	0.274 8	0.379 5	0.266 2	0.367 2	0.259 1	0.356 8
4		0.296 7	0.369 5	0.286 8	0.359 5	0.280 7	0.352 2	0.274 9	0.344 3
3		0.300 4*	0.356 6*	0.292 8*	0.349 0*	0.288 3*	0.343 5*	0.283 8*	0.337 5*
2		0.303 9	0.343 7	0.298 8	0.338 2	0.295 8	0.334 4	0.292 9	0.330 3
1		0.307 2*	0.330 4*	0.304 6*	0.327 3*	0.303 1*	0.325 2*	0.301 8*	0.323 1*

Attached Table 2. (continued)

V/C	Y_c(%)	G							
		2.5 G		5.0 G		7.5 G		10.0 G	
		x	y	x	y	x	y	x	y
5/28	19.27	0.079 4	0.738 5	0.060 9	0.589 8	0.058 5	0.522 4	0.057 2	0.459 0
26		0.099 2	0.715 5	0.078 4	0.576 1	0.073 0	0.513 1	0.069 0	0.454 2
24		0.118 8	0.691 8	0.095 3	0.562 8	0.087 8	0.503 9	0.081 1	0.449 1
22		0.137 7	0.667 4	0.114 4	0.546 3	0.105 0	0.492 7	0.095 8	0.442 8
20		0.157 9	0.639 2	0.131 8	0.532 1	0.121 2	0.481 7	0.112 0	0.436 0
18		0.178 2	0.609 5	0.148 9	0.517 1	0.137 2	0.470 5	0.127 5	0.428 8
16		0.200 5	0.575 9	0.169 5	0.498 1	0.157 1	0.456 1	0.146 9	0.419 2
14		0.221 1	0.541 1	0.191 2	0.477 3	0.177 6	0.441 5	0.167 1	0.408 9
12		0.238 5	0.507 1	0.210 4	0.457 8	0.196 4	0.427 1	0.185 2	0.399 2
10		0.256 5	0.470 5	0.232 9	0.433 1	0.220 0	0.408 2	0.209 5	0.385 3
8		0.271 0	0.438 0	0.251 1	0.410 7	0.239 5	0.391 5	0.229 7	0.373 0
6		0.284 1	0.404 5	0.269 0	0.386 0	0.259 8	0.372 4	0.251 9	0.358 7
4		0.294 3	0.373 5	0.284 1	0.362 8	0.277 5	0.354 5	0.271 1	0.345 5
3		0.298 8*	0.358 8*	0.291 1*	0.351 0*	0.286 1*	0.345 1*	0.281 1*	0.338 3*
2		0.303 0	0.344 5	0.297 8	0.339 2	0.294 5	0.335 5	0.291 0	0.331 0
1		0.306 8*	0.330 4*	0.304 1*	0.327 6*	0.302 5*	0.325 9*	0.300 7*	0.323 6*
4/26	11.70	0.052 8	0.750 2	0.040 7	0.601 0	0.039 2	0.525 8	0.040 0	0.454 5
24		0.076 0	0.725 0	0.061 4	0.585 7	0.058 1	0.515 1	0.055 3	0.449 2
22		0.100 9	0.697 5	0.084 1	0.568 4	0.077 0	0.504 0	0.070 2	0.444 0
20		0.123 0	0.670 6	0.101 8	0.554 3	0.092 8	0.494 2	0.085 0	0.438 8
18		0.144 6	0.643 1	0.118 8	0.540 0	0.108 6	0.484 2	0.100 6	0.433 0
16		0.168 2	0.611 1	0.140 2	0.521 4	0.129 3	0.470 3	0.121 2	0.424 5
14		0.190 9	0.577 9	0.162 7	0.501 5	0.150 0	0.456 2	0.139 8	0.416 8
12		0.212 8	0.542 5	0.184 3	0.480 7	0.170 6	0.441 9	0.160 2	0.407 0
10		0.235 5	0.500 6	0.211 5	0.453 2	0.198 9	0.421 9	0.187 6	0.393 3
8		0.256 1	0.459 7	0.235 9	0.426 6	0.223 2	0.402 2	0.212 4	0.379 9
6		0.273 5	0.421 5	0.258 1	0.399 2	0.246 7	0.382 2	0.237 4	0.365 5
4		0.289 1	0.382 1	0.278 1	0.370 4	0.270 2	0.360 2	0.262 8	0.349 8
3		0.295 6*	0.364 0*	0.287 4*	0.355 8*	0.281 4*	0.348 6*	0.275 6*	0.341 3*
2		0.301 2	0.347 0	0.295 9	0.341 7	0.291 9	0.337 1	0.288 0	0.332 7
1		0.306 0*	0.331 1*	0.303 5*	0.328 4*	0.301 5*	0.326 2*	0.299 6*	0.324 3*
3/22	6.391	0.039 0	0.746 8	0.034 0	0.601 1	0.033 2	0.520 6	0.033 3	0.444 4
20		0.072 0	0.712 7	0.062 0	0.580 2	0.056 8	0.508 2	0.052 8	0.439 3
18		0.104 9	0.676 6	0.088 2	0.560 5	0.079 8	0.495 4	0.071 8	0.434 0
16		0.134 1	0.642 0	0.112 0	0.541 4	0.102 3	0.481 8	0.092 5	0.427 5
14		0.162 6	0.605 2	0.138 2	0.519 7	0.126 2	0.466 7	0.116 1	0.419 2
12		0.190 2	0.564 2	0.166 0	0.494 8	0.151 6	0.450 5	0.141 1	0.409 5
10		0.217 0	0.521 1	0.193 5	0.468 2	0.180 0	0.431 0	0.168 8	0.397 4
8		0.243 5	0.475 2	0.222 8	0.438 0	0.208 8	0.410 1	0.197 0	0.384 1
6		0.264 2	0.434 2	0.247 1	0.410 0	0.234 6	0.390 1	0.224 0	0.369 9
4		0.283 6	0.391 5	0.271 1	0.378 0	0.261 8	0.366 7	0.252 5	0.353 7
3		0.292 3*	0.370 2*	0.282 8*	0.360 7*	0.275 8*	0.352 9*	0.268 6*	0.343 8*
2		0.299 9	0.350 0	0.293 5	0.343 9	0.289 0	0.339 1	0.284 4	0.333 7
1		0.305 9*	0.331 8*	0.302 8*	0.328 8*	0.300 7*	0.326 5*	0.298 6*	0.324 3*
2/16	3.048	0.032 9	0.735 8	0.027 7	0.598 6	0.027 6	0.515 3	0.028 5	0.432 7
14		0.082 0	0.686 0	0.068 8	0.569 1	0.062 9	0.497 3	0.059 9	0.427 0
12		0.130 7	0.630 8	0.112 0	0.535 8	0.102 2	0.475 9	0.093 4	0.418 3
10		0.177 3	0.569 8	0.156 0	0.498 1	0.144 2	0.450 5	0.132 1	0.405 9
8		0.219 2	0.504 2	0.197 9	0.458 3	0.184 2	0.424 4	0.170 5	0.391 1
6		0.249 3	0.452 2	0.231 8	0.423 1	0.220 0	0.398 3	0.209 2	0.373 9
4		0.276 3	0.399 8	0.264 0	0.384 5	0.254 0	0.370 5	0.244 2	0.355 9
3		0.288 0*	0.374 1*	0.278 8*	0.364 1*	0.271 1*	0.355 0*	0.263 5*	0.345 0*
2		0.297 8	0.350 7	0.291 8	0.345 0	0.286 9	0.340 0	0.282 0	0.334 1
1		0.305 3*	0.331 0*	0.302 5*	0.328 6*	0.300 3*	0.326 7*	0.298 0*	0.324 2*
1/ 8	1.180	0.062 0	0.689 6	0.055 9	0.571 0	0.053 0	0.494 3	0.051 1	0.415 8
6		0.171 1	0.561 9	0.146 8	0.499 6	0.134 4	0.450 5	0.124 9	0.401 9
4		0.245 4	0.448 9	0.229 0	0.421 8	0.215 9	0.396 7	0.204 0	0.372 4
3		0.271 7*	0.402 0*	0.259 6*	0.386 7*	0.248 8*	0.371 2*	0.238 8*	0.356 2*
2		0.291 0	0.363 4	0.283 3	0.356 4	0.275 8	0.348 4	0.268 9	0.340 7
1		0.303 7*	0.334 4*	0.300 1*	0.332 4*	0.296 4*	0.329 7*	0.293 1*	0.327 0*

Attached Table 2. (continued)

V/C	Y_c(%)	BG							
		2.5 BG		5.0 BG		7.5 BG		10.0 BG	
		x	y	x	y	x	y	x	y
9/10	76.69	0.238 2	0.356 8	0.230 1	0.340 5	0.221 5	0.322 6	—	—
8		0.250 9	0.350 7	0.243 7	0.337 8	0.236 1	0.322 5	—	—
6		0.265 2	0.343 3	0.259 9	0.333 8	0.254 3	0.322 0	0.250 1	0.311 8
4		0.280 5	0.334 9	0.276 8	0.328 7	0.272 8	0.320 8	0.270 0	0.314 0
3		0.287 6*	0.330 9*	0.284 9*	0.326 1*	0.281 9*	0.319 9*	0.280 4*	0.315 1*
2		0.294 7	0.326 7	0.293 0	0.323 2	0.291 1	0.318 8	0.290 7	0.315 9
1		0.302 1*	0.321 9*	0.301 3*	0.320 0*	0.300 5*	0.317 6*	0.300 7*	0.316 4*
8/18	57.62	0.175 9	0.378 2	—	—	—	—	—	—
16		0.191 5	0.373 2	0.181 4	0.345 0	0.172 1	0.316 8	—	—
14		0.205 7	0.368 1	0.195 8	0.343 2	0.186 8	0.317 9	0.178 8	0.293 6
12		0.219 6	0.363 0	0.210 1	0.341 2	0.201 0	0.318 8	0.193 7	0.297 8
10		0.235 2	0.356 6	0.226 4	0.338 3	0.218 4	0.319 6	0.212 0	0.302 5
8		0.250 0	0.350 0	0.241 9	0.335 2	0.235 2	0.319 8	0.230 2	0.306 3
6		0.264 7	0.342 9	0.258 8	0.331 8	0.252 5	0.319 8	0.248 9	0.309 9
4		0.279 1	0.335 1	0.275 2	0.327 8	0.271 8	0.320 0	0.268 6	0.313 0
3		0.286 4*	0.331 1*	0.283 4*	0.325 5*	0.280 9*	0.319 3*	0.278 9*	0.314 2*
2		0.294 0	0.326 8	0.291 9	0.322 8	0.290 0	0.318 3	0.289 4	0.315 2
1		0.301 9*	0.321 9*	0.300 7*	0.319 8*	0.299 6*	0.317 2*	0.299 8*	0.315 9*
7/22	41.98	0.133 4	0.387 0	—	—	—	—	—	—
20		0.149 0	0.382 7	0.138 0	0.341 2	—	—	—	—
18		0.162 6	0.378 8	0.151 5	0.341 0	0.142 7	0.307 6	—	—
16		0.178 8	0.373 9	0.167 5	0.340 1	0.158 4	0.310 1	0.148 9	0.276 8
14		0.193 2	0.369 4	0.183 8	0.339 0	0.175 1	0.312 9	0.167 1	0.283 2
12		0.210 2	0.363 6	0.199 7	0.337 9	0.191 4	0.314 8	0.184 1	0.289 2
10		0.226 4	0.357 6	0.216 3	0.336 1	0.209 4	0.316 5	0.203 5	0.295 6
8		0.243 9	0.350 8	0.235 4	0.333 5	0.229 2	0.317 8	0.223 5	0.301 4
6		0.260 8	0.343 0	0.254 3	0.330 2	0.249 0	0.318 6	0.244 8	0.306 9
4		0.276 4	0.335 4	0.271 2	0.326 9	0.267 1	0.318 9	0.264 2	0.310 9
3		0.284 4*	0.331 3*	0.280 3*	0.324 9*	0.277 2*	0.318 7*	0.275 3*	0.312 7*
2		0.292 7	0.326 9	0.289 8	0.322 5	0.287 8	0.318 2	0.286 9	0.314 3
1		0.301 2*	0.321 9*	0.299 7*	0.319 7*	0.298 8*	0.317 4*	0.298 6*	0.315 5*
6/22	29.30	0.112 0	0.386 0	—	—	—	—	—	—
20		0.126 9	0.382 9	0.116 8	0.334 4	—	—	—	—
18		0.142 8	0.379 0	0.132 5	0.334 5	0.124 8	0.298 1	0.118 1	0.258 1
16		0.160 0	0.374 8	0.149 1	0.334 5	0.140 8	0.301 7	0.133 7	0.265 1
14		0.177 9	0.369 9	0.166 2	0.334 3	0.158 5	0.305 2	0.151 8	0.272 9
12		0.195 4	0.364 5	0.184 4	0.333 7	0.176 2	0.308 1	0.169 8	0.280 2
10		0.214 8	0.358 4	0.203 7	0.332 9	0.196 1	0.311 0	0.190 9	0.288 1
8		0.233 2	0.352 2	0.223 6	0.331 1	0.217 1	0.313 8	0.211 6	0.295 0
6		0.252 6	0.344 8	0.244 1	0.329 0	0.238 4	0.315 5	0.233 5	0.301 5
4		0.270 2	0.336 9	0.264 8	0.326 2	0.260 4	0.316 9	0.257 8	0.307 8
3		0.280 1*	0.332 0*	0.275 9*	0.324 2*	0.272 5*	0.317 2*	0.270 6*	0.310 7*
2		0.290 2	0.326 8	0.287 2	0.321 9	0.284 9	0.317 2	0.283 7	0.313 2
1		0.300 3*	0.321 5*	0.298 7*	0.319 3*	0.297 5*	0.316 9*	0.296 9*	0.315 1*
5/24	19.27	0.073 8	0.385 1	—	—	—	—	—	—
22		0.086 1	0.383 2	0.078 1	0.321 1	—	—	—	—
20		0.100 5	0.381 4	0.090 4	0.323 1	—	—	—	—
18		0.116 5	0.378 5	0.104 6	0.324 4	0.098 2	0.282 8	—	—
16		0.134 8	0.375 0	0.124 3	0.326 1	0.116 7	0.288 0	0.110 8	0.248 9
14		0.155 9	0.370 8	0.144 8	0.327 5	0.136 4	0.293 2	0.130 8	0.258 2
12		0.173 5	0.366 8	0.161 4	0.328 0	0.153 7	0.297 6	0.148 5	0.266 2
10		0.198 0	0.360 6	0.185 0	0.328 0	0.177 6	0.303 2	0.171 6	0.276 0
8		0.220 5	0.353 7	0.210 0	0.328 0	0.203 0	0.308 2	0.197 0	0.286 0
6		0.244 8	0.345 2	0.236 0	0.327 0	0.229 2	0.312 5	0.223 4	0.295 2
4		0.265 9	0.336 9	0.259 1	0.324 6	0.255 0	0.315 0	0.251 2	0.304 0
3		0.276 9*	0.332 1*	0.271 4*	0.322 9*	0.267 9*	0.315 7*	0.265 2*	0.307 8*
2		0.288 0	0.327 0	0.284 1	0.321 0	0.281 2	0.316 1	0.279 6	0.311 1
1		0.299 1*	0.321 7*	0.297 0*	0.318 8*	0.295 2*	0.316 3*	0.294 5*	0.313 9*

Attached Table 2. (continued)

V/C	Y_c(%)	BG							
		2.5 BG		5.0 BG		7.5 BG		10.0 BG	
		x	y	x	y	x	y	x	y
4/24	11.70	0.051 0	0.380 0	—	—	—	—	—	—
22		0.063 6	0.378 8	—	—	—	—	—	—
20		0.076 8	0.377 3	0.067 5	0.307 5	—	—	—	—
18		0.091 5	0.375 4	0.082 8	0.310 8	0.076 8	0.266 7	—	—
16		0.110 2	0.372 0	0.099 2	0.314 1	0.092 2	0.271 8	0.088 8	0.229 8
14		0 128 3	0.368 8	0 117 0	0.317 0	0.109 2	0.277 4	0.103 3	0.237 6
12		0 149 2	0.364 9	0.137 9	0.319 8	0.129 8	0.284 0	0.124 8	0.248 4
10		0.173 8	0.360 0	0.161 8	0.321 9	0.154 0	0.291 0	0.148 0	0 260 0
8		0 200 6	0.354 0	0.189 0	0.323 4	0.181 5	0.298 5	0.176 0	0.273 0
6		0 227 8	0.346 3	0 218 2	0.324 0	0.211 3	0 305 2	0.206 5	0 286 3
4		0.255 2	0.337 5	0.248 0	0.323 2	0.242 9	0.310 8	0.238 4	0 298 4
3		0.269 7*	0.332 4*	0.263 9*	0.322 2*	0.259 5*	0.313 1*	0.255 9*	0 304 1*
2		0 284 0	0.327 0	0.279 9	0.320 8	0.276 4	0.314 8	0.274 0	0 309 1
1		0.297 6*	0.321 6*	0 295 4*	0.318 8*	0.293 3*	0.315 9*	0.292 2*	0.313 3*
3/20	6.391	0 048 2	0.369 5	—	—	—	—	—	—
18		0.064 8	0.368 2	0.058 0	0.294 0	—	—	—	—
16		0.084 3	0.3667	0.073 5	0.297 9	0.069 1	0.255 9	—	—
14		0 105 1	0.364 8	0 094 0	0.302 7	0.087 4	0.262 7	0.079 8	0 215 1
12		0.128 8	0.362 0	0 115 8	0.307 1	0.108 6	0.270 6	0.101 8	0 228 1
10		0.155 2	0.358 0	0 141 0	0.311 8	0.132 6	0.278 4	0.125 0	0.241 1
8		0.184 5	0.353 1	0.170 3	0.315 9	0.162 0	0.287 2	0.155 1	0 257 1
6		0.213 2	0.346 8	0.202 0	0.318 8	0.192 8	0.295 8	0.186 1	0 272 2
4		0.243 7	0.338 6	0 234 3	0.320 0	0.227 2	0.304 1	0.222 1	0 288 6
3		0.261 8*	0.333 0*	0.254 0*	0.319 9*	0.248 2*	0.308 3*	0.243 5*	0.297 1*
2		0.279 9	0.327 1	0 274 2	0.319 2	0.269 9	0.312 0	0.266 0	0 305 0
1		0.296 5*	0.321 4*	0 293 4*	0 318 0*	0.291 0*	0.314 8*	0.288 5*	0 311 6*
2/14	3.048	0.055 5	0.358 8	—	—	—	—	—	—
12		0.085 1	0.357 6	0.076 9	0.288 0	0.072 4	0.247 8	—	—
10		0.119 0	0.355 1	0.105 0	0.295 6	0.099 1	0.258 2	0.092 9	0 213 3
8		0.155 7	0.351 7	0.140 5	0.303 7	0.132 5	0.271 0	0.125 8	0 233 1
6		0.197 1	0.345 2	0.184 3	0.311 0	0.174 7	0.285 3	0.166 9	0 257 0
4		0.234 3	0.337 8	0 223 4	0.315 0	0.216 2	0.298 1	0.209 6	0.279 0
3		0.255 6*	0.332 7*	0.246 5*	0.316 6*	0.240 4*	0.304 3*	0.234 7*	0 290 4*
2		0.276 5	0.327 1	0 269 7	0.317 5	0.265 1	0.309 8	0.260 6	0.301 0
1		0.295 2*	0.321 5*	0.291 5*	0.317 5*	0.288 8*	0.314 0*	0.286 1*	0.309 9*
1/ 8	1.180	0.047 6	0.345 8	—	—	—	—	—	—
6		0.116 9	0.345 2	0.109 3	0.286 0	0.105 9	0.248 5	0.107 4	0.212 9
4		0.188 3	0.340 6	0.175 3	0.302 1	0.170 2	0.276 8	0.165 8	0.249 6
3		0.225 5*	0.335 3*	0.213 0*	0.309 0*	0.206 4*	0.290 4*	0.200 0*	0.269 4*
2		0.260 0	0.328 9	0.250 0	0 314 1	0.243 0	0.302 3	0.236 2	0.288 2
1		0.289 1*	0.322 3*	0.283 3*	0.316 8*	0.278 2*	0.311 3*	0.273 2*	0.304 3*

Attached Table 2. (continued)

V/C	Y_C(%)	B							
		2.5 B		5.0 B		7.5 B		10.0 B	
		x	y	x	y	x	y	x	y
9/ 4	76.69	0.268 0	0.307 3	0.267 5	0.300 5	0.268 8	0.296 1	0.271 2	0.292 4
3		0.279 9*	0.310 1*	0.280 5*	0.305 8*	0.282 3*	0.303 0*	0.284 1*	0.300 8*
2		0.290 9	0.312 5	0.291 9	0.310 2	0.293 7	0.308 7	0.294 9	0.307 6
1		0.301 0*	0.314 6*	0.301 8*	0.313 7*	0.303 0*	0.313 1*	0.303 6*	0.312 8*
8/12	57.62	0.187 7	0.275 2	—	—	—	—	—	—
10		0.206 6	0.283 9	—	—	—	—	—	—
8		0.226 4	0.292 3	0.223 7	0.276 1	0.225 2	0.266 8	0.229 4	0.258 7
6		0.246 2	0.300 0	0.245 7	0.288 8	0.247 2	0.282 1	0.251 2	0.276 0
4		0.266 8	0.306 7	0.267 1	0.299 8	0.268 8	0.295 6	0.271 8	0.291 1
3		0.278 3*	0.309 7*	0.279 1*	0.305 0*	0.280 7*	0.302 0*	0.282 9*	0.299 0*
2		0.289 7	0.312 4	0.290 8	0.309 6	0.292 2	0.307 7	0.293 5	0.306 2
1		0.300 5*	0.314 6*	0.301 4*	0.313 5*	0.302 3*	0.312 6*	0.302 8*	0.312 2*
7/16	41.98	0.143 5	0.247 2	—	—	—	—	—	—
14		0.162 4	0.258 1	0.161 5	0.230 7	—	—	—	—
12		0.179 7	0.267 2	0.177 8	0.243 0	0.181 8	0.230 3	0.188 3	0.220 3
10		0.199 4	0.277 5	0.198 6	0.257 9	0.201 6	0.246 6	0.207 8	0.238 2
8		0.220 8	0.287 1	0.220 4	0.272 9	0.222 5	0 263 1	0.227 7	0.255 9
6		0.241 8	0.296 0	0.241 0	0.285 4	0.243 6	0.278 7	0.247 8	0.272 8
4		0.262 9	0.303 8	0.263 3	0.297 2	0.265 1	0.292 7	0.268 5	0.288 6
3		0.274 7*	0.307 6*	0.275 4*	0.302 7*	0.277 0*	0.299 5*	0.279 7*	0.296 5*
2		0.286 7	0 311 0	0.287 5	0.307 8	0 288 8	0.305 8	0.290 8	0.303 9
1		0.298 6*	0.314 0*	0.299 2*	0.312 4*	0.300 0*	0.311 5*	0.301 1*	0.310 6*
6/16	29.30	0.129 4	0 234 8	0.131 0	0 204 8	0 137 6	0.187 9	0 145 4	0.177 8
14		0.148 0	0.245 9	0.149 6	0.219 3	0.155 6	0.204 3	0.162 9	0 194 7
12		0.166 0	0.256 1	0.168 5	0.233 9	0.173 4	0.220 3	0.180 3	0.211 4
10		0.187 9	0.268 2	0.188 3	0.248 7	0.193 4	0.237 4	0.200 0	0.229 8
8		0.208 0	0.278 9	0.208 8	0.263 5	0.213 2	0.253 7	0.218 9	0.246 8
6		0,231 2	0.289 9	0.232 0	0.278 9	0.235 2	0.270 8	0.239 9	0.265 0
4		0.257 1	0.300 8	0.257 9	0.293 8	0.260 2	0.288 1	0.263 7	0.284 0
3		0.270 3*	0.305 5*	0.271 1*	0.300 4*	0.272 8*	0.296 2*	0.275 5*	0.292 8*
2		0.283 5	0.309 7	0.284 2	0.306 3	0.285 4	0.303 7	0.287 1	0.301 2
1		0.296 8*	0.313 3*	0.297 2*	0.311 6*	0.297 9*	0.310 5*	0.298 7*	0.309 0*
5/18	19.27	—	—	—	—	—	—	0.120 3	0.150 5
16		0.109 0	0.216 6	0.113 2	0.186 3	0.123 0	0.171 1	0.132 6	0.163 2
14		0.128 3	0.229 2	0.132 0	0.202 1	0.140 4	0.187 8	0.149 2	0.179 7
12		0.146 1	0.240 6	0.150 5	0.217 2	0.158 4	0.204 2	0.166 6	0.196 4
10		0.169 7	0.254 9	0.172 9	0.234 7	0.179 2	0.223 0	0.186 0	0.214 9
8		0.194 7	0.268 7	0.195 8	0.251 9	0.200 7	0.241 7	0.206 7	0.234 4
6		0.221 0	0.282 3	0.221 5	0.270 1	0.224 8	0.261 2	0.229 9	0 254 8
4		0.249 2	0.295 4	0 249 3	0.287 9	0.251 1	0.280 8	0.254 7	0.275 7
3		0.264 0*	0.301 5*	0.264 2*	0.295 8*	0.265 5*	0 290 6*	0 268 2*	0 286 2*
2		0.279 1	0.307 1	0.279 4	0.303 2	0 280 3	0.300 0	0.282 1	0.296 6
1		0.294 5*	0.312 1*	0.294 8*	0.310 0*	0.295 3*	0.308 7*	0.296 1*	0.306 7*
4/16	11.70	0.090 0	0.197 3	—	—	—	—	0.115 5	0.141 6
14		0 102 7	0.205 7	0 109 8	0 178 5	0 120 4	0.165 5	0.131 0	0.158 0
12		0.124 7	0.220 9	0.129 9	0.196 3	0.139 3	0.183 7	0.148 7	0.176 0
10		0.146 3	0.235 4	0.151 2	0.214 8	0.160 1	0.202 8	0.168 1	0.195 4
8		0.173 7	0.252 4	0.175 9	0.234 5	0.182 1	0.223 2	0 189 3	0 216 0
6		0.204 8	0.270 8	0.206 0	0.257 2	0.210 2	0.247 0	0.215 7	0.240 7
4		0.236 0	0.287 2	0.236 3	0.278 2	0.238 8	0.270 4	0 242 9	0 264 8
3		0.254 0*	0.295 7*	0.253 8*	0.288 9*	0.255 5*	0.282 7*	0.258 6*	0.277 8*
2		0.272 7	0.303 8	0.272 3	0.299 2	0.273 3	0.294 7	0.275 3	0.291 0
1		0.291 6*	0 310 8*	0.291 2*	0.308 5*	0.291 6*	0.306 1*	0.292 6*	0.304 0*

Attached Table 2. (continued)

V/C	Y_C(%)	B							
		2.5 B		5.0 B		7.5 B		10.0 B	
		x	y	x	y	x	y	x	y
3/14	6.391	—	—	—	—	—	—	0.106 5	0.128 5
12		0.098 9	0.196 3	0.104 2	0.168 1	0.113 1	0.154 2	0.122 8	0.146 0
10		0.122 0	0.213 2	0.125 9	0.187 9	0.134 3	0.175 6	0.143 2	0.167 5
8		0.151 1	0.233 1	0.152 7	0.211 9	0.158 3	0.198 7	0.165 8	0.190 5
6		0.182 6	0.253 6	0.183 5	0.237 5	0.187 5	0.225 8	0.193 3	0.217 3
4		0.218 3	0.274 8	0.217 6	0.263 2	0.220 0	0.253 6	0.224 6	0.246 7
3		0.240 3*	0.286 8*	0.238 8*	0.277 7*	0.239 8*	0.269 5*	0.242 9*	0.263 0*
2		0.263 6	0.298 3	0.261 7	0.292 1	0.261 6	0.285 7	0.263 1	0.280 1
1		0.287 2*	0.308 5*	0.285 7*	0.305 3*	0.285 1*	0.301 6*	0.285 5*	0.297 9*
2/10	3.048	0.091 1	0.182 8	0.096 5	0.155 8	0.105 1	0.142 2	0.115 7	0.134 6
8		0.123 0	0.207 6	0.124 5	0.182 7	0.131 3	0.169 2	0.139 6	0.160 3
6		0.162 1	0.235 8	0.161 7	0.216 2	0.165 8	0.202 6	0.171 6	0.193 7
4		0.206 0	0.264 9	0.204 8	0.251 8	0.206 3	0.240 0	0.210 2	0.231 3
3		0.231 4*	0.279 9*	0.229 7*	0.270 0*	0.229 5*	0.260 0*	0.232 0*	0.251 5*
2		0.257 8	0.294 0	0.255 9	0.287 4	0.254 5	0.279 9	0.255 8	0.272 5
1		0.284 4*	0.306 4*	0.282 9*	0.303 1*	0.281 4*	0.298 9*	0.281 8*	0.294 1*
1/ 8	1.180	—	—	—	—	0.096 8	0.128 0	0.107 7	0.121 8
6		0.111 8	0.190 8	0.121 2	0.174 5	0.130 3	0.163 9	0.139 2	0.156 3
4		0.164 9	0.232 4	0.166 7	0.216 8	0.171 6	0.204 8	0.178 3	0.197 4
3		0.197 0*	0.255 5*	0.195 7*	0.241 9*	0.197 9*	0.230 3*	0.202 1*	0.221 6*
2		0.232 2	0.278 1	0.229 1	0.267 7	0.229 1	0.257 9	0.230 9	0.249 1
1		0.270 1*	0.298 9*	0.267 2*	0.293 0*	0.266 2*	0.286 9*	0.266 4*	0.280 5*

Attached Table 2. (continued)

V/C	Y_c(%)	PB							
		2.5 PB		5.0 PB		7.5 PB		10.0 PB	
		x	y	x	y	x	y	x	y
9/ 4	76.69	—	—	—	—	—	—	0.291 0	0.285 0
3		—	—	—	—	—	—	0.298 2*	0.296 4*
2		0.297 5	0.306 3	0.299 1	0.305 7	0.301 5	0.305 2	0.303 8	0.305 4
1		0.305 0*	0.312 2*	0.305 6*	0.311 9*	0.306 5*	0.311 8*	0.307 8*	0.312 0*
8/ 8	57.62	—	—	—	—	—	—	0.267 7	0.244 3
6		0.256 2	0.270 9	0.261 4	0.267 0	0.270 2	0.264 8	0.279 2	0.264 9
4		0.275 8	0.287 9	0.279 8	0.286 1	0.285 6	0.284 6	0.291 1	0.284 8
3		0.286 1*	0.296 6*	0.289 0*	0.295 4*	0.293 3*	0.294 4*	0.297 2*	0.294 6*
2		0.295 7	0.304 7	0.297 4	0.303 9	0.300 3	0.303 4	0.302 7	0.303 5
1		0.304 0*	0.311 5*	0.304 6*	0.311 0*	0.306 1*	0.310 9*	0.307 2*	0.310 9*
7/12	41.98	—	—	—	—	—	—	0.246 5	0.205 8
10		0.216 2	0.230 9	0.225 4	0.226 7	0.241 0	0.222 4	0.256 3	0.224 0
8		0.235 2	0.249 8	0.242 7	0.245 8	0.254 6	0.241 8	0.267 0	0.242 5
6		0.253 8	0.267 7	0.259 6	0.264 3	0.268 7	0.261 2	0.277 6	0.261 2
4		0.272 9	0.284 8	0.277 3	0.282 8	0.283 3	0.280 9	0.288 6	0.280 1
3		0.283 2*	0.293 9*	0.286 4*	0.292 2*	0.290 9*	0.290 8*	0.294 6*	0.290 2*
2		0.293 2	0.302 5	0.295 2	0.301 1	0.298 2	0.300 3	0.300 5	0.300 0
1		0.302 4*	0.310 2*	0.303 2*	0.309 3*	0.304 7*	0.308 9*	0.305 8*	0.308 9*
6/16	29.30	—	—	—	—	—	—	0.226 5	0.167 1
14		0.175 4	0.186 8	0.187 3	0 182 2	0.211 9	0.179 9	0.235 2	0.183 9
12		0.191 3	0.203 8	0.202 6	0.199 9	0.224 1	0.197 5	0.244 0	0.199 8
10		0 209 5	0.222 5	0.219 7	0.218 8	0.237 8	0.216 8	0.254 0	0.217 6
8		0.227 4	0 240 6	0 236 0	0.236 5	0.250 5	0 234 7	0 263 7	0.235 2
6		0.246 5	0.259 9	0.253 3	0.255 8	0.263 8	0.253 1	0.274 0	0.253 3
4		0.268 4	0.280 4	0.273 4	0.277 8	0.279 8	0.275 2	0.286 3	0.274 7
3		0.279 1*	0.290 0*	0.283 0*	0.288 0*	0.287 7*	0.285 9*	0.292 6*	0.285 5*
2		0.289 7	0.299 1	0.292 3	0.297 8	0.295 5	0.296 3	0.298 8	0.296 1
1		0.300 0*	0.307 9*	0.301 3*	0.307 2*	0.303 0*	0.306 4*	0.304 7*	0.306 4*
5/22	19.27	—	—	—	—	—	—	0.208 2	0.122 5
20		—	—	—	—	0.179 4	0.123 9	0.212 1	0.132 9
18		0.136 3	0.141 0	0.151 8	0.136 5	0.186 2	0.136 5	0.217 4	0.144 4
16		0.149 5	0.155 9	0.163 8	0.152 1	0.194 5	0.151 1	0.222 4	0.155 5
14		0.164 2	0.172 8	0.177 3	0.168 9	0.204 2	0.166 1	0.229 9	0.169 8
12		0.179 3	0.189 4	0.191 8	0.185 8	0.215 7	0.183 0	0.238 4	0.185 7
10		0.196 8	0.207 8	0.208 0	0.204 1	0.228 5	0.202 0	0.247 8	0.203 0
8		0.215 7	0.227 8	0.225 5	0.223 9	0.241 7	0.220 4	0.257 2	0.221 1
6		0.236 5	0.248 8	0.244 7	0.244 9	0.256 3	0.241 7	0 268 6	0.241 2
4		0.260 0	0.272 0	0.266 2	0.268 7	0.273 9	0.266 6	0.282 1	0.265 9
3		0.272 2*	0.283 2*	0.277 2*	0.280 5*	0.282 8*	0.278 7*	0.289 0*	0.278 1*
2		0.284 7	0.294 2	0.288 2	0.292 3	0.291 8	0.290 8	0.295 9	0.290 5
1		0.297 3*	0.305 2*	0.299 2*	0 304 2*	0 300 9*	0 303 3*	0.302 9*	0.303 2*
4/30	11.70	—	—	—	—	—	—	0.195 2	0.077 8
28		—	—	—	—	—	—	0.197 1	0 084 0
26		—	—	—	—	0.165 9	0.082 5	0.199 4	0.090 4
24		—	—	—	—	0.168 4	0.089 9	0.202 0	0.098 5
22		—	—	—	—	0.171 3	0.098 0	0.204 8	0.106 4
20		—	—	0.128 8	0.102 7	0.174 2	0.105 8	0.207 5	0.114 0
18		0 121 8	0 120 8	0 139 2	0 116 7	0 179 8	0 118 5	0.212 0	0.125 6
16		0.133 6	0.134 9	0.150 4	0.131 7	0.186 1	0.131 6	0.217 0	0.137 3
14		0.147 3	0.151 3	0.162 7	0.147 9	0 194 1	0 146 8	0.222 0	0.150 3
12		0.163 4	0.169 8	0.177 3	0.165 9	0.203 7	0.162 9	0.229 8	0.165 9
10		0.180 5	0.188 8	0.192 5	0.184 3	0.215 8	0.181 1	0.238 8	0.183 7
8		0.199 5	0.2094	0.210 3	0.205 0	0.230 4	0.202 3	0.249 7	0.203 8
6		0.223 5	0.234 3	0.232 5	0.230 0	0.247 1	0.226 6	0.261 8	0.226 3
4		0.248 7	0.259 7	0.256 2	0.256 0	0.265 7	0 252 8	0.275 9	0.252 2
3		0.263 0*	0.273 4*	0 268 6*	0.269 7*	0.275 6*	0.266 8*	0.283 2*	0.265 7*
2		0.278 2	0.287 6	0.281 6	0.284 2	0.286 1	0.281 9	0.291 1	0.280 4
1		0.294 0*	0.302 0*	0.295 4*	0.299 7*	0.297 5*	0.298 3*	0.300 0*	0.297 1*

Attached Table 2. (continued)

V/C	Y_c(%)	PB							
		2.5 PB		5.0 PB		7.5 PB		10.0 PB	
		x	y	x	y	x	y	x	y
3/34	6.391	—	—	—	—	0.160 8	0.048 0	0.191 8	0.050 3
32		—	—	—	—	0.161 2	0.051 1	0.192 6	0.054 2
30		—	—	—	—	0.162 1	0.055 6	0.193 8	0.059 9
28		—	—	—	—	0.163 2	0.060 9	0.195 0	0.065 0
26		—	—	—	—	0.164 2	0.065 5	0.196 3	0.070 8
24		—	—	—	—	0.165 8	0.071 1	0.198 2	0.077 2
22		—	—	—	—	0.167 7	0.078 2	0.200 4	0.084 7
20		—	—	—	—	0.170 2	0.086 7	0.203 0	0.093 0
18		—	—	0.122 8	0.089 5	0.173 0	0.094 8	0.206 0	0.102 0
16		—	—	0.131 8	0.102 4	0.176 5	0.104 8	0.209 2	0.111 8
14		0.125 1	0.121 8	0.143 1	0.118 4	0.182 4	0.118 8	0.214 2	0.125 0
12		0.139 8	0.139 5	0.155 7	0.135 6	0.190 3	0.135 3	0.220 6	0.140 7
10		0.157 6	0.160 0	0.171 8	0.156 2	0.200 5	0.153 6	0.227 8	0.156 5
8		0.178 0	0.183 3	0.190 8	0.179 9	0.214 9	0.176 1	0.238 7	0.178 6
6		0.202 2	0.210 1	0.212 2	0.205 2	0.231 1	0.201 0	0.251 1	0.203 1
4		0.231 2	0.240 5	0.239 3	0.236 1	0.252 0	0.231 9	0.266 0	0.231 9
3		0.247 8*	0.257 4*	0.254 3*	0.253 2*	0.264 1*	0.249 3*	0.274 7*	0.248 2*
2		0.266 3	0.275 6	0.270 8	0.271 9	0.277 7	0.268 7	0.284 7	0.267 0
1		0.287 0*	0.295 2*	0.289 3*	0.292 8*	0.292 9*	0.290 8*	0.296 4*	0.289 4*
2/38	3.048	—	—	—	—	0.162 3	0.028 0	—	—
36		—	—	—	—	0.162 8	0.031 0	—	—
34		—	—	—	—	0.163 0	0.034 0	0.191 1	0.034 4
32		—	—	—	—	0.163 5	0.037 3	0.191 8	0.037 9
30		—	—	—	—	0.164 0	0.040 9	0.192 5	0.042 0
28		—	—	—	—	0.164 7	0.045 1	0.193 7	0.047 1
26		—	—	—	—	0.165 3	0.049 2	0.194 9	0.052 6
24		—	—	—	—	0.166 0	0.053 8	0.196 2	0.057 8
22		—	—	—	—	0.167 0	0.059 4	0.197 8	0.064 3
20		—	—	—	—	0.168 5	0.066 6	0.199 8	0.071 8
18		—	—	—	—	0.170 1	0.074 2	0.202 1	0.080 8
16		—	—	—	—	0.172 8	0.083 9	0.205 2	0.091 0
14		—	—	0.125 3	0.087 3	0.176 2	0.095 5	0.208 7	0.102 6
12		0.116 6	0.107 6	0.136 3	0.104 8	0.181 3	0.109 4	0.213 9	0.117 0
10		0.133 2	0.127 8	0.150 0	0.124 0	0.188 2	0.125 8	0.220 0	0.133 0
8		0.154 0	0.153 0	0.168 5	0.149 1	0.200 5	0.149 5	0.229 4	0.155 1
6		0.182 5	0.185 7	0.194 2	0.181 1	0.218 9	0.179 0	0.244 0	0.184 0
4		0.217 5	0.224 5	0.226 3	0.219 2	0.242 0	0.214 8	0.260 0	0.216 2
3		0.237 4*	0.245 4*	0.244 2*	0.239 8*	0.255 6*	0.235 1*	0.269 3*	0.234 7*
2		0.259 2	0.267 5	0.263 8	0.262 4	0.271 2	0.258 2	0.280 3	0.256 7
1		0.283 3*	0.291 1*	0.285 6*	0.287 7*	0.289 2*	0.285 0*	0.293 7*	0.283 4*
1/38	1.180	—	—	—	—	0.168 0	0.014 0	—	—
36		—	—	—	—	0.168 1	0.016 0	—	—
34		—	—	—	—	0.168 2	0.018 0	—	—
32		—	—	—	—	0.168 2	0.020 2	—	—
30		—	—	—	—	0.168 4	0.023 4	0.192 8	0.024 0
28		—	—	—	—	0.168 6	0.027 0	0.193 6	0.028 1
26		—	—	—	—	0.168 9	0.030 9	0.194 2	0.032 6
24		—	—	—	—	0.169 1	0.035 2	0.195 2	0.038 0
22		—	—	—	—	0.169 6	0.040 2	0.196 5	0.043 6
20		—	—	—	—	0.170 1	0.045 4	0.197 6	0.049 3
18		—	—	—	—	0.170 9	0.051 8	0.199 1	0.056 4
16		—	—	—	—	0.172 0	0.058 3	0.200 8	0.063 8
14		—	—	—	—	0.173 8	0.068 8	0.203 8	0.074 5
12		—	—	—	—	0.176 3	0.080 4	0.207 0	0.086 9
10		—	—	0.128 5	0.087 0	0.180 4	0.095 0	0.212 0	0.102 9
8		0.127 3	0.115 7	0.144 7	0.112 4	0.187 2	0.114 1	0.219 0	0.122 8
6		0.153 9	0.149 1	0.167 8	0.144 7	0.200 0	0.142 2	0.229 0	0.147 0
4		0.189 5	0.191 1	0.201 2	0.186 7	0.223 2	0.182 1	0.245 9	0.182 8
3		0.210 3*	0.214 5*	0.219 8*	0.209 4*	0.236 9*	0.203 7*	0.255 2*	0.202 1*
2		0.236 0	0.242 0	0.242 7	0.236 8	0.254 7	0.231 0	0.267 7	0.228 0
1		0.268 6*	0.275 3*	0.272 1*	0.271 5*	0.278 4*	0.267 4*	0.285 3*	0.264 7*

Attached Table 2. (continued)

V/C	Y_c(%)	P							
		2.5 P		5.0 P		7.5 P		10.0 P	
		x	y	x	y	x	y	x	y
9/ 6	76.69	—	—	—	—	0.312 0	0.278 8	0.3218	0.284 5
4		0.296 3	0.286 5	0.300 3	0.287 0	0.311 7	0.292 8	0.317 6	0.296 6
3		0.301 1*	0.296 7*	0.303 9*	0.297 6*	0.311 2*	0.300 8*	0.315 1*	0.303 3*
2		0.305 0	0.305 1	0.306 7	0.306 0	0.310 7	0.308 1	0.312 8	0.309 4
1		0.308 0*	0.311 6*	0.308 8*	0.312 2*	0.310 3*	0.313 6*	0.311 0*	0.314 0*
8/14	57.62	—	—	—	—	—	—	0.334 2	0.234 9
12		—	—	—	—	0.311 7	0.237 0	0.331 2	0.247 0
10		—	—	0.287 0	0.238 0	0.311 6	0.249 7	0.328 2	0.258 2
8		0.280 0	0.248 8	0.291 4	0.253 4	0.311 6	0.262 6	0.325 0	0.270 0
6		0.288 1	0.267 1	0.296 3	0.270 4	0.311 4	0.278 5	0.321 3	0.282 9
4		0.296 2	0.285 0	0.301 2	0.286 8	0.311 4	0.291 5	0.317 5	0.295 5
3		0.300 7*	0.294 9*	0.303 9*	0.296 1*	0.311 1*	0.299 5*	0.315 2*	0.302 2*
2		0.304 8	0.304 0	0.306 5	0.304 7	0.310 7	0.307 0	0.313 1	0.308 4
1		0.308 1*	0.311 5*	0.308 6*	0.311 8*	0.310 3*	0.313 0*	0.311 3*	0.313 3*
7/22	41.98	—	—	—	—	—	—	0.343 0	0.188 3
20		—	—	—	—	—	—	0.341 0	0.198 8
18		—	—	—	—	0.309 3	0.196 2	0.339 1	0.208 8
16		—	—	—	—	0.309 9	0.207 4	0.336 8	0.219 2
14		—	—	0.280 1	0.2068	0.310 1	0.219 2	0.334 1	0.230 8
12		0.266 4	0.212 7	0.283 3	0.219 7	0.310 4	0.232 0	0.331 4	0.242 3
10		0.272 9	0.228 9	0.287 2	0.234 3	0.310 8	0.244 2	0 328 8	0.253 1
8		0.279 9	0 245 9	0.291 8	0.250 4	0.310 9	0.258 4	0 325 6	0.265 4
6		0 287 3	0.263 3	0.296 1	0.266 3	0.311 1	0.273 0	0 322 1	0 278 6
4		0 295 0	0 281 0	0.300 9	0.283 1	0.311 1	0.288 0	0.318 1	0.292 0
3		0.299 1*	0 290 6*	0.303 4*	0.292 1*	0.311 1*	0.296 0*	0.315 9*	0.298 9*
2		0.303 1	0.300 0	0.305 9	0.301 0	0.310 9	0.303 7	0.313 8	0.305 4
1		0.306 8*	0.308 7*	0.308 2*	0.309 2*	0.3106*	0.310 6*	0.311 8*	0.311 3*
6/26	29.30	—	—	—	—	—	—	0.345 7	0.160 4
24		—	—	—	—	0.305 8	0.154 7	0.344 1	0.169 8
22		—	—	—	—	0.306 2	0.163 8	0.342 6	0.178 5
20		—	—	0.270 2	0.162 1	0.306 9	0.174 5	0.340 9	0.188 2
18		0.250 4	0.165 8	0.273 1	0.173 8	0.307 5	0.187 0	0.338 8	0.199 5
16		0.254 8	0.176 8	0.276 1	0.185 2	0.308 0	0.197 6	0.337 0	0.209 5
14		0.259 3	0.190 9	0.279 4	0.197 9	0.308 4	0.209 5	0.334 9	0.220 3
12		0.264 7	0.205 2	0.282 9	0.212 1	0.309 0	0.222 2	0.332 1	0.232 9
10		0.270 3	0.220 4	0.286 2	0.226 0	0.309 2	0.235 0	0.329 3	0.245 0
8		0.277 0	0.237 2	0.290 5	0.242 1	0.309 9	0.250 2	0.325 9	0.258 4
6		0.284 2	0.255 0	0.295 0	0.258 5	0.310 1	0.265 0	0.322 6	0 271 6
4		0.293 2	0.275 9	0.300 1	0.277 8	0.310 7	0.283 1	0.318 1	0.287 1
3		0.297 4*	0.286 0*	0.302 5*	0.287 2*	0.310 8*	0.291 3*	0.316 4*	0.294 5*
2		0.301 6	0.296 0	0.305 0	0.296 7	0.310 7	0.299 3	0.314 6	0.301 8
1		0.305 8*	0.306 1*	0.307 5*	0.306 3*	0.310 5*	0.307 5*	0 312 6*	0.309 0*
5/30	19.27	—	—	—	—	0.301 0	0.117 0	0.349 0	0.130 8
28		—	—	0.261 8	0.113 5	0.301 8	0.125 3	0.347 8	0.138 8
26		0.234 8	0.114 0	0.263 5	0.122 4	0.302 2	0.133 1	0.346 8	0.146 0
24		0.237 2	0.122 3	0.265 2	0.130 4	0.303 0	0.142 3	0.345 0	0.155 5
22		0.240 2	0.131 5	0.267 3	0 139 8	0.303 8	0.150 0	0.343 7	0 164 4
20		0.243 8	0.141 9	0.269 4	0.149 9	0.304 2	0.160 6	0.342 2	0 173 5
18		0 247 6	0 153 2	0 271 8	0.160 4	0.305 2	0 171 1	0 340 1	0 184 0
16		0.251 5	0.164 4	0.274 4	0.171 8	0.306 0	0.183 0	0.338 2	0.195 1
14		0.256 0	0 177 4	0.277 5	0.184 7	0.306 8	0.195 1	0.336 0	0.206 6
12		0.260 8	0.191 3	0.280 6	0.197 7	0.307 1	0.208 0	0.333 5	0.218 7
10		0.266 5	0.207 5	0.284 5	0.213 7	0.308 0	0.223 0	0.330 8	0.232 8
8		0.272 8	0.224 0	0.288 5	0.229 6	0.308 7	0.237 5	0.328 0	0.246 4
6		0.280 6	0.244 4	0.293 2	0.248 7	0.309 3	0.255 5	0.324 3	0.263 0
4		0.289 8	0.266 7	0.298 6	0.269 9	0.310 0	0.275 0	0.319 8	0.280 7
3		0.294 8*	0.278 8*	0.301 5*	0.281 2*	0.310 2*	0.285 4*	0.317 3*	0.289 7*
2		0.300 0	0.291 2	0.304 5	0.292 8	0.310 3	0.295 9	0.314 8	0.298 6
1		0.305 1*	0.303 8*	0.307 4*	0.304 5*	0 310 3*	0.306 3*	0.312 4*	0.307 5*

Attached Table 2. (continued)

V/C	Y_c(%)	P							
		2.5 P		5.0 P		7.5 P		10.0 P	
		x	y	x	y	x	y	x	y
4/32	11.70	0.226 5	0.077 4	0.257 4	0.083 3	0.296 2	0.090 6	—	—
30		0.228 5	0.084 7	0.258 8	0.090 7	0.296 9	0.097 9	0.344 0	0.108 0
28		0.230 2	0.090 9	0.260 0	0.097 1	0.297 9	0.106 2	0.343 2	0.117 2
26		0.232 2	0.097 8	0.261 8	0.105 2	0.298 6	0.113 5	0.342 8	0.124 8
24		0.234 8	0.106 2	0.263 5	0.113 2	0.299 3	0.122 5	0.342 1	0.133 7
22		0.237 1	0.114 3	0.265 2	0.121 8	0.300 1	0.130 6	0.341 1	0.142 4
20		0.239 4	0.122 1	0.267 0	0.130 0	0.301 0	0.139 6	0.340 0	0.150 0
18		0.243 0	0.133 2	0.269 3	0.140 8	0.301 6	0.150 0	0.338 6	0.162 6
16		0.246 7	0.145 2	0.271 8	0.152 0	0.302 8	0.162 1	0.337 0	0.175 6
14		0.250 9	0.158 5	0.274 7	0.166 0	0.303 5	0.175 5	0.335 1	0.187 5
12		0.255 9	0.173 0	0.277 8	0.180 8	0.304 5	0.190 5	0.333 1	0.201 4
10		0.261 9	0.190 3	0.281 4	0.196 7	0.305 6	0.206 0	0.330 6	0.216 2
8		0.268 5	0.208 9	0.285 5	0.215 0	0.306 6	0.222 8	0.328 0	0.231 8
6		0.276 3	0.230 0	0.290 3	0.234 7	0.307 6	0.241 6	0.324 8	0.249 3
4		0.285 5	0.253 1	0.295 8	0.256 5	0.308 4	0.262 2	0.321 0	0.268 6
3		0.290 6*	0.266 1*	0.298 9*	0.268 8*	0.308 9*	0.273 4*	0.318 7*	0.279 0*
2		0.296 2	0.280 7	0.302 2	0.282 5	0.309 3	0.285 9	0.316 2	0.290 2
1		0.302 6*	0.297 3*	0.305 9*	0.298 2*	0.309 7*	0.300 0*	0.313 3*	0.302 6*
3/34	6.391	0.223 0	0.054 3	—	—	—	—	—	—
32		0.224 2	0.058 7	0.255 7	0.063 0	—	—	—	—
30		0.225 2	0.063 8	0.2568	0.069 0	0.292 2	0.075 0	—	—
28		0.226 8	0.069 8	0.257 9	0.075 0	0.293 0	0.081 2	—	—
26		0.228 6	0.076 5	0.259 0	0.082 2	0.293 8	0.089 2	0.334 3	0.097 8
24		0.230 5	0.083 2	0.260 2	0.089 1	0.294 4	0.096 7	0.334 1	0.105 5
22		0.232 9	0.091 1	0.262 0	0.097 8	0.295 3	0.105 7	0.334 0	0.114 6
20		0.235 4	0.100 3	0.263 9	0.107 4	0.296 1	0.115 1	0.333 2	0.124 0
18		0.238 0	0.109 4	0.265 7	0.116 3	0.296 9	0.123 9	0.332 9	0.133 2
16		0.241 0	0.119 8	0.268 0	0.127 2	0.298 1	0.135 6	0.332 0	0.145 6
14		0.244 9	0.132 5	0.270 7	0.139 7	0.299 2	0.147 5	0.330 9	0.157 2
12		0.249 8	0.148 0	0.273 9	0.153 9	0.300 3	0.161 8	0.330 1	0.171 5
10		0.254 8	0.163 8	0.277 2	0.170 7	0.302 0	0.179 4	0.328 6	0.188 9
8		0.261 5	0.184 5	0.281 9	0.191 0	0.303 7	0.198 1	0.326 9	0.207 5
6		0.269 1	0.207 2	0.287 0	0.213 5	0.305 7	0.220 8	0.324 3	0.229 3
4		0.279 2	0.234 2	0.292 8	0.238 6	0.307 2	0.244 8	0.321 4	0.251 7
3		0.285 2*	0.249 8*	0.296 0*	0.253 0*	0.308 0*	0.258 3*	0.319 5*	0.264 4*
2		0.292 2	0.268 0	0.299 7	0.270 0	0.308 8	0.274 0	0.317 0	0.279 0
1		0.300 4*	0.289 9*	0.304 3*	0.290 8*	0.309 5*	0.293 0*	0.313 9*	0.296 1*
2/30	3.048	0.223 1	0.043 2	—	—	—	—	—	—
28		0.224 5	0.049 1	0.255 9	0.052 5	—	—	—	—
26		0.226 0	0.055 5	0.256 9	0.059 4	—	—	—	—
24		0.227 7	0.062 1	0.258 2	0.066 9	0.288 2	0.071 9	—	—
22		0.229 8	0.069 6	0.259 7	0.075 0	0.289 0	0.079 9	0.323 0	0.086 1
20		0.232 0	0.077 9	0.261 2	0.083 8	0.290 2	0.090 1	0.323 1	0.096 2
18		0.234 5	0.087 3	0.263 2	0.093 5	0.291 2	0.099 5	0.323 3	0.106 3
16		0.237 2	0.098 0	0.265 2	0.104 5	0.292 2	0.110 6	0.323 5	0.118 1
14		0.240 6	0.110 0	0.267 6	0.116 3	0.293 8	0.123 5	0.323 5	0.131 7
12		0.244 9	0.124 5	0.270 9	0.132 0	0.295 6	0.139 2	0.323 3	0.147 7
10		0.250 1	0.142 2	0.274 8	0.150 0	0.297 9	0.156 9	0.323 0	0.165 9
8		0.257 0	0.163 5	0.279 1	0.170 7	0.300 0	0.178 1	0.321 9	0.186 2
6		0.266 1	0.192 3	0.285 0	0.199 2	0.302 5	0.205 8	0.320 7	0.213 2
4		0.275 8	0.220 8	0.290 8	0.226 1	0.304 8	0.232 1	0.318 9	0.239 0
3		0.281 8*	0.237 7*	0.294 2*	0.241 9*	0.305 9*	0.246 8*	0.317 8*	0.252 7*
2		0.289 2	0.258 3	0.298 4	0.261 2	0.307 1	0.264 7	0.316 1	0.269 1
1		0.298 5*	0.284 0*	0.303 6*	0.285 5*	0.308 5*	0.287 3*	0.313 6*	0.289 8*

Attached Table 2. (continued)

V/C	Y_c(%)	P							
		2.5 P		5.0 P		7.5 P		10.0 P	
		x	y	x	y	x	y	x	y
1/26	1.180	0.225 1	0.035 5	—	—	—	—	—	—
24		0.226 6	0.041 8	—	—	—	—	—	—
22		0.227 9	0.047 3	0.259 0	0.050 9	—	—	—	—
20		0.229 5	0.054 2	0.260 1	0.058 6	0.283 1	0.062 5	—	—
18		0.231 2	0.061 8	0.261 2	0.066 7	0.284 1	0.070 6	0.306 9	0.074 8
16		0.233 1	0.069 6	0.262 5	0.074 6	0.285 2	0.079 0	0.307 8	0.083 9
14		0.236 1	0.081 0	0.264 5	0.086 3	0.286 8	0.090 3	0.308 4	0.095 2
12		0.239 4	0.094 0	0.267 0	0.100 6	0.288 4	0.105 9	0.309 4	0.111 0
10		0.244 1	0.111 2	0.270 1	0.117 8	0.290 5	0.122 9	0.310 2	0.128 2
8		0.249 6	0.130 3	0.274 2	0.137 5	0.293 2	0.142 9	0.311 4	0.148 1
6		0.257 0	0.155 9	0.279 4	0.162 8	0.296 0	0.168 2	0.312 6	0.173 7
4		0.266 8	0.187 4	0.285 4	0.192 7	0.299 1	0.197 4	0.313 2	0.203 2
3		0.272 6*	0.205 1*	0.288 8*	0.209 5*	0.300 8*	0.213 6*	0.313 4*	0.218 9*
2		0.280 8	0.229 6	0.293 6	0.233 0	0.303 0	0.236 1	0.313 2	0.240 4
1		0.292 8*	0.265 3*	0.300 4*	0.267 2*	0.306 0*	0.269 0*	0.312 2*	0.271 6*

Attached Table 2. (continued)

V/C	Y_c(%)	RP							
		2.5 RP		5.0 RP		7.5 RP		10.0 RP	
		x	y	x	y	x	y	x	y
9/ 6	76.69	0.332 2	0.291 0	0.343 1	0.298 8	0.351 2	0.305 2	0.359 0	0.311 8
4		0.323 4	0.301 0	0.330 1	0.306 0	0.335 0	0.309 9	0.340 0	0.314 0
3		0.318 9*	0.306 2*	0.323 3*	0.309 5*	0.326 5*	0.312 2*	0.329 7*	0.314 8*
2		0.314 9	0.310 8	0.317 2	0.312 6	0.319 0	0.314 1	0.320 5	0.315 5
1		0.311 8*	0.314 3*	0.312 6*	0.315 0*	0.313 2*	0.315 5*	0.313 6*	0.316 0*
8/14	57.62	0.362 1	0.249 6	—	—	—	—	—	—
12		0.355 2	0.259 4	0.381 8	0.274 2	0.400 2	0.285 9	—	—
10		0.347 9	0.269 9	0.368 5	0.282 8	0.383 0	0.293 0	0.398 3	0.304 9
8		0.340 6	0.279 3	0.357 0	0.290 0	0.368 2	0.298 3	0.380 0	0.308 2
6		0.332 7	0.289 8	0.344 0	0.297 8	0.352 1	0.304 2	0.360 0	0.311 2
4		0.323 9	0.300 0	0.330 8	0.305 2	0.336 0	0.309 2	0.341 2	0.313 5
3		0.319 4*	0.305 2*	0.324 1*	0.308 8*	0.327 6*	0.311 5*	0.331 1*	0.314 4*
2		0.315 4	0.310 0	0.318 0	0.312 0	0.320 0	0.313 6	0.321 8	0.315 2
1		0.312 2*	0.313 8*	0.313 2*	0.314 6*	0.313 9*	0.315 2*	0.314 5*	0.315 8*
7/20	41.98	0.381 1	0.214 3	—	—	—	—	—	—
18		0.375 1	0.224 1	0.418 6	0.245 9	—	—	—	—
16		0.368 8	0.234 2	0.407 6	0.254 0	0.434 6	0.268 9	0.464 8	0.287 8
14		0.362 0	0.244 8	0.395 8	0.262 8	0.419 5	0.276 2	0.445 6	0.293 1
12		0.355 5	0.254 5	0.384 1	0.271 0	0.404 0	0.283 4	0.426 0	0.298 0
10		0.348 7	0.264 8	0.371 3	0.279 8	0.387 1	0.290 6	0.404 0	0.303 0
8		0.341 7	0.274 5	0.360 3	0.286 9	0.372 2	0.296 3	0.385 1	0.306 7
6		0.333 8	0.285 4	0.347 0	0.294 9	0.356 2	0.302 2	0.364 8	0.309 8
4		0.325 4	0.297 1	0.333 2	0.303 2	0.338 9	0.307 9	0.344 6	0.312 5
3		0.321 1*	0.302 5*	0.326 7*	0.307 0*	0.330 8*	0.310 3*	0.334 9*	0.313 7*
2		0.317 0	0.307 6	0.320 6	0.310 4	0.323 2	0.312 5	0.325 8	0.314 8
1		0.313 3*	0.312 2*	0.315 0*	0.313 5*	0.316 3*	0.314 5*	0.317 5*	0.315 7*
6/24	29.30	0.392 7	0.189 2	—	—	—	—	—	—
22		0.387 7	0.1978	0.444 9	0.221 9	—	—	—	—
20		0.383 3	0.205 6	0.436 8	0.228 3	0.473 5	0.246 4	—	—
18		0.377 3	0.215 8	0.424 5	0.238 2	0.458 1	0.254 9	0.496 1	0.275 1
16		0.371 8	0.225 1	0.413 6	0.246 7	0.444 8	0.262 2	0.478 1	0.281 2
14		0.365 2	0.235 5	0.402 3	0.255 2	0.428 5	0.270 5	0.455 2	0.288 1
12		0.358 2	0.246 2	0.390 0	0.264 6	0.412 5	0.278 4	0.436 0	0.293 6
10		0.350 9	0.257 8	0.376 9	0.273 8	0.396 0	0.286 0	0.415 0	0.298 9
8		0.343 7	0.268 8	0.364 8	0.282 0	0.379 1	0.292 9	0.393 0	0.303 8
6		0.336 2	0.279 9	0.352 0	0.290 4	0.363 5	0.298 7	0.374 0	0.307 4
4		0.327 2	0.292 9	0.337 1	0.300 1	0.343 9	0.305 6	0.350 8	0.311 2
3		0.323 0*	0.298 9*	0.330 0*	0.304 4*	0.334 8*	0.308 6*	0.339 7*	0.312 7*
2		0.318 8	0.304 8	0.323 2	0.308 5	0.326 1	0.311 3	0.329 2	0.314 1
1		0.314 5*	0.310 6*	0.316 6*	0.312 4*	0.317 9*	0.313 9*	0.319 3*	0.315 3*
5/26	19.27	0.401 1	0.165 2	—	—	—	—	—	—
24		0.396 5	0.173 8	0.468 3	0.197 8	—	—	—	—
22		0.392 4	0.181 4	0.458 1	0.206 8	0.504 5	0.224 8	—	—
20		0.387 3	0.190 9	0.448 4	0.215 0	0.491 5	0.233 0	0.539 6	0.253 5
18		0.382 1	0.200 7	0.437 2	0.224 2	0.476 1	0.242 1	0.518 5	0.262 0
16		0.376 3	0.210 8	0.426 1	0.233 1	0.461 7	0.250 6	0.498 6	0.269 5
14		0.370 3	0.221 1	0.414 2	0.242 8	0.445 4	0.259 6	0.476 7	0.277 6
12		0.363 5	0.232 5	0.402 2	0.252 3	0.430 3	0.267 5	0.457 9	0.284 1
10		0.356 0	0.245 2	0.388 0	0.263 0	0.410 8	0.277 3	0.433 2	0.291 8
8		0.349 0	0.257 0	0.374 8	0.272 9	0.393 2	0.285 2	0.410 5	0.298 0
6		0.339 6	0.271 8	0.358 5	0.284 2	0.372 6	0.294 1	0.385 1	0.303 9
4		0.329 8	0.286 9	0.342 1	0.295 4	0.351 5	0.302 4	0.359 4	0.309 0
3		0.324 8*	0.294 4*	0.333 8*	0.301 0*	0.340 4*	0.306 2*	0.346 1*	0.311 2*
2		0.319 9	0.301 9	0.325 6	0.306 5	0.329 6	0.309 8	0.333 2	0.313 1
1		0.315 0*	0.309 2*	0.317 7*	0.311 6*	0.319 4*	0.313 2*	0.321 0*	0.314 8*

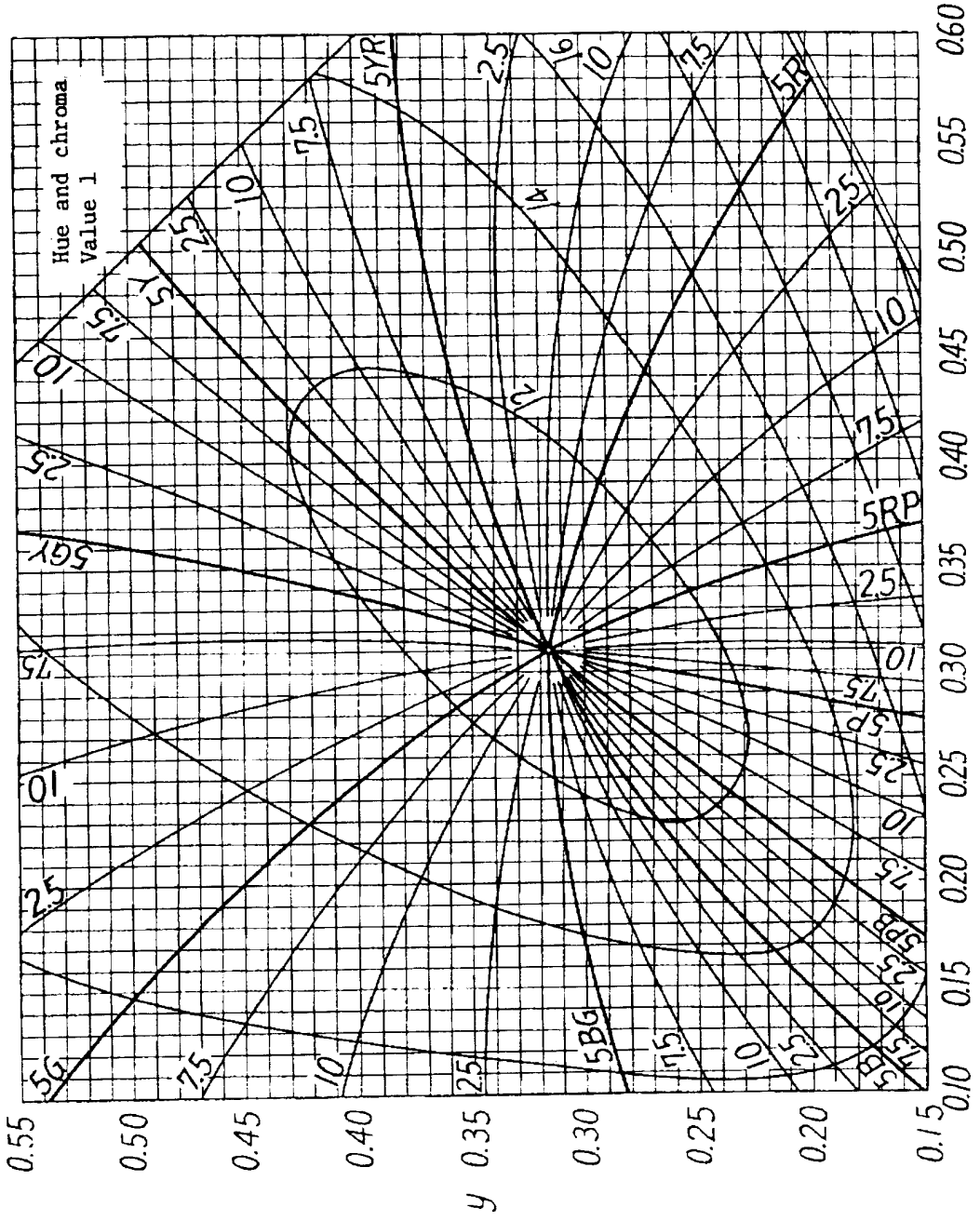
Attached Table 2. (continued)

V/C	Y_c(%)	RP							
		2.5 RP		5.0 RP		7.5 RP		10.0 RP	
		x	y	x	y	x	y	x	y
4/26	11.70	0.404 8	0.142 8	—	—	—	—	—	—
24		0.401 1	0.150 4	—	—	—	—	—	—
22		0.396 7	0.159 3	0.465 6	0.182 1	—	—	—	—
20		0.392 6	0.167 9	0.457 1	0.190 6	0.513 0	0.210 1	0.567 4	0.231 9
18		0.386 5	0.180 2	0.445 5	0.202 3	0.496 5	0.221 7	0.546 6	0.242 4
16		0.380 7	0.192 3	0.433 9	0.213 9	0.479 9	0.232 9	0.523 4	0.253 0
14		0.374 8	0.203 9	0.422 5	0.224 9	0.462 9	0.243 7	0.502 0	0.262 3
12		0.368 3	0.216 2	0.410 4	0.236 1	0.445 0	0.254 1	0.478 9	0.271 7
10		0.360 8	0.230 1	0.396 0	0.248 9	0.425 9	0.265 1	0.452 8	0.281 1
8		0.353 3	0.243 8	0.383 3	0.260 0	0.407 2	0.275 0	0.428 2	0.289 0
6		0.344 2	0.259 5	0.367 1	0.273 3	0.385 0	0.285 9	0.399 9	0.297 2
4		0.334 0	0.277 0	0.349 1	0.287 2	0.361 2	0.296 3	0.371 5	0.304 2
3		0.328 7*	0.285 8*	0.340 2*	0.294 0*	0.349 4*	0.301 2*	0.356 8*	0.307 5*
2		0.323 1	0.295 1	0.331 0	0.301 0	0.337 1	0.306 1	0.341 7	0.310 6
1		0.317 0*	0.305 2*	0.321 1*	0.308 4*	0.324 1*	0.311 1*	0.326 1*	0.313 5*
3/22	6.391	0.401 8	0.130 4	—	—	—	—	—	—
20		0.396 9	0.141 3	0.457 7	0.159 3	—	—	—	—
18		0.392 9	0.150 6	0.450 3	0.169 5	0.513 0	0.189 3	—	—
16		0.387 6	0.162 9	0.441 8	0.180 9	0.499 1	0.201 1	0.562 8	0.224 1
14		0.381 8	0.175 8	0.431 3	0.194 4	0.483 1	0.214 0	0.538 0	0.236 9
12		0.375 4	0.189 8	0.419 9	0.208 9	0.465 4	0.227 3	0.513 9	0.248 9
10		0.368 1	0.205 4	0.407 3	0.223 5	0.444 5	0.241 9	0.485 1	0.261 8
8		0.359 8	0 223 3	0 393 0	0.239 5	0.423 4	0.255 6	0.455 2	0.274 1
6		0.350 1	0.242 5	0.376 5	0.256 9	0.399 0	0.270 8	0 421 8	0.286 4
4		0.340 0	0.262 4	0.358 6	0.274 2	0.373 9	0.285 1	0.388 9	0.296 9
3		0.334 0*	0.273 6*	0.348 4*	0.283 8*	0.360 1*	0.292 5*	0.371 4*	0.301 9*
2		0.327 2	0.286 1	0.337 0	0.294 0	0.345 0	0.300 1	0.352 6	0.306 8
1		0.319 3*	0.300 2*	0.324 3*	0.304 8*	0.328 4*	0.308 0*	0.332 3*	0.311 6*
2/20	3.048	0.380 2	0.108 0	—	—	—	—	—	—
18		0.377 8	0.118 8	0.433 8	0.134 0	—	—	—	—
16		0.374 8	0.131 0	0.426 9	0.145 4	0.474 4	0.159 5	—	—
14		0.371 1	0.144 9	0.418 0	0.159 8	0.462 4	0.173 7	0.512 9	0.188 8
12		0.366 8	0.161 8	0.408 0	0.176 4	0.448 1	0.190 3	0.491 1	0.206 0
10		0.361 7	0.180 0	0.397 1	0.193 9	0.432 1	0.208 2	0.467 8	0.223 7
8		0.355 5	0.200 3	0.385 8	0.214 0	0.413 7	0.227 6	0.442 8	0.241 9
6		0.347 0	0.225 9	0.370 8	0.238 0	0.391 8	0.249 0	0.413 9	0.260 8
4		0 338 2	0.249 6	0.355 8	0.259 7	0.370 2	0.268 3	0.385 0	0.277 8
3		0.333 6*	0.261 4*	0.347 9	0.270 6*	0.358 9*	0.278 3*	0.370 0*	0 286 5*
2		0.327 9	0.275 4	0.338 3	0.282 9	0.345 9	0.289 2	0.353 2	0.295 7
1		0.320 3*	0.293 2*	0.326 0*	0.297 8*	0.330 0*	0.301 7*	0.333 6*	0.305 6*
1/16	1.180	0.336 8	0.090 2	—	—	—	—	—	—
14		0.336 8	0.102 0	0.381 1	0.113 8	—	—	—	—
12		0.336 1	0.118 1	0.377 2	0.128 3	0.424 0	0.140 0	0.466 8	0.151 4
10		0.335 4	0.135 1	0.372 7	0.145 8	0.413 2	0.158 0	0.452 1	0.171 0
8		0.334 2	0.155 1	0.366 0	0.166 2	0.400 5	0.179 3	0.435 7	0.192 1
6		0 332 1	0.181 1	0.358 8	0.192 0	0.386 5	0.203 6	0.415 1	0.216 9
4		0.329 0	0.209 5	0.350 3	0.219 6	0.370 5	0.230 0	0 392 0	0.242 3
3		0 327 2*	0.225 1*	0.345 3*	0.234 7*	0.361 6*	0.244 1*	0.379 3*	0.255 4*
2		0 324 0	0 245 9	0 337 8	0 254 2	0 349 8	0.261 7	0 362 9	0 271 0
1		0.318 6*	0.275 2*	0.326 6*	0.280 5*	0.333 2*	0.285 0*	0.340 6*	0.290 7*

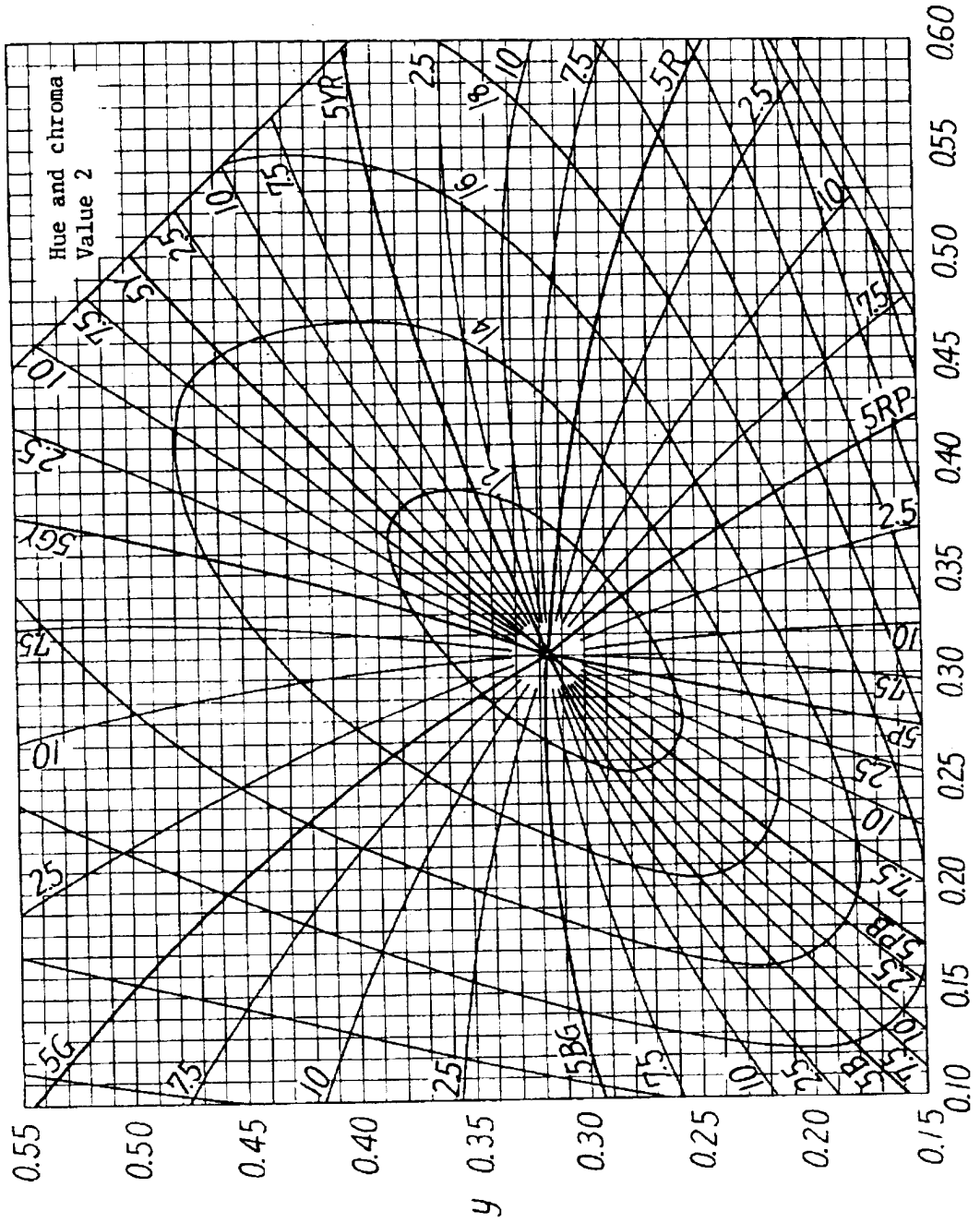
Note *: These values have been obtained by the cubic interpolation from the values given in the original text.

Remarks: This table has been reprinted from "Journal of the Optical Society of America, Vol. 33 (1943), pp. 397 to 405, Table 1" with permission of the author. However, Y_c (%) was calculated by the formula shown in Remarks of Attached Table 1.

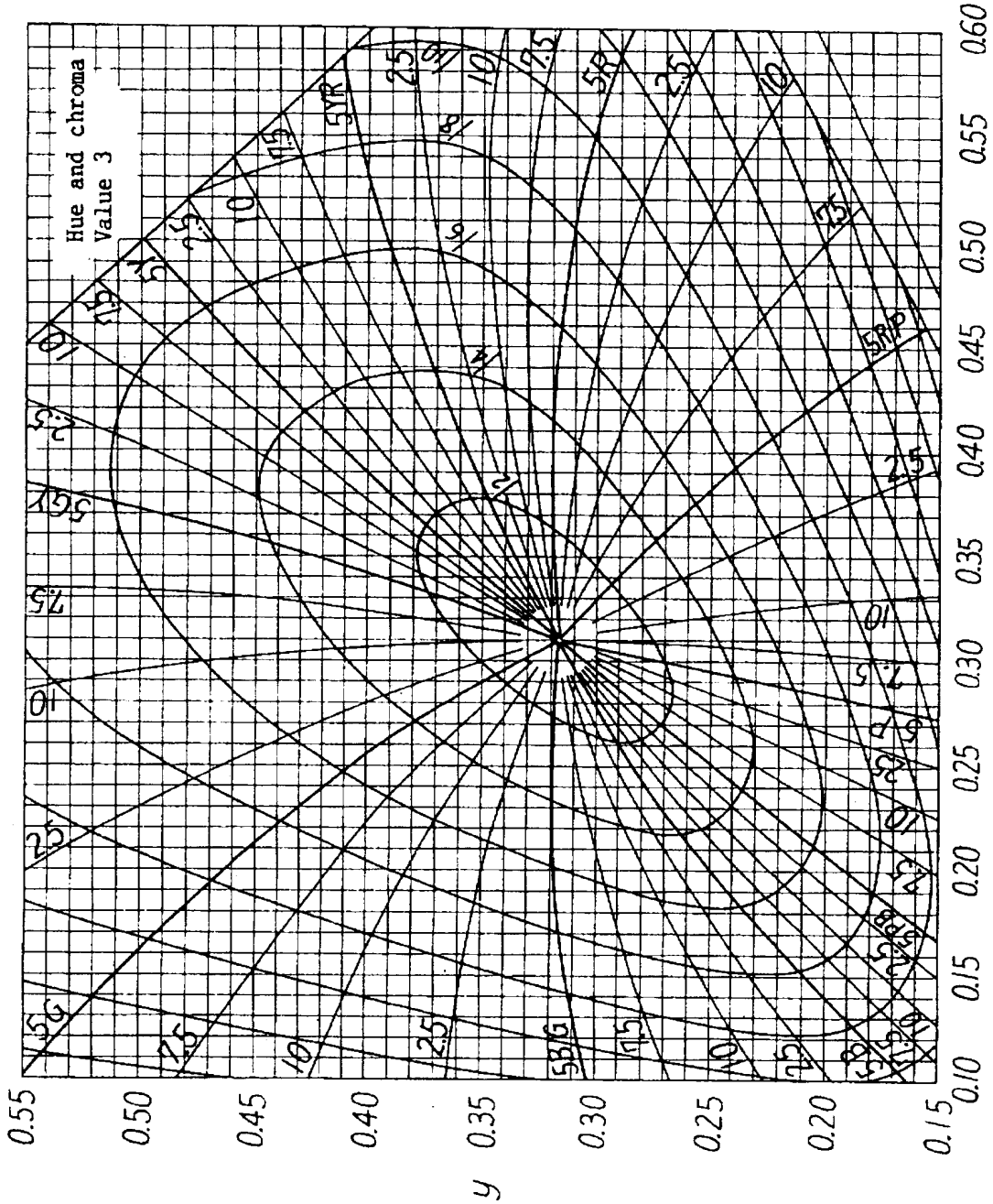
Attached Fig. 1

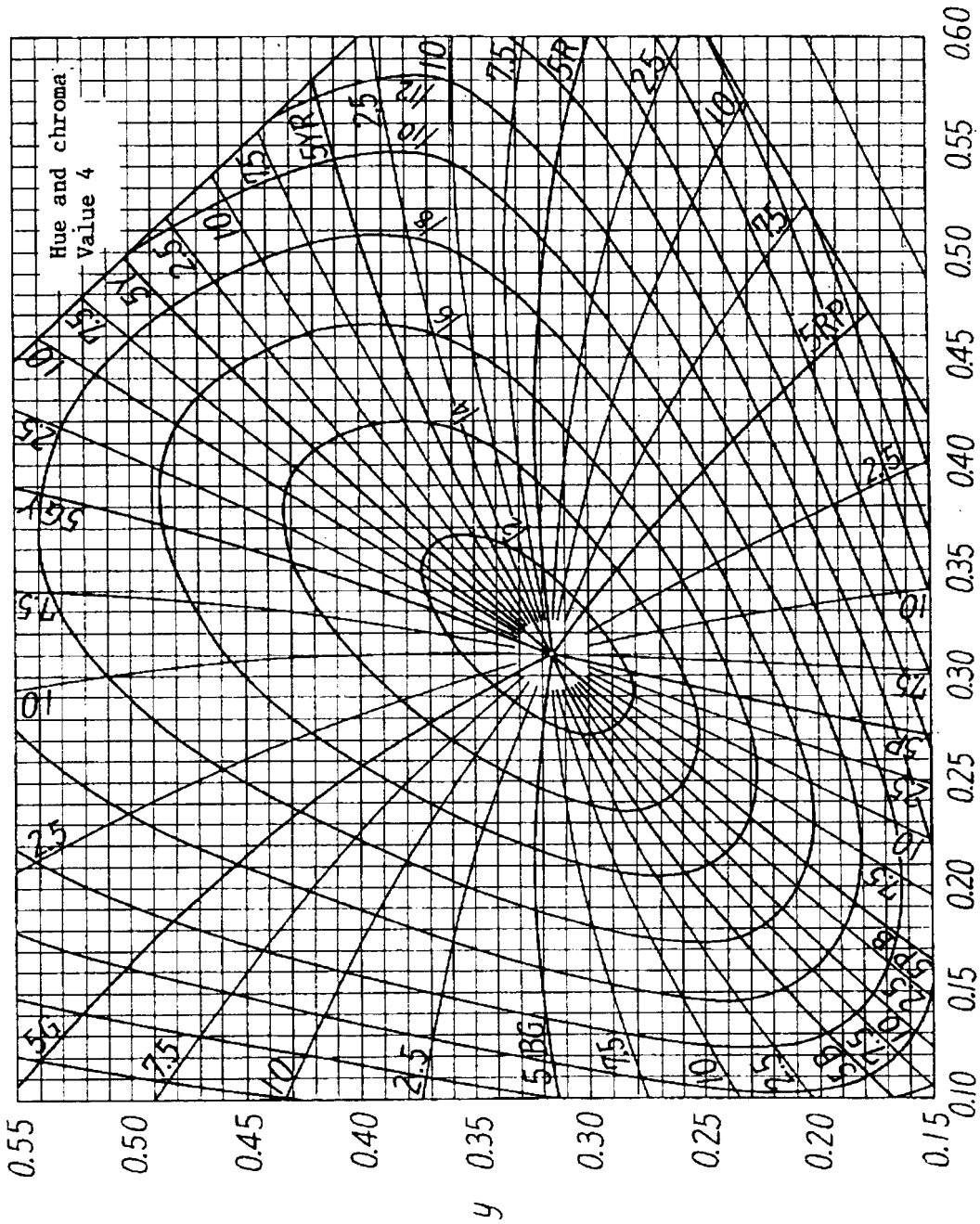


Attached Fig. 2

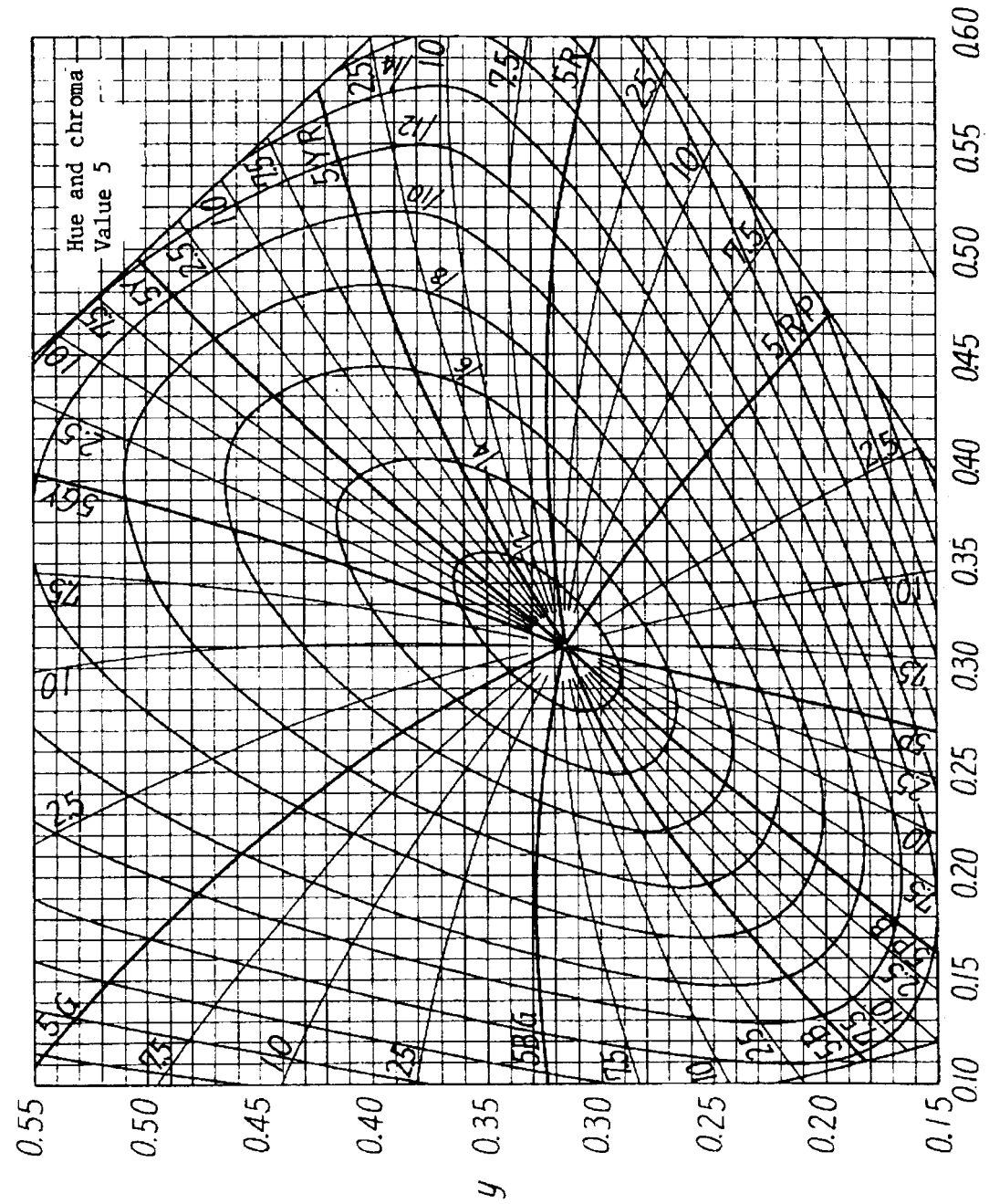


Attached Fig. 3



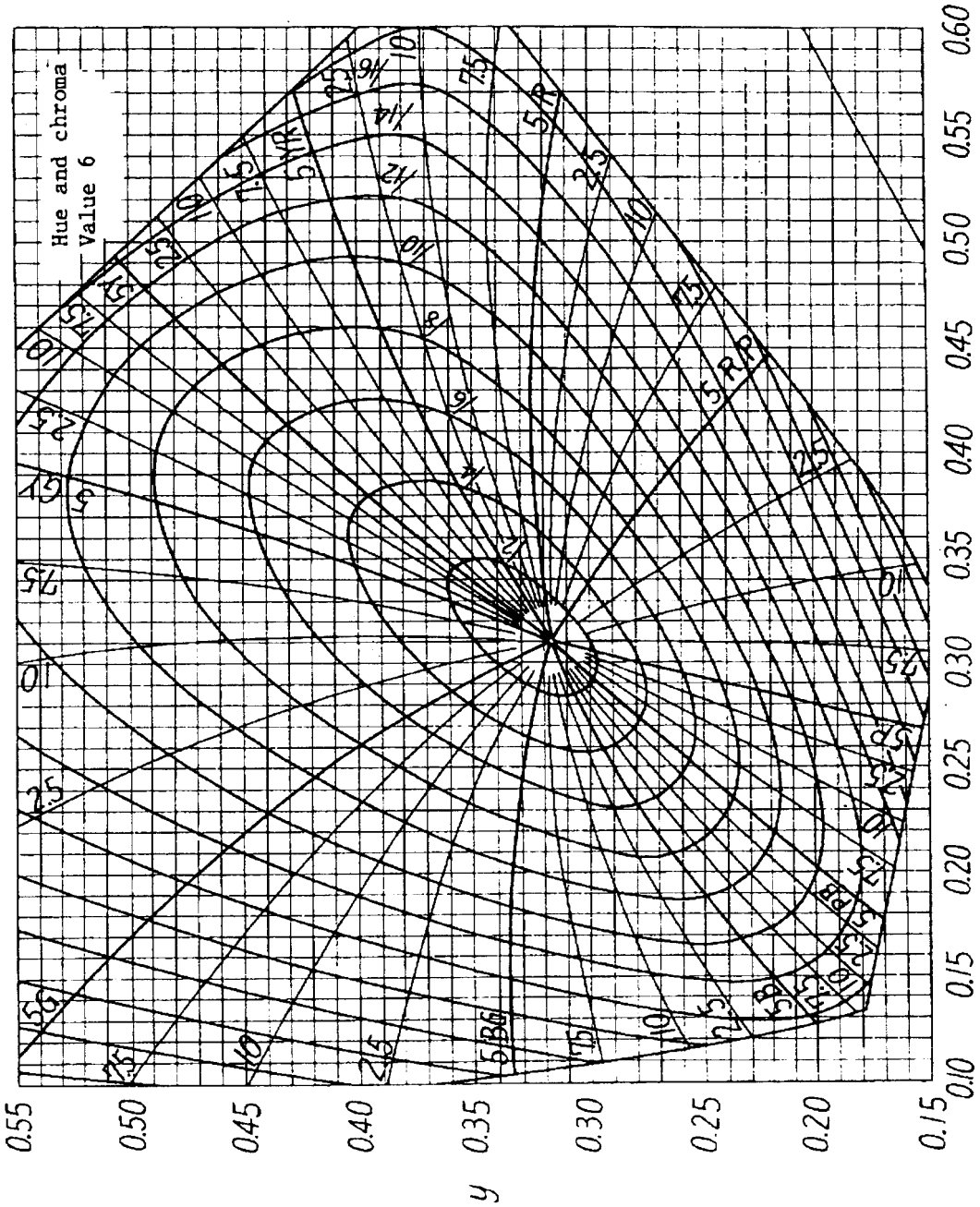


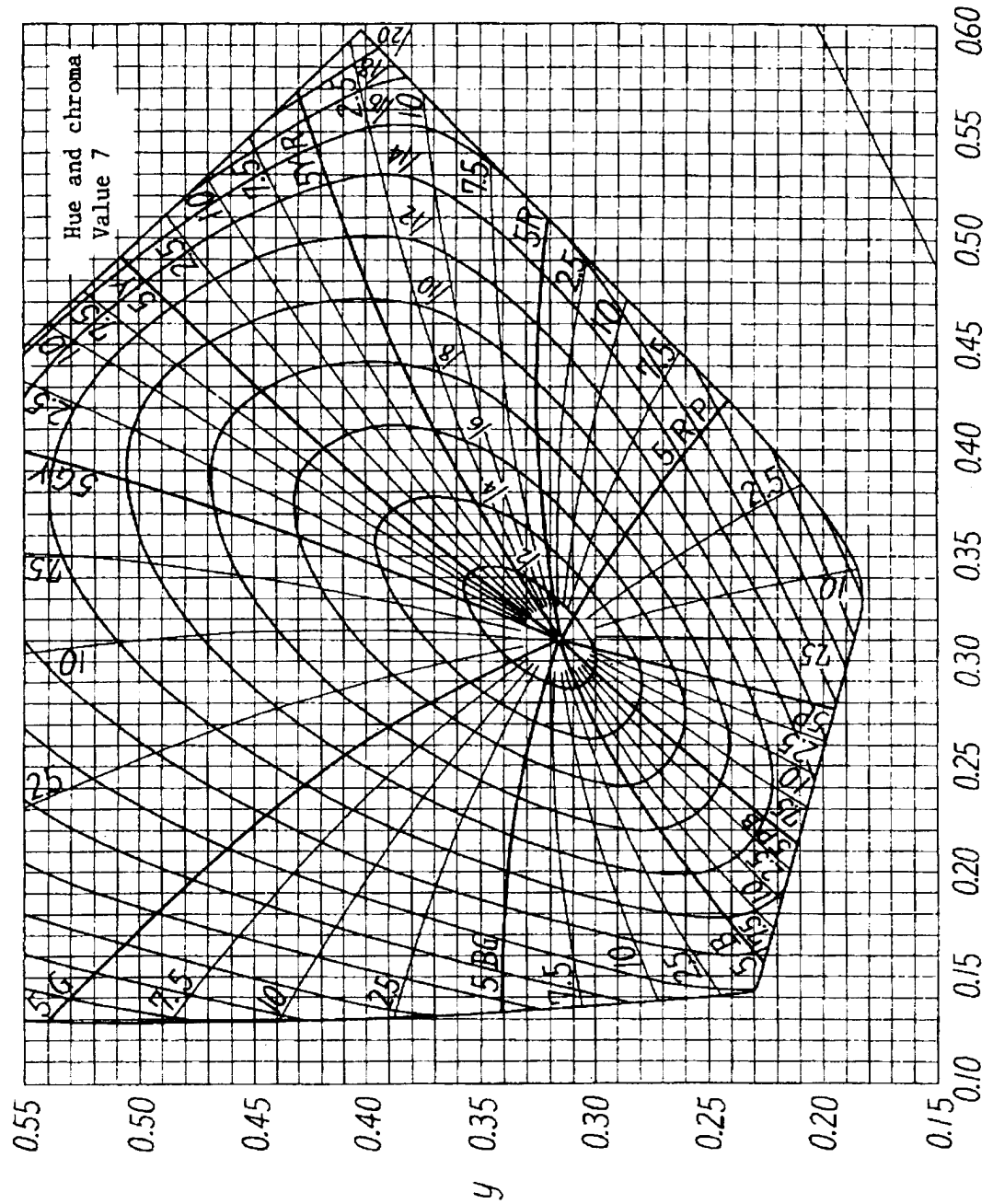
Attached Fig. 4



Attached Fig. 5

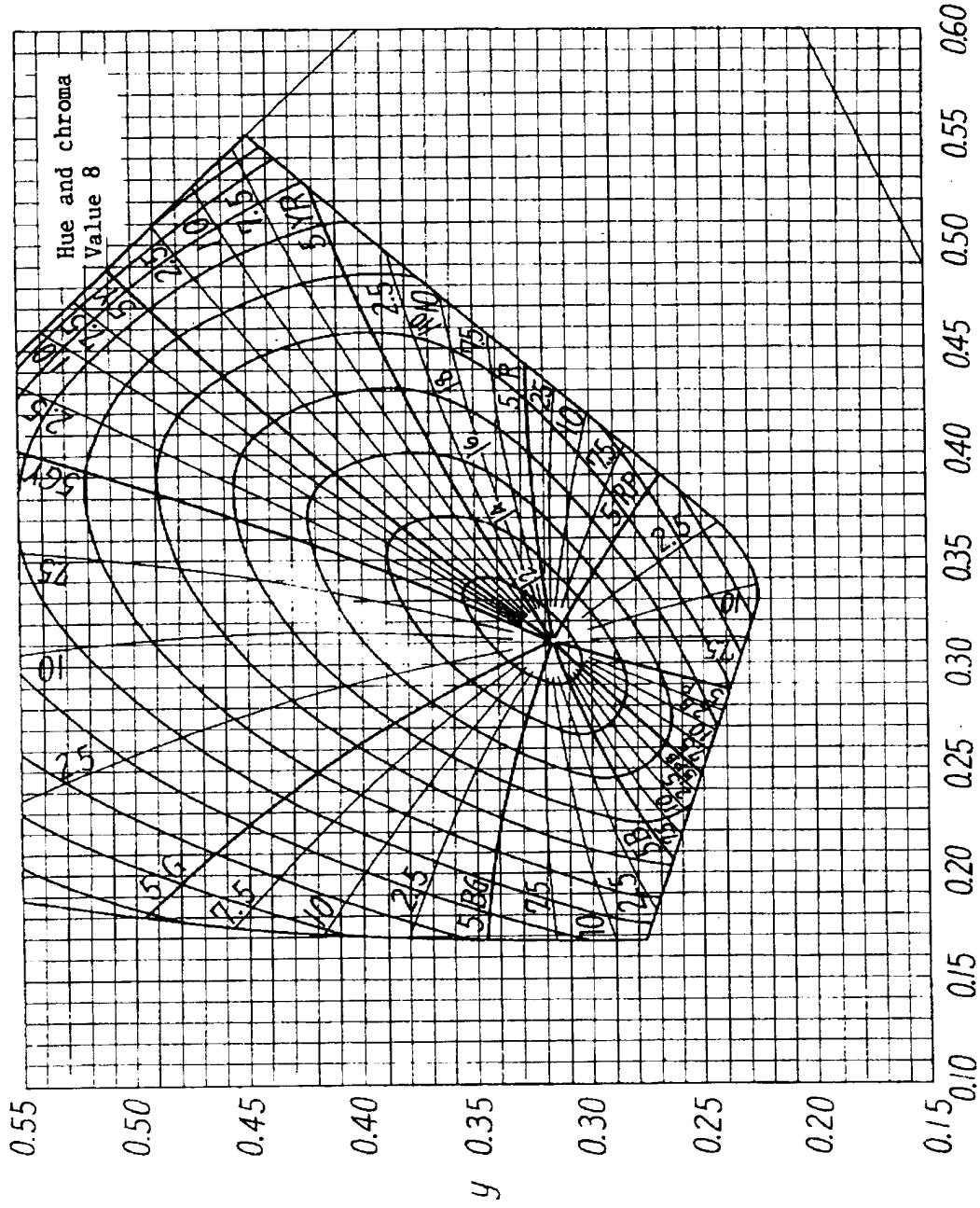
Attached Fig. 6



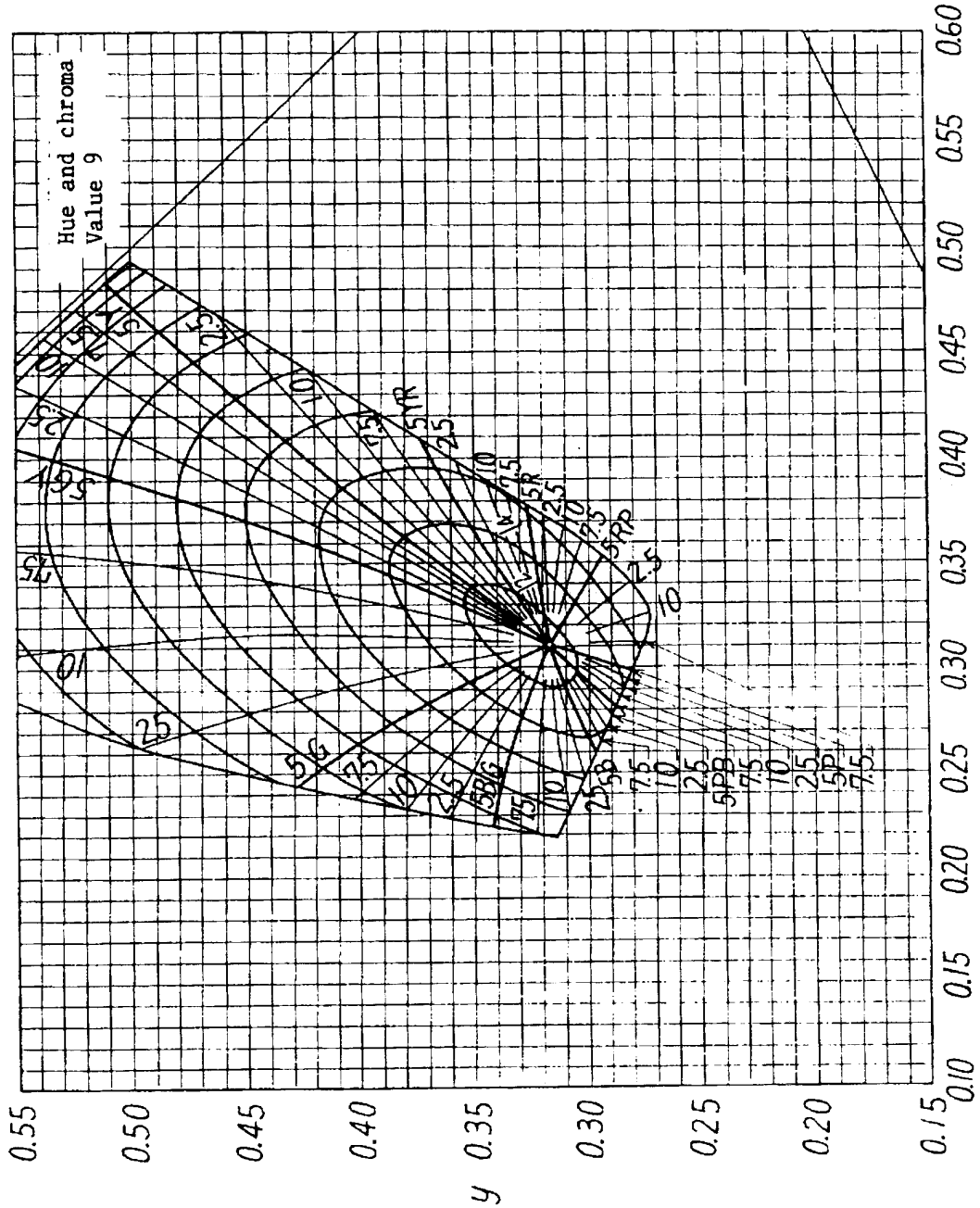


Attached Fig. 7

Attached Fig. 8



Attached Fig. 9



Annex Basis of colour system according to three attributes under illumination by standard illuminant D_{65}

1. Scope This Annex specifies the basis on which the basis Y_C, x_C, y_C of the colour system according to three attributes under the lighting by the standard illuminant C is converted to the basis Y_D, x_D, y_D of the colour system under the lighting by the standard illuminant D_{65}.

2. Basis of colour system according to three attributes under the illumination by standard illuminant D_{65} The basis of colour system according to three attributes under the illumination by standard illuminant D_{65} shall be Y_D of luminance factor and the values of chromaticity coordinates x_D, y_D shown in Annex Attached Table 1.

The relation between the hue and chroma of the equal lightness and the values of chromaticity coordinates x_D, y_D is shown in Annex Attached Figs. 1 to 9.

3. Determination of notation to specify colours The notation to specify colours shall be, in the method to obtain from the values of Y_D, x_D and y_D, determined by means of interpolation or extrapolation([5]) using Annex Attached Table 1.

Note ([5]) Example of calculation by interpolation is shown in Informative reference 2.

4. Recording of notation to specify colours The notation to specify colours shall be recorded as shown in the following examples as to hue H_D, value V_D and chroma C_D for chromatic colours and as to value V_D for achromatic colours:

Example 1. When H_D = 5R, V_D = 4 and C_D = 10 in chromatic colour,

5R 4/10 [D]

Example 2. When H_D = 7.5P, V_D = 2.5 and C_D = 2.5 in chromatic colour,

7.5P 2.5/2.5 [D]

Example 3. When V_D = 8 in achromatic colour,

N8 [D]

Example 4. When H_D = 7.5R, V_D = 5.5 and C_D = 0.3 in chromatic colour,

N5.5 (R0.3) [D]

Annex Attached Table 1. Basis of colour system according to three attributes (chromatic colour)

	2.5R			5R			7.5R			10R		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
9/ 6	75.93	0.371 0	0.328 6	75.96	0.377 8	0.336 0	76.00	0.385 5	0.345 4	76.06	0.392 3	0.354 8
4	76.42	0.347 8	0.329 4	76.41	0.352 8	0.333 9	76.37	0.358 4	0.339 4	76.40	0.363 1	0.345 8
3	76.55	0.335 7	0.329 5	76.54	0.339 1	0.332 7	76.52	0.343 1	0.336 3	76.51	0.346 5	0.340 6
2	76.60	0.323 9	0.329 3	76.59	0.326 9	0.331 2	76.58	0.329 2	0.333 3	76.58	0.331 3	0 335 6
1	76.64	0.316 8	0.329 2	76.64	0.317 6	0.330 0	76.63	0.318 5	0.330 8	76.63	0.319 3	0.331 5
8/10	56.52	0.418 2	0.323 6	56.50	0.430 8	0.334 8	56.46	0.444 4	0.348 9	56.56	0.453 7	0.365 4
8	57.06	0.394 2	0.326 4	57.01	0.404 3	0.335 2	57.01	0.415 6	0.347 0	57.16	0.424 1	0.361 0
6	57.38	0.370 5	0.328 3	57.36	0.377 6	0.335 3	57.35	0.386 1	0.343 7	57.34	0.393 8	0.354 1
4	57.45	0.349 2	0.329 3	57.44	0.354 2	0.333 8	57.43	0.359 5	0.339 1	57.42	0.365 0	0 345 9
3	57.50	0.337 4	0.329 4	57.49	0.340 8	0.332 4	57.48	0.344 5	0.336 3	57.47	0.348 4	0 340 8
2	57.54	0.326 6	0.329 3	57 53	0.328 3	0.330 9	57.53	0.330 6	0.333 4	57.52	0.333 0	0 335 9
1	57.57	0.318 0	0.329 2	57.57	0.318 5	0.329 8	57 56	0.319 5	0.331 0	57.56	0.320 5	0.331 8
7/16	41.03	0.497 5	0.311 5	—	—	—	41.02	0.540 3	0.349 9	41.11	0.555 1	0 375 7
14	41.21	0.472 3	0.314 8	41.18	0.490 6	0.329 5	41.19	0 510 6	0.349 6	41.28	0.526 2	0 373 6
12	41.50	0.448 1	0.319 5	41 47	0.463 7	0.332 2	41.51	0.480 9	0.349 8	41.55	0.494 9	0 371 6
10	41.66	0.422 2	0.323 3	41 65	0.435 5	0.334 4	41.64	0.450 0	0.349 1	41.64	0.462 2	0 366 7
8	41.73	0.399 8	0.325 7	41.72	0.410 2	0.334 9	41 70	0.422 7	0.347 0	41 70	0.433 4	0 361 6
6	41.79	0.376 3	0.327 6	41.78	0.383 9	0.334 7	41.77	0 391 9	0.343 6	41.76	0.401 2	0 354 8
4	41.86	0.353 2	0.328 5	41.85	0.358 4	0.333 4	41.84	0.364 2	0.339 2	41 83	0.370 0	0 346 8
3	41.89	0.342 1	0.328 9	41.88	0.345 7	0.332 3	41.87	0.350 0	0.336 6	41.87	0.354 2	0 342 0
2	41.91	0.331 4	0.329 2	41 91	0.333 6	0.331 1	41 91	0 336 5	0.334 0	41.90	0.338 9	0 337 2
1	41.94	0.321 6	0.329 3	41 94	0.322 5	0 330 0	41.94	0 323 9	0.331 5	41 93	0.325 0	0 332 8
6/18	28 87	0 533 2	0 299 0	28 87	0 560 6	0 318 7	28 88	0 585 8	0 342 6	28 85	0 600 9	0 373 5
16	28.90	0.509 2	0.304 1	28.88	0.533 6	0.322 7	28.87	0 558 3	0.345 7	28 88	0.574 6	0.373 9
14	28.94	0.483 4	0.310 8	28.93	0.505 6	0.327 0	28 92	0 529 0	0.347 9	28 92	0.547 8	0 373 4
12	28.99	0.461 0	0.315 7	28 98	0.479 6	0.330 2	28 97	0.498 8	0.348 7	28.97	0.516 5	0 371 6
10	29.04	0.436 0	0.320 2	29 03	0.451 6	0 332 8	29 02	0 468 4	0.348 3	29.02	0.483 2	0 368 2
8	29.10	0.410 3	0.323 7	29 08	0.422 2	0 334 0	29 08	0 434 9	0.346 6	29 07	0.447 4	0 362 7
6	29.14	0.386 8	0.326 0	29.13	0.395 5	0.334 2	29 13	0.403 2	0.343 5	29.12	0.413 1	0 356 4
4	29.19	0.360 0	0.327 4	29 18	0.366 1	0 333 0	29.18	0.372 4	0.339 8	29 17	0.379 7	0 348 5
3	29.22	0.347 2	0.328 1	29 21	0.351 4	0 332 1	29 20	0.356 6	0.337 4	29.20	0.362 1	0.343 6
2	29.24	0.334 9	0 328 6	29.24	0.337 4	0.331 0	29 23	0.341 1	0.334 6	29.23	0.344 7	0.338 5
1	29.26	0.323 5	0.329 1	29.26	0.324 3	0.329 9	29 26	0 326 4	0.331 9	29.25	0.328 0	0.333 6
5/20	19.05	0.584 8	0.277 1	19 05	0.618 0	0 300 5	19 05	0.640 2	0.323 4	—	—	—
18	18.99	0.559 8	0.284 9	18.99	0.595 8	0 307 0	19 00	0.618 2	0.329 6	19.10	0.630 1	0.364 2
16	18.94	0.535 1	0.292 8	18 93	0.567 5	0.313 8	18.93	0 592 4	0.335 6	18 95	0.604 0	0.367 2
14	18.99	0.509 5	0.300 7	18.98	0.537 8	0 320 4	18 97	0 561 5	0.340 6	18 98	0.577 8	0.368 9
12	19.02	0.486 6	0.306 7	19.01	0.510 8	0.325 0	19.01	0 530 7	0.343 6	19.01	0.549 3	0.369 6
10	19.07	0.457 6	0.313 3	19 06	0.478 4	0.329 5	19 05	0.495 6	0.345 9	19.05	0.513 1	0.368 0
8	19.11	0.429 3	0.318 7	19 10	0.444 9	0 332 0	19.09	0.459 4	0.346 1	19.09	0.473 6	0.364 1
6	19.15	0.399 8	0.322 6	19 14	0.411 4	0 333 0	19 13	0.421 2	0.343 6	19.13	0.432 6	0.358 2
4	19.18	0.369 5	0.325 5	19 18	0.377 4	0 332 5	19 17	0.383 8	0.339 6	19.17	0.390 9	0 349 7
3	19.20	0.354 1	0.326 7	19.20	0.359 6	0 331 8	19 20	0.364 4	0.337 1	19.19	0.369 9	0.344 6
2	19.22	0.339 2	0.327 6	19.22	0.342 3	0 330 9	19 22	0.345 6	0.334 5	19 21	0.349 5	0 339 3
1	19.24	0.325 3	0.328 4	19.24	0.326 5	0 330 0	19 24	0.328 2	0.331 8	19.23	0.330 3	0.334 0
4/20	—	—	—	—	—	—	11 49	0 681 0	0 300 1	—	—	—
18	11 52	0.595 7	0.266 5	11 55	0.636 0	0.290 8	11 60	0.655 2	0.311 5	—	—	—
16	11 55	0 567 9	0 276 7	11 55	0 607 6	0 300 6	11 56	0 628 1	0 320 9	11 63	0 641 2	0 353 4
14	11.49	0 542 3	0.285 4	11.48	0.577 4	0 308 9	11 49	0.598 5	0.329 1	11.54	0.616 2	0.357 8
12	11.52	0.512 3	0.295 2	11.51	0.542 4	0.317 3	11 51	0.563 0	0.335 6	11.52	0.581 2	0.361 2
10	11.55	0.482 2	0.303 5	11.54	0.508 1	0.323 2	11.54	0.526 4	0.339 9	11 54	0.543 5	0.361 9
8	11.58	0.451 7	0.310 8	11.57	0.472 8	0.327 8	11.57	0.488 1	0.342 1	11 57	0.501 7	0.361 2
6	11.61	0.418 2	0.317 4	11.60	0.433 6	0.330 9	11.60	0.444 8	0.341 8	11 60	0.456 2	0.357 3
4	11.63	0.384 4	0.322 6	11.63	0.395 2	0.332 0	11 63	0.402 4	0.339 4	11 62	0.410 8	0.350 3
3	11.65	0.367 1	0.324 6	11.64	0.374 9	0.331 8	11.64	0.379 8	0.337 3	11.64	0.386 3	0.345 6
2	11.66	0.349 5	0.326 4	11.66	0.354 1	0.331 2	11 66	0.357 0	0.334 7	11.65	0.361 3	0.340 3
1	11.67	0.331 4	0.327 8	11.67	0.333 4	0.330 2	11 67	0.334 6	0.331 9	11.67	0.336 6	0.334 7

Annex Attached Table 1. (continued)

	2.5R			5R			7.5R			10R		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
3/16	6.151	0.616 8	0.248 9	6.152	0.655 1	0.268 1	6.182	0.682 5	0.288 2	—	—	—
14	6.249	0.588 1	0.261 7	6.252	0.623 8	0.281 5	6.274	0.650 9	0.302 7	6.362	0.670 0	0.325 6
12	6.288	0.559 4	0.273 4	6.289	0.592 6	0.293 5	6.298	0.618 4	0.314 9	6.310	0.633 3	0.337 1
10	6.280	0.524 6	0.285 9	6.276	0.554 4	0.306 2	6.276	0.576 1	0.326 9	6.279	0.588 9	0.346 1
8	6.301	0.487 2	0.298 0	6.298	0.510 6	0.316 7	6.297	0.528 3	0.334 3	6.298	0.541 6	0.351 5
6	6.322	0.445 5	0.308 6	6.319	0.463 2	0.323 8	6.318	0.477 2	0.338 0	6.318	0.488 2	0.352 6
4	6.341	0.406 3	0.316 7	6.338	0.418 7	0.327 6	6.337	0.427 5	0.338 5	6.337	0.433 9	0.349 2
3	6.350	0.385 1	0.320 4	6.348	0.394 0	0.328 8	6.347	0.400 6	0.337 2	6.347	0.405 5	0.346 0
2	6.360	0.362 7	0.323 7	6.359	0.368 0	0.329 5	6.358	0.372 4	0.335 1	6.358	0.376 1	0.341 6
1	6.370	0.338 8	0.326 5	6.369	0.341 0	0.329 5	6.369	0.343 2	0.332 3	6.369	0.345 3	0.335 9
2/14	2.867	0.579 9	0.211 8	2.854	0.632 4	0.229 8	2.854	0.680 3	0.252 6	2.861	0.716 7	0.273 7
12	2.940	0.549 8	0.229 6	2.930	0.597 3	0.249 7	2.930	0.641 5	0.272 4	2.955	0.673 8	0.294 8
10	2.986	0.518 9	0.248 0	2.983	0.561 0	0.267 4	2.982	0.598 7	0.290 3	2.992	0.626 5	0.313 9
8	2.995	0.484 1	0.265 0	2.992	0.520 0	0.284 6	2.991	0.547 8	0.306 3	2.990	0.574 4	0.328 3
6	3.008	0.444 6	0.283 2	3.005	0.469 3	0.299 8	3.004	0.491 9	0.317 8	3.003	0.512 9	0.337 7
4	3.018	0.407 0	0.298 5	3.016	0.423 0	0.311 2	3.015	0.437 7	0.324 4	3.014	0.451 7	0.339 8
3	3.023	0.387 2	0.306 0	3.021	0.398 9	0.316 3	3.021	0.409 0	0.326 4	3.020	0.418 9	0.339 0
2	3.028	0.365 5	0.313 4	3.027	0.373 2	0.320 9	3.026	0.379 0	0.327 7	3.026	0.384 7	0.336 8
1	3.033	0.341 2	0.320 7	3.033	0.344 9	0.324 9	3.033	0.347 2	0.328 3	3.032	0.349 5	0.333 2
1/10	1.119	0.512 5	0.194 3	1.113	0.565 9	0.213 4	1.104	0.614 9	0.231 4	1.096	0.668 0	0.251 2
8	1.146	0.488 7	0.216 1	1.141	0.534 5	0.234 6	1.137	0.576 8	0.252 5	1.135	0.620 3	0.273 8
6	1.156	0.458 8	0.239 1	1.155	0.495 0	0.256 9	1.154	0.528 9	0.274 3	1.156	0.562 6	0.295 6
4	1.160	0.423 2	0.263 4	1.159	0.448 3	0.278 6	1.158	0.471 8	0.293 7	1.157	0.498 4	0.310 7
3	1.163	0.404 7	0.275 8	1.162	0.424 3	0.289 3	1.161	0.441 6	0.302 5	1.161	0.460 3	0.317 2
2	1.165	0.382 2	0.289 6	1.165	0.396 0	0.300 5	1.164	0.407 0	0.310 6	1.164	0.417 5	0.322 1
1	1.168	0.352 9	0.306 2	1.168	0.360 3	0.312 7	1.168	0.365 4	0.318 5	1.168	0.369 1	0.325 3

Annex Attached Table 1. (continued)

	2.5YR			5YR			7.5YR			10YR		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
9/ 8	—	—	—	—	—	—	76.14	0.424 7	0.402 5	76.34	0.421 1	0.415 5
6	76.12	0.396 5	0.365 6	76.21	0.397 9	0.376 0	76.35	0.397 2	0.386 0	76.51	0.395 3	0.397 4
4	76.45	0.366 8	0.353 1	76.47	0.369 2	0.361 7	76.51	0.370 1	0.369 3	76.58	0.369 5	0.377 7
3	76.51	0.350 4	0.346 2	76 53	0.353 5	0.353 3	76.56	0.355 4	0.359 7	76.61	0.355 7	0.366 8
2	76.58	0.334 8	0.339 4	76 59	0.338 0	0.344 5	76.61	0.340 5	0.349 7	76.65	0.341 5	0.355 0
1	76.63	0.321 7	0.333 5	76.64	0.324 0	0.336 3	76 66	0.326 1	0.339 4	76.68	0.327 1	0.342 5
8/20	—	—	—	—	—	—	56 32	0.540 0	0.451 3	56.54	0.524 8	0.470 5
18	—	—	—	—	—	—	56.44	0.532 3	0.448 3	57.12	0.515 4	0.469 3
16	—	—	—	—	—	—	56 67	0.519 7	0.444 1	57.25	0.505 2	0.464 7
14	—	—	—	56.42	0.511 3	0.417 6	57 06	0.501 8	0.437 7	57.28	0.491 9	0 457 3
12	56.38	0.489 9	0.390 2	56.69	0.487 0	0.409 2	57 20	0.481 2	0.428 5	57.32	0.474 0	0.446 8
10	56.74	0.458 5	0.382 1	57.20	0.458 6	0.400 6	57 26	0.457 1	0.416 7	57.36	0.452 2	0.433 5
8	57.24	0.429 6	0.374 5	57.27	0 432 6	0.390 0	57 32	0.431 6	0.403 2	57.41	0.428 4	0.418 2
6	57.33	0.398 5	0.364 3	57.35	0.400 9	0.375 8	57 39	0.401 7	0.386 4	57.46	0.400 6	0.399 1
4	57.42	0.369 4	0.353 7	57.43	0.371 5	0.361 7	57 47	0.372 1	0.369 3	57.52	0.371 9	0.378 2
3	57 47	0.352 5	0.346 7	57.48	0.355 6	0.353 5	57 50	0.357 1	0.359 8	57.55	0.357 6	0.367 1
2	57 52	0.336 2	0.339 7	57.53	0.340 0	0 344 9	57 54	0.342 0	0.349 8	57.57	0.343 0	0 355 3
1	57 57	0.322 4	0.333 6	57 57	0.325 4	0.336 7	57.58	0.327 2	0.339 5	57.60	0.328 1	0.342 7
7/20	41 09	0.583 4	0.404 3	41 27	0 565 5	0.429 9	—	—	—	—	—	—
18	41.17	0.570 5	0.403 0	41.49	0.554 8	0.428 7	41 50	0.539 8	0.450 8	40 96	0.528 8	0 468 8
16	41.32	0.552 9	0.400 9	41.51	0 542 5	0.425 4	41 60	0.529 8	0.447 5	41.70	0.515 8	0.467 8
14	41.50	0.530 0	0.397 6	41.55	0.524 6	0.420 3	41.62	0.515 9	0.441 5	41.72	0.504 9	0.461 6
12	41 56	0.501 1	0.391 2	41 59	0 500 8	0 412 8	41 65	0.496 2	0.432 8	41 74	0.488 2	0.452 6
10	41.63	0.468 7	0.383 4	41 65	0 471 9	0.403 4	41 70	0.470 4	0.421 1	41 77	0.465 8	0 439 4
8	41 69	0.439 2	0.375 8	41 71	0 441 7	0 391 8	41 75	0 442 3	0 407 1	41 81	0.440 0	0 423 8
6	41 76	0.407 8	0.366 2	41 77	0 411 1	0.379 1	41 80	0.412 3	0.390 9	41.85	0.411 1	0 404 9
4	41.83	0.374 2	0.354 5	41.84	0.377 5	0 363 5	41 86	0.379 4	0.371 7	41 90	0.379 5	0 382 4
3	41 87	0.357 9	0.348 1	41 87	0 361 0	0 355 1	41.89	0.362 9	0.361 8	41.92	0.363 3	0.370 1
2	41 90	0.342 0	0.341 6	41 91	0 344 8	0.346 7	41 92	0.346 2	0.351 4	41.95	0.346 6	0 357 2
1	41 94	0.326 9	0.335 3	41 94	0 328 7	0.337 9	41.96	0.329 5	0.340 6	41.97	0.329 8	0 343 6
6/18	28 87	0.587 2	0.403 1	28 73	0 572 5	0 426 0	—	—	—	—	—	—
16	28 90	0.569 3	0.401 1	28 94	0.558 2	0.425 8	28.81	0.546 1	0.448 3	—	—	—
14	28.93	0.548 8	0.397 7	28.96	0 541 3	0.421 5	29.02	0.530 1	0.443 9	29.09	0.517 1	0 465 1
12	28.96	0.522 2	0.392 9	28.99	0 519 6	0.415 7	29.04	0.513 2	0.436 8	29 10	0.502 8	0 457 3
10	29 01	0.490 4	0.386 2	29 03	0 492 5	0.407 4	29.07	0.489 9	0.427 0	29 13	0.482 9	0.446 6
8	29 06	0.455 2	0.378 0	29 07	0 460 4	0.396 7	29.10	0.460 1	0.412 9	29 15	0.456 6	0 431 4
6	29.11	0.420 4	0.368 7	29 12	0 424 8	0.383 4	29.15	0.425 5	0.395 9	29.19	0.424 7	0.411 3
4	29 17	0.383 3	0.356 9	29.18	0 386 4	0.366 5	29.19	0.388 1	0.375 2	29.23	0.387 7	0 386 8
3	29 20	0.365 6	0.350 5	29 21	0 368 2	0.357 8	29.22	0.369 7	0.364 7	29 24	0.369 7	0 373 8
2	29 23	0 348 1	0.343 7	29 23	0 350 1	0.348 8	29 24	0.351 2	0.353 6	29.26	0.351 4	0 359 9
1	29.26	0.330 6	0.336 5	29 26	0 331 7	0.339 3	29.27	0.332 3	0.341 9	29.28	0.332 5	0.345 1
5/16	18 99	0.593 4	0.399 1	—	—	—	—	—	—	—	—	—
14	18.99	0.572 7	0 397 2	19 02	0 562 9	0.421 8	18.91	0.550 6	0.444 9	—	—	—
12	19.02	0.548 4	0.393 9	19 04	0 541 5	0.416 9	19.08	0.531 8	0.440 5	19 13	0.518 3	0 462 8
10	19 05	0.518 4	0.388 8	19.06	0 516 1	0.410 4	19.09	0.509 9	0.431 5	19.14	0.500 6	0 452 8
8	19 08	0.481 1	0.381 8	19 10	0 483 8	0.401 6	19.12	0.482 0	0.419 5	19.16	0.476 0	0 439 2
6	19 13	0.438 7	0.371 9	19 13	0 443 6	0.388 3	19.15	0.445 0	0.402 7	19.18	0.443 0	0 420 1
4	19 17	0.395 2	0.359 1	19.18	0 399 1	0.370 9	19.19	0.401 0	0.380 8	19 21	0.400 9	0 393 5
3	19 19	0.374 1	0.352 2	19 20	0 377 3	0.361 1	19.21	0.378 8	0.368 6	19.22	0.379 0	0 378 6
2	19.21	0.353 5	0.345 0	19.22	0 355 7	0.350 8	19.23	0.356 5	0.355 8	19.24	0.356 8	0.362 8
1	19 24	0.333 1	0 337 3	19 24	0 334 3	0.340 1	19 25	0.334 5	0.342 6	19.26	0 334 7	0 346 3
4/12	11 52	0.580 6	0.392 6	11.51	0.572 9	0.417 2	—	—	—	—	—	—
10	11.54	0.548 0	0.388 7	11.56	0.542 7	0.412 4	11.58	0.534 0	0.436 8	11.61	0.522 3	0 460 0
8	11 57	0.508 5	0.382 5	11.58	0.507 5	0.403 9	11.59	0.503 3	0.424 7	11.62	0.495 0	0 445 7
6	11 59	0.463 3	0.374 2	11 60	0 466 5	0 392 3	11.61	0.466 1	0 409 2	11.63	0.461 5	0 427 6
4	11 62	0.416 7	0.362 6	11.63	0 420 9	0.376 4	11.64	0.422 4	0.389 3	11.65	0.419 9	0 403 3
3	11.64	0.391 4	0.355 5	11 64	0.394 9	0.366 3	11.65	0.396 3	0.376 0	11.66	0.394 9	0 387 6
2	11 66	0.365 3	0.347 5	11.66	0.367 8	0.354 9	11.67	0.368 6	0.361 2	11.68	0.368 1	0.369 9
1	11 67	0.339 0	0.338 7	11 68	0.340 2	0.342 5	11.68	0 340 5	0.345 4	11.69	0.340 4	0.350 4

Annex Attached Table 1. (continued)

	2.5YR			5YR			7.5YR			10YR		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
3/10	6.283	0.594 7	0.382 5	—	—	—	—	—	—	—	—	—
8	6.299	0.548 5	0.380 1	6.307	0.545 4	0.406 6	6.321	0.537 6	0.433 0	6.321	0.528 8	0.457 6
6	6.317	0.497 3	0.374 4	6.323	0.497 6	0.395 7	6.333	0.493 0	0.416 4	6.348	0.486 2	0.437 5
4	6.338	0.438 6	0.364 0	6.342	0.439 7	0.379 0	6.349	0.439 2	0.394 0	6.361	0.434 8	0.409 5
3	6.348	0.409 1	0.357 2	6.352	0.410 3	0.369 1	6.358	0.410 2	0.380 4	6.368	0.406 5	0.392 5
2	6.359	0.378 7	0.349 2	6.362	0.379 8	0.357 7	6.367	0.379 5	0.365 1	6.376	0.376 7	0.373 5
1	6.371	0.346 8	0.339 8	6.374	0.347 6	0.344 5	6.378	0.347 1	0.348 0	6.384	0.345 5	0.352 3
2/ 8	2.987	0.600 7	0.360 0	—	—	—	—	—	—	—	—	—
6	3.001	0.530 3	0.361 7	3.004	0.543 2	0.395 0	3.005	0.546 7	0.428 8	—	—	—
4	3.014	0.462 8	0.357 1	3.017	0.469 4	0.379 7	3.022	0.469 9	0.402 2	3.029	0.467 5	0.422 6
3	3.021	0.426 1	0.352 3	3.023	0.430 4	0.369 1	3.028	0.430 8	0.386 2	3.034	0.428 0	0.401 3
2	3.027	0.388 5	0.345 8	3.030	0.390 9	0.356 9	3.034	0.391 3	0.368 5	3.039	0.389 1	0.378 6
1	3.034	0.350 6	0.337 9	3.037	0.351 5	0.343 3	3.040	0.352 0	0.349 3	3.044	0.350 7	0.354 5
1/ 8	1.145	0.671 8	0.307 1	—	—	—	—	—	—	—	—	—
6	1.151	0.606 1	0.328 9	—	—	—	—	—	—	—	—	—
4	1.157	0.534 4	0.339 8	1.157	0.566 4	0.381 4	—	—	—	—	—	—
3	1.161	0.485 0	0.341 8	1.163	0.504 0	0.374 7	—	—	—	—	—	—
2	1.165	0.429 8	0.340 8	1.167	0.440 7	0.364 2	1.170	0.444 9	0.383 8	1.174	0.445 3	0.404 8
1	1.170	0.371 8	0.336 1	1.172	0.373 0	0.347 1	1.175	0.369 5	0.353 7	1.178	0.365 0	0.359 4

Annex Attached Table 1. (continued)

	2.5Y			5Y			7.5Y			10Y		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
9/20	—	—	—	76.45	0.480 0	0.511 9	—	—	—	—	—	—
18	—	—	—	76.49	0.475 1	0.508 1	76.68	0.463 1	0.522 0	76.85	0.450 5	0.535 3
16	—	—	—	76.55	0.467 8	0.501 6	76.69	0.456 1	0.514 3	76.84	0.444 1	0.526 5
14	—	—	—	76.61	0.456 9	0.491 8	76.71	0.446 7	0.504 2	76.82	0.435 6	0.515 1
12	76.31	0.456 1	0.458 7	76.62	0.443 0	0.477 9	76.72	0.434 0	0.489 0	76.81	0.424 0	0.498 2
10	76.50	0.436 2	0.444 1	76.64	0.426 0	0 460 2	76.72	0.418 3	0.469 6	76.80	0.410 0	0.477 0
8	76.54	0.415 4	0.427 1	76.65	0.407 5	0.440 5	76.73	0.401 1	0.448 0	76.79	0.394 7	0.454 0
6	76.59	0.391 8	0.407 0	76.67	0.386 3	0.417 1	76.73	0.381 4	0.422 4	76.78	0.376 3	0.425 8
4	76.63	0.367 1	0.384 8	76.69	0.363 4	0.391 1	76.73	0.360 3	0.394 5	76.76	0.356 9	0.396 6
3	76.65	0.354 4	0.372 6	76.70	0.351 9	0.377 3	76.73	0.349 7	0.380 2	76.75	0.347 2	0.381 8
2	76.67	0.341 2	0.359 3	76.70	0.339 9	0.362 5	76.73	0.338 5	0.364 9	76.74	0.336 8	0.366 0
1	76.70	0.327 3	0.344 9	76.71	0.327 0	0.346 7	76.72	0.326 3	0.347 6	76.73	0.325 5	0.348 6
8/20	56.48	0.510 5	0.488 5	—	—	—	—	—	—	—	—	—
18	56.77	0.502 7	0.486 1	56.68	0.484 5	0.507 2	56.71	0.470 3	0.522 6	56.80	0.455 8	0.537 7
16	57.20	0.493 2	0.482 8	56.95	0.477 7	0.502 8	56.93	0.464 4	0.517 5	56.99	0.450 7	0.531 5
14	57.39	0.481 3	0.475 4	57.39	0.466 8	0.495 8	57.29	0.454 8	0.509 6	57.30	0.442 3	0.521 6
12	57.42	0.465 7	0.464 2	57.54	0.453 3	0.484 1	57.62	0.442 1	0.497 1	57.70	0.430 5	0.507 5
10	57.45	0.445 8	0.449 0	57.55	0.435 7	0.466 8	57.63	0.426 0	0.478 0	57.69	0.416 5	0.486 1
8	57.48	0.422 9	0.431 2	57.57	0.415 0	0.446 0	57.63	0.407 7	0.454 9	57.69	0.399 5	0.460 6
6	57.52	0.397 6	0.410 4	57.59	0.391 6	0.421 4	57.64	0.386 3	0.427 3	57.68	0.380 2	0.431 6
4	57.56	0.370 0	0.386 0	57.61	0.366 3	0.393 6	57.64	0.363 3	0.397 2	57.67	0.359 1	0.399 6
3	57.58	0.356 5	0.373 6	57.61	0.354 1	0.379 2	57.64	0.351 9	0.382 1	57.66	0.348 7	0.383 9
2	57.60	0.342 8	0.360 4	57.62	0.341 4	0.363 9	57.64	0.339 9	0.366 2	57.65	0.337 8	0.367 5
1	57.61	0.328 3	0.345 8	57.62	0.327 9	0.347 3	57.64	0.326 9	0.348 8	57.64	0.326 0	0.349 5
7/16	41.20	0.504 4	0.484 8	41.03	0.487 6	0.504 6	40 99	0.472 9	0.521 4	41.03	0.458 0	0.537 6
14	41 80	0.491 7	0.480 8	41 48	0 477 3	0 498 6	41.35	0.463 8	0.514 4	41.33	0 450 2	0.529 3
12	41.82	0.478 0	0.471 1	41.91	0.464 3	0.490 2	41.85	0.451 5	0.504 7	41.77	0.439 1	0.517 0
10	41.85	0.458 9	0.457 4	41.92	0.448 5	0.475 4	41.99	0.437 1	0.488 9	42.05	0.425 7	0.499 8
8	41.87	0.434 7	0.438 6	41.94	0.425 9	0.453 7	41.99	0.416 8	0.464 4	42.04	0.407 2	0.472 0
6	41.90	0.407 8	0.416 3	41.96	0.400 9	0.428 9	42.00	0.394 1	0.435 7	42.04	0.386 0	0.440 1
4	41.93	0.377 5	0.390 5	41.97	0.372 9	0.399 2	42.00	0.368 6	0.403 4	42.03	0.363 2	0.406 2
3	41.95	0.361 8	0.377 0	41.98	0.358 6	0.383 1	42.00	0.355 3	0.386 0	42.02	0.351 2	0.388 0
2	41.97	0.345 7	0.362 6	41.99	0.343 9	0.366 0	42.00	0.341 5	0.367 9	42.02	0.338 8	0.369 1
1	41.99	0.329 4	0.346 7	41.99	0.328 7	0.348 1	42.00	0.327 3	0.348 9	42.01	0.326 0	0.349 5
6/14	28.76	0.505 4	0.483 5	28.56	0.491 0	0.503 3	28.45	0.476 3	0.521 1	28.23	0.459 8	0.538 7
12	29.17	0.489 7	0.476 8	29.07	0.475 4	0.495 0	28.93	0.461 9	0.510 9	28.91	0.447 1	0.525 8
10	29.18	0.473 7	0.465 6	29.24	0.460 9	0.483 9	29.30	0.447 6	0.499 3	29.31	0.433 5	0.511 8
8	29.20	0.450 5	0.448 5	29.25	0.440 7	0.465 3	29.30	0.429 8	0.478 5	29.34	0.417 5	0.488 1
6	29.23	0.420 4	0.425 9	29.27	0.413 5	0.438 9	29.30	0.405 2	0.448 6	29.33	0.395 0	0 454 1
4	29.25	0.385 2	0.396 8	29.28	0.380 3	0.405 8	29.31	0.375 2	0.410 9	29.33	0.368 5	0.414 1
3	29.27	0.367 8	0.381 8	29.29	0.364 0	0.388 3	29.31	0.360 2	0.391 8	29.32	0.355 2	0.393 9
2	29.28	0.350 1	0.365 7	29.30	0.347 6	0.369 8	29.31	0.344 9	0.372 0	29.32	0.341 6	0.373 2
1	29.29	0.331 8	0.348 3	29.30	0.330 6	0.350 2	29.31	0.329 2	0.351 3	29.31	0.327 5	0.351 8
5/12	18.94	0.507 4	0.481 8	18.83	0.493 8	0.501 3	18.68	0.477 6	0.519 9	18.58	0.459 4	0.538 6
10	19.18	0.487 7	0.472 3	19.22	0.474 1	0.491 6	19.12	0.460 7	0.508 5	19.14	0.444 3	0.523 9
8	19.19	0.466 7	0.457 8	19.23	0.455 4	0.474 7	19.27	0 442 0	0.490 6	19.30	0.427 3	0.502 5
6	19.21	0.437 5	0.436 5	19.24	0.429 1	0.450 8	19.27	0.418 4	0.462 7	19.29	0.405 5	0.470 1
4	19.23	0.397 7	0.404 9	19.25	0.392 0	0.415 4	19.27	0.385 3	0.421 9	19.29	0 376 4	0 426 1
3	19.24	0.376 7	0.387 1	19.26	0.372 0	0.395 0	19.27	0.367 2	0.399 2	19.29	0.360 3	0.401 6
2	19.25	0.355 4	0.368 5	19.27	0.351 8	0.373 6	19.27	0.348 8	0.375 8	19.28	0.343 9	0.376 8
1	19 26	0 334 0	0.349 1	19.27	0.331 9	0 351 6	19.27	0.330 5	0.352 2	19 28	0.327 8	0.352 3
4/10	11.53	0.511 3	0.480 5	—	—	—	—	—	—	—	—	—
8	11.65	0.484 0	0.466 8	11.67	0.471 2	0.485 3	11.70	0.455 6	0.503 3	11.70	0.439 3	0.519 6
6	11.66	0.453 1	0.445 4	11.68	0.443 4	0.461 4	11.70	0.430 9	0.475 4	11.72	0.416 5	0.486 4
4	11.67	0.414 3	0.416 2	11.69	0.406 9	0.427 6	11.70	0.397 9	0.436 3	11.71	0.386 6	0.441 6
3	11.68	0.390 6	0.397 5	11.69	0.384 5	0.405 7	11.70	0.377 5	0.411 3	11.71	0.368 3	0.413 9
2	11.69	0.365 2	0.376 4	11.69	0.360 7	0.381 3	11.70	0.355 7	0.384 2	11.71	0.349 1	0.385 0
1	11.69	0.338 9	0.353 6	11.70	0.336 3	0.355 6	11.70	0.333 8	0.356 4	11.71	0.330 2	0.356 2

Annex Attached Table 1. (continued)

	2.5Y			5Y			7.5Y			10Y		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
3/ 6	6.362	0.476 4	0.457 9	6.375	0.464 3	0.475 9	6.388	0.449 2	0.493 8	6.401	0.430 8	0.507 9
4	6.372	0.427 8	0.424 4	6.381	0.418 7	0.436 3	6.390	0.407 8	0.446 2	6.399	0.395 1	0.453 9
3	6.377	0.400 6	0.403 7	6.384	0.393 0	0.412 1	6.391	0.384 5	0.418 4	6.398	0.374 2	0.422 7
2	6.382	0.372 1	0.380 7	6.388	0.366 1	0.385 7	6.392	0.360 3	0.389 0	6.397	0.352 6	0.390 4
1	6.388	0.342 6	0.355 8	6.391	0.339 1	0.357 8	6.393	0.336 2	0.358 9	6.396	0.331 7	0.358 8
2/ 4	3.036	0.461 5	0.444 8	3.041	0.452 3	0.462 9	3.047	0.437 6	0.478 1	3.053	0.416 3	0.485 4
3	3.039	0.422 0	0.417 0	3.044	0.413 3	0.428 1	3.048	0.400 5	0.435 6	3.052	0.384 7	0.438 1
2	3.043	0.384 0	0.388 5	3.046	0.377 0	0.394 2	3.049	0.367 2	0.396 5	3.052	0.356 8	0.396 0
1	3.046	0.347 6	0.359 2	3.048	0.343 5	0.361 2	3.050	0.337 9	0.360 9	3.051	0.332 7	0.359 6
1/ 2	1.177	0.436 1	0.424 4	1.179	0.422 6	0.433 6	1.181	0.403 8	0.436 6	1.182	0.380 2	0.430 3
1	1.179	0.357 6	0.363 8	1.180	0.350 1	0.364 4	1.181	0.342 8	0.363 8	1.182	0.335 4	0.362 0

Annex Attached Table 1. (continued)

	2.5GY			5GY			7.5GY			10GY		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
9/18	77.04	0.431 1	0.554 4	77.25	0.405 9	0.574 0	77.35	0.354 6	0.597 5	77.19	0.299 2	0.582 8
16	77.02	0.424 7	0.542 8	77.17	0.401 2	0.559 1	77.25	0.353 8	0.572 0	77.23	0.304 6	0.553 2
14	76.99	0.417 2	0.529 1	77.14	0.395 2	0.539 0	77.21	0.351 7	0.541 9	77.23	0.309 0	0.523 1
12	76.95	0.407 4	0.509 4	77.10	0.387 7	0.515 5	77.22	0.349 2	0.513 5	77.23	0.312 2	0.494 0
10	76.92	0.395 1	0.484 2	77.04	0.378 8	0.487 9	77.22	0.345 3	0.483 9	77.22	0.314 4	0.467 6
8	76.89	0.382 3	0.458 5	76.99	0.368 7	0.459 7	77.15	0.340 6	0.452 9	77.25	0.315 3	0.438 6
6	76.85	0.367 1	0.428 5	76.92	0.357 2	0.429 0	77.05	0.335 3	0.423 3	77.15	0.315 6	0.413 9
4	76.81	0.351 0	0.398 3	76.85	0.344 7	0.398 1	76.93	0.328 5	0.392 0	76.98	0.315 6	0.384 3
3	76.78	0.342 8	0.382 8	76.81	0.337 9	0.382 4	76.87	0.325 2	0.377 6	76.91	0.315 1	0.371 4
2	76.75	0.334 0	0.366 3	76.77	0.330 3	0.365 9	76.81	0.321 7	0.362 9	76.83	0.314 3	0.358 5
1	76.73	0.324 1	0.348 6	76.73	0.322 0	0.348 3	76.74	0.317 7	0.347 0	76.74	0.313 5	0.344 7
8/24	—	—	—	—	—	—	—	—	—	58.65	0.271 3	0.689 2
22	—	—	—	—	—	—	—	—	—	58.51	0.278 7	0.662 4
20	—	—	—	56.96	0.409 7	0.588 0	57.78	0.354 0	0.628 1	58.39	0.286 7	0.632 5
18	57.03	0.435 0	0.557 6	57.32	0.407 1	0.581 5	57.90	0.353 5	0.611 2	58.33	0.294 4	0.599 8
16	57.18	0.430 1	0.550 2	57.48	0.402 6	0.568 0	57.97	0.352 3	0.585 7	58.32	0.300 6	0.566 7
14	57.43	0.423 0	0.538 3	57.65	0.397 4	0.551 8	58.07	0.350 6	0.556 2	58.36	0.305 9	0.534 6
12	57.82	0.411 5	0.519 3	57.95	0.388 5	0.526 7	58.13	0.347 8	0.523 1	58.27	0.310 1	0.503 7
10	57.80	0.399 4	0.494 5	57.90	0.379 0	0.496 4	58.05	0.344 3	0.489 4	58.17	0.312 6	0.472 2
8	57.77	0.384 5	0.464 2	57.85	0.368 4	0.464 2	57.97	0.339 9	0.456 6	58.06	0.314 4	0.441 1
6	57.74	0.368 9	0.433 5	57.80	0.357 2	0.432 5	57.89	0.334 0	0.425 1	57.96	0.315 3	0.414 5
4	57.71	0.351 4	0.400 4	57.74	0.344 3	0.399 2	57.81	0.327 6	0.393 6	57.85	0.315 1	0.385 9
3	57.69	0.343 2	0.384 5	57.71	0.337 6	0.383 2	57.76	0.324 6	0.378 5	57.79	0.314 6	0.372 6
2	57.67	0.334 6	0.367 9	57.68	0.330 3	0.366 8	57.71	0.321 3	0.363 1	57.73	0.314 0	0.359 0
1	57.64	0.324 7	0.349 8	57.64	0.322 1	0.348 9	57.65	0.317 5	0.346 8	57.65	0.313 4	0.344 7
7/22	—	—	—	—	—	—	—	—	—	42.83	0.267 6	0.694 2
20	—	—	—	—	—	—	—	—	—	42.74	0.276 5	0.662 3
18	—	—	—	—	—	—	41.97	0.351 3	0.628 2	42.68	0.285 8	0.625 9
16	41.13	0.435 8	0.558 5	41.60	0.404 8	0.580 9	42.23	0.350 3	0.605 2	42.63	0.294 0	0.591 9
14	41.47	0.428 9	0.548 2	41.75	0.399 7	0.565 2	42.27	0.349 1	0.576 4	42.58	0.301 2	0.555 3
12	41.88	0.418 0	0.531 5	42.05	0.391 2	0.542 3	42.37	0.346 5	0.540 8	42.50	0.306 5	0.520 1
10	42.13	0.405 7	0.509 7	42.22	0.382 0	0.512 8	42.34	0.343 5	0.504 7	42.42	0.310 5	0.485 0
8	42.11	0.390 1	0.477 0	42.18	0.370 5	0.476 4	42.27	0.339 3	0.466 9	42.34	0.313 2	0.451 3
6	42.09	0.372 4	0.441 9	42.14	0.357 8	0.440 0	42.21	0.334 0	0.431 2	42.26	0.314 4	0.418 9
4	42.06	0.354 2	0.406 8	42.09	0.344 5	0.404 8	42.14	0.327 6	0.397 5	42.17	0.314 3	0.389 6
3	42.05	0.344 6	0.388 4	42.07	0.337 6	0.386 9	42.10	0.324 3	0.381 1	42.12	0.314 0	0.374 9
2	42.03	0.334 6	0.369 3	42.04	0.330 2	0.368 5	42.06	0.320 8	0.364 5	42.07	0.313 6	0.360 0
1	42.01	0.324 1	0.349 6	42.01	0.322 1	0.349 2	42.02	0.317 1	0.347 3	42.02	0.313 2	0.344 8
6/20	—	—	—	—	—	—	—	—	—	29.98	0.260 4	0.704 8
18	—	—	—	—	—	—	—	—	—	29.95	0.271 1	0.668 0
16	—	—	—	—	—	—	29.35	0.345 6	0.632 3	29.90	0.282 2	0.627 8
14	28.58	0.435 1	0.559 7	29.12	0.401 4	0.581 6	29.63	0.345 0	0.604 4	29.86	0.291 8	0.589 2
12	29.03	0.424 6	0.544 2	29.26	0.394 7	0.560 8	29.60	0.344 6	0.566 9	29.72	0.300 3	0.545 7
10	29.37	0.412 1	0.524 6	29.47	0.385 1	0.533 0	29.58	0.342 9	0.528 3	29.64	0.306 3	0.506 1
8	29.40	0.397 9	0.496 1	29.46	0.374 7	0.496 6	29.53	0.339 8	0.487 3	29.58	0.310 3	0.468 6
6	29.38	0.378 9	0.456 6	29.42	0.361 3	0.454 3	29.47	0.334 6	0.444 0	29.51	0.312 6	0.430 5
4	29.36	0.357 7	0.415 1	29.38	0.346 7	0.412 6	29.42	0.328 2	0.404 8	29.44	0.313 2	0.395 5
3	29.34	0.347 0	0.394 2	29.36	0.338 8	0.392 2	29.39	0.324 7	0.386 3	29.41	0.313 1	0.379 1
2	29.33	0.335 9	0.373 0	29.34	0.330 5	0.371 8	29.36	0.321 0	0.367 9	29.37	0.313 0	0.362 8
1	29.32	0.324 5	0.351 5	29.32	0.321 8	0.350 9	29.32	0.317 1	0.349 0	29.33	0.312 9	0.346 2
5/18	—	—	—	—	—	—	—	—	—	19.80	0.251 4	0.721 4
16	—	—	—	—	—	—	—	—	—	19.77	0.264 7	0.676 7
14	—	—	—	—	—	—	19.34	0.338 5	0.637 9	19.74	0.278 2	0.629 4
12	18.84	0.432 7	0.560 8	19.24	0.397 9	0.583 5	19.60	0.339 6	0.601 7	19.66	0.289 4	0.584 6
10	19.25	0.419 1	0.541 0	19.36	0.388 9	0.554 0	19.52	0.340 8	0.557 0	19.53	0.299 7	0.533 9
8	19.34	0.405 3	0.513 3	19.39	0.378 1	0.517 0	19.44	0.338 6	0.507 4	19.48	0.306 2	0.487 8
6	19.33	0.386 2	0.473 4	19.36	0.364 8	0.471 3	19.40	0.334 4	0.459 8	19.43	0.310 3	0.443 0
4	19.31	0.362 3	0.425 3	19.33	0.348 5	0.421 3	19.36	0.327 9	0.412 0	19.38	0.311 8	0.401 4
3	19.30	0.349 6	0.400 5	19.32	0.339 6	0.397 2	19.34	0.324 2	0.390 0	19.35	0.312 3	0.382 3
2	19.29	0.336 9	0.375 9	19.30	0.330 6	0.373 8	19.31	0.320 5	0.369 0	19.32	0.312 7	0.364 0
1	19.28	0.324 4	0.352 0	19.28	0.321 5	0.351 1	19.29	0.316 6	0.348 7	19.29	0.312 9	0.346 3

Annex Attached Table 1. (continued)

	2.5GY			5GY			7.5GY			10GY		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
4/16	—	—	—	—	—	—	—	—	—	12.10	0.240 2	0.738 0
14	—	—	—	—	—	—	—	—	—	12.06	0.253 4	0.692 4
12	—	—	—	—	—	—	11.70	0.331 1	0.650 4	12.01	0.270 0	0.637 0
10	—	—	—	11.64	0.395 3	0.588 0	11.92	0.333 8	0.598 7	11.93	0.286 3	0.577 0
8	11.76	0.413 1	0.535 3	11.80	0.382 3	0.544 9	11.83	0.336 2	0.543 0	11.86	0.298 1	0.520 4
6	11.74	0.394 2	0.493 5	11.77	0.369 4	0.494 1	11.80	0.333 7	0.484 8	11.82	0.305 6	0.467 5
4	11.73	0.370 3	0.443 2	11.75	0.353 4	0.439 5	11.77	0.328 1	0.428 1	11.78	0.310 2	0.415 1
3	11.73	0.355 2	0.413 2	11.74	0.343 3	0.409 8	11.75	0.324 2	0.400 0	11.76	0.311 6	0.390 9
2	11.72	0.339 7	0.382 8	11.72	0.332 7	0.380 3	11.73	0.320 1	0.373 4	11.74	0.312 5	0.368 3
1	11.71	0.325 1	0.354 1	11.71	0.322 3	0.352 9	11.71	0.316 1	0.349 4	11.72	0.312 9	0.347 6
3/14	—	—	—	—	—	—	—	—	—	6.677	0.225 8	0.745 0
12	—	—	—	—	—	—	—	—	—	6.585	0.247 3	0.677 6
10	—	—	—	—	—	—	6.463	0.321 4	0.650 1	6.539	0.267 2	0.611 9
8	—	—	—	6.419	0.388 0	0.587 6	6.492	0.329 0	0.577 8	6.491	0.285 5	0.546 2
6	6.418	0.403 2	0.517 3	6.436	0.371 6	0.518 7	6.455	0.330 7	0.506 8	6.469	0.297 5	0.484 1
4	6.412	0.376 1	0.458 0	6.423	0.354 5	0.453 7	6.436	0.326 5	0.441 1	6.445	0.305 2	0.425 7
3	6.408	0.359 5	0.423 5	6.416	0.344 1	0.419 0	6.425	0.323 1	0.408 2	6.431	0.308 1	0.397 5
2	6.403	0.342 5	0.388 8	6.408	0.333 2	0.385 4	6.413	0.319 4	0.377 5	6.417	0.310 3	0.371 2
1	6.398	0.326 4	0.356 5	6.400	0.322 5	0.354 8	6.402	0.315 8	0.350 5	6.403	0.311 8	0.348 1
2/12	—	—	—	—	—	—	—	—	—	3.266	0.190 0	0.780 5
10	—	—	—	—	—	—	—	—	—	3.162	0.225 6	0.689 1
8	—	—	—	—	—	—	3.095	0.310 6	0.656 4	3.115	0.258 4	0.593 4
6	—	—	—	3.084	0.378 5	0.580 1	3.088	0.322 2	0.546 4	3.095	0.282 8	0.509 3
4	3.061	0.386 0	0.483 4	3.068	0.356 5	0.475 0	3.075	0.323 7	0.457 7	3.081	0.298 0	0.437 6
3	3.058	0.363 2	0.434 5	3.063	0.344 2	0.428 0	3.069	0.321 2	0.415 5	3.073	0.303 8	0.402 8
2	3.055	0.343 3	0.392 2	3.058	0.332 1	0.386 8	3.062	0.317 8	0.378 2	3.064	0.308 2	0.371 6
1	3.053	0.326 5	0.356 9	3.054	0.321 3	0.353 2	3.055	0.314 6	0.348 5	3.057	0.311 2	0.346 3
1/ 6	—	—	—	—	—	—	—	—	—	1.223	0.218 6	0.649 6
4	—	—	—	1.188	0.371 5	0.599 6	1.202	0.308 8	0.548 9	1.201	0.269 7	0.503 7
3	—	—	—	1.195	0.352 0	0.492 0	1.195	0.313 9	0.462 7	1.197	0.288 1	0.439 5
2	1.186	0.354 2	0.419 9	1.188	0.336 3	0.410 3	1.190	0.316 0	0.397 3	1.192	0.301 2	0.386 3
1	1.183	0.329 1	0.359 3	1.185	0.323 2	0.356 6	1.186	0.315 6	0.352 7	1.188	0.310 0	0.350 7

Annex Attached Table 1. (continued)

	2.5G			5G			7.5G			10G		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
9/16	77.11	0.261 1	0.507 1	—	—	—	—	—	—	—	—	—
14	77.15	0.269 5	0.483 9	—	—	—	—	—	—	—	—	—
12	77.19	0.277 5	0.461 5	77.13	0.252 3	0.429 8	77.10	0.241 7	0.413 0	77.08	0.232 5	0.394 6
10	77.22	0.284 6	0.440 7	77.18	0.263 9	0.414 5	77.15	0.254 7	0.400 4	77.13	0.246 0	0.385 5
8	77.24	0.291 3	0.419 1	77.22	0.273 9	0.399 9	77.19	0.265 8	0.388 6	77.17	0.258 1	0.376 9
6	77.20	0.297 2	0.398 5	77.23	0.284 1	0.384 2	77.24	0.277 3	0.375 4	77.21	0.271 4	0.366 2
4	77.02	0.303 1	0.374 3	77.04	0.294 7	0.365 9	77.05	0.289 7	0.360 2	77.05	0.285 6	0.354 4
3	76.94	0.305 5	0.363 8	76.95	0.299 3	0.357 6	76.96	0.295 3	0.353 1	76.96	0.292 1	0.348 8
2	76.85	0.307 8	0.353 3	76.86	0.303 7	0.349 1	76.86	0.300 8	0.345 8	76.86	0.298 6	0.342 8
1	76.75	0.310 1	0.342 0	76.76	0.308 2	0.339 8	76.76	0.306 5	0.337 9	76.75	0.305 4	0.336 4
8/24	58.68	0.206 6	0.613 7	—	—	—	—	—	—	—	—	—
22	58.67	0.219 4	0.591 0	58 65	0.181 2	0.507 8	—	—	—	—	—	—
20	58.64	0.231 2	0.567 9	58.64	0.194 5	0.495 2	58.64	0.183 8	0.464 5	58.64	0.173 0	0.431 8
18	58.61	0.242 7	0.543 2	58.61	0 209 1	0.480 7	58.61	0.197 2	0.453 8	58.61	0.186 1	0.426 0
16	58.55	0.254 2	0.517 4	58.57	0 223 0	0.465 9	58.57	0.211 3	0.442 1	58.57	0.200 7	0.416 9
14	58.45	0.264 5	0.491 5	58.49	0.236 0	0.450 6	58.50	0.224 9	0.429 1	58.50	0.214 5	0.407 6
12	58.35	0.273 1	0.469 2	58.39	0.248 4	0.434 7	58.39	0.237 8	0.416 4	58.39	0.228 2	0.397 8
10	58.24	0.282 3	0.444 1	58.27	0.261 2	0.417 9	58.27	0.251 6	0.402 5	58.27	0.243 3	0.387 1
8	58.12	0.289 6	0.420 6	58 15	0.272 6	0.401 4	58.15	0.264 4	0.388 6	58.15	0.257 1	0.376 6
6	58.01	0.295 8	0.399 1	58.03	0 283 0	0.384 7	58.03	0.276 4	0.375 5	58.03	0.270 4	0.366 1
4	57.87	0.302 2	0.375 1	57 89	0.293 8	0 366 3	57.89	0.288 9	0.360 5	57.89	0.284 4	0.354 6
3	57.81	0.304 8	0 364 4	57 82	0.298 4	0 357 9	57.82	0.294 6	0.353 4	57.82	0.291 0	0.348 8
2	57.74	0.307 3	0 353 7	57.75	0.302 9	0.349 4	57.75	0.300 1	0.346 1	57.75	0.297 8	0.342 9
1	57.66	0.309 8	0 342 2	57 67	0.307 6	0.339 9	57.67	0.306 2	0.338 2	57.66	0.305 0	0.336 4
7/26	43 64	0.167 6	0 665 1	43 55	0 140 1	0 548 0	43.55	0.131 1	0 503 8	—	—	—
24	43.49	0.185 5	0 638 1	43 51	0 152 0	0 536 7	43.50	0 141 8	0.495 7	43.52	0.131 6	0.456 1
22	43.32	0.200 6	0 614 0	43 42	0.165 3	0.524 3	43.45	0.153 7	0.486 6	43.46	0.143 6	0.449 7
20	43.12	0.215 7	0.587 2	43.30	0.179 6	0.510 5	43.33	0.168 3	0.475 6	43.36	0.158 6	0.442 0
18	42.92	0.230 4	0.559 7	43 12	0.195 6	0.494 3	43.17	0.183 4	0.463 5	43.22	0.172 9	0.433 4
16	42.76	0.242 6	0.533 3	42.93	0.210 0	0.478 4	42.99	0.197 5	0.451 3	43.03	0.187 6	0.424 2
14	42.65	0.254 9	0.506 4	42 72	0.225 2	0 461 2	42.76	0.213 3	0.437 3	42.81	0.202 9	0.413 8
12	42.57	0.265 8	0.480 5	42.59	0.240 9	0.442 5	42.60	0.229 1	0.422 4	42.60	0.219 3	0.402 5
10	42.48	0.276 7	0.453 6	42.50	0.255 1	0.424 2	42.51	0.244 5	0.407 4	42.51	0.235 4	0.391 3
8	42.39	0.285 9	0.427 0	42.40	0.268 9	0 405 2	42.41	0.259 9	0.391 9	42.41	0.251 9	0.379 3
6	42.29	0.293 8	0.401 3	42 30	0.280 8	0.386 7	42.31	0.273 7	0.377 1	42.31	0.267 2	0.367 7
4	42.19	0.300 4	0 378 2	42 20	0 291 5	0.368 9	42.21	0.286 4	0.362 5	42.21	0.281 8	0.355 9
3	42.14	0.303 5	0.366 6	42 15	0 296 8	0.359 7	42.15	0.292 8	0.354 8	42.15	0.289 1	0.349 7
2	42.09	0.306 6	0 354 7	42 09	0.302 1	0.350 1	42.09	0.299 2	0.346 9	42.09	0.296 5	0.343 3
1	42.02	0.309 7	0.342 2	42.03	0 307 4	0.339 9	42.03	0.305 9	0.338 3	42.03	0.304 4	0.336 5
6/28	31.09	0.115 0	0 720 2	30 81	0.092 2	0.588 2	30.74	0.087 1	0.533 5	—	—	—
26	31.00	0.133 5	0.697 4	30 80	0 108 4	0.574 8	30.73	0.101 7	0.522 3	30.69	0.094 8	0.473 4
24	30.87	0.152 2	0.672 5	30 76	0.125 0	0 559 8	30.72	0.116 0	0.511 4	30.67	0.107 3	0.466 8
22	30.68	0.172 0	0 645 0	30 68	0 142 4	0 544 4	30.66	0.132 0	0.500 0	30.64	0.122 7	0.459 0
20	30.47	0.190 0	0 617 3	30 55	0.159 7	0 528 1	30.57	0 147 7	0.488 2	30.57	0.137 6	0 451 5
18	30.25	0.207 8	0 587 7	30.39	0.177 2	0 511 1	30.42	0.164 4	0.475 3	30.45	0.154 3	0.442 2
16	30.03	0.225 4	0 556 8	30 19	0 194 7	0 493 1	30.24	0.182 2	0.461 0	30.28	0.171 4	0.432 0
14	29 85	0.240 5	0 526 8	29 98	0 211 8	0 474 2	30.03	0 199 2	0 446 3	30 07	0 188 8	0 421 1
12	29.75	0.255 7	0.495 1	29.77	0 228 4	0 455 1	29.81	0.216 5	0.431 0	29.86	0 205 6	0.409 5
10	29.69	0.267 9	0.467 1	29.70	0.246 1	0 433 8	29.70	0.234 8	0.414 3	29.71	0.224 7	0.396 5
8	29.61	0.279 4	0.438 2	29.63	0.261 2	0 414 3	29.63	0.251 2	0.398 7	29.63	0.242 4	0.384 1
6	29.54	0.289 4	0.410 5	29.55	0.275 3	0 394 3	29.56	0.266 9	0.382 4	29.55	0.259 9	0.371 2
4	29.46	0.297 7	0.383 4	29.47	0 287 9	0 373 8	29.48	0.281 9	0.366 7	29.48	0 276 2	0.358 9
3	29.42	0.301 8	0.370 3	29.43	0 294 3	0 363 0	29.43	0.289 9	0.357 6	29.43	0.285 4	0.351 7
2	29.38	0.305 7	0.357 1	29.38	0.300 7	0 351 8	29.38	0.297 7	0.348 1	29.38	0.294 9	0.344 0
1	29.33	0.309 5	0.343 5	29.33	0.306 9	0.340 5	29.33	0.305 4	0.338 4	29.33	0.304 2	0.336 3

Annex Attached Table 1. (continued)

	2.5G			5G			7.5G			10G		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
5/28	20.69	0.080 3	0.745 1	20.20	0.061 4	0.606 7	20.01	0.058 6	0.541 3	19.87	0.056 9	0.478 0
26	20.65	0.099 1	0.724 9	20.25	0.078 3	0.594 1	20.08	0.072 7	0.532 5	19.92	0.068 5	0.473 7
24	20.56	0.117 9	0.703 1	20.27	0.094 7	0.581 7	20.14	0.087 2	0.523 9	19.99	0.080 4	0.468 8
22	20.46	0.136 2	0.680 3	20.26	0.113 3	0.566 0	20.15	0.104 0	0.513 1	20.04	0.094 9	0.462 9
20	20.33	0.155 8	0.653 3	20.21	0.130 4	0.551 9	20.15	0.120 0	0.502 3	20.07	0.110 9	0.456 6
18	20.15	0.175 9	0.624 1	20.15	0.147 3	0.536 9	20.11	0.135 8	0.491 1	20.06	0.126 3	0.449 7
16	19.96	0.198 0	0.590 6	20.04	0.167 8	0.517 3	20.02	0.155 7	0.476 4	20.01	0.145 6	0.440 2
14	19.78	0.218 7	0.555 5	19.88	0.189 6	0.495 6	19.90	0.176 3	0.461 0	19.90	0.166 0	0.429 3
12	19.64	0.236 4	0.521 1	19.73	0.209 1	0.475 1	19.76	0.195 4	0.445 7	19.77	0.184 4	0.418 6
10	19.56	0.255 0	0.484 6	19.57	0.232 1	0.449 1	19.58	0.219 5	0.425 2	19.59	0.209 2	0.403 0
8	19.51	0.270 2	0.452 4	19.52	0.250 8	0.426 3	19.52	0.239 4	0.407 8	19.52	0.229 8	0.389 7
6	19.45	0.284 1	0.418 8	19.46	0.269 3	0.401 1	19.46	0.260 3	0.387 9	19.46	0.252 6	0.374 4
4	19.39	0.295 2	0.387 5	19.40	0.285 1	0.377 2	19.40	0.278 6	0.369 1	19.40	0.272 3	0.360 3
3	19.36	0.300 1	0.372 6	19.36	0.292 5	0.365 1	19.37	0.287 6	0.359 3	19.37	0.282 7	0.352 6
2	19.33	0.304 8	0.358 0	19.33	0.299 6	0.352 8	19.33	0.296 4	0.349 2	19.33	0.292 9	0.344 8
1	19.29	0.309 0	0.343 6	19.29	0.306 4	0.340 8	19.29	0.304 8	0.339 2	19.29	0.303 0	0.336 9
4/26	12.53	0.053 0	0.754 8	12.11	0.040 3	0.613 8	11.93	0.038 5	0.539 6	11.75	0.039 0	0.467 8
24	12.53	0.075 6	0.733 1	12.17	0.060 5	0.600 6	12.02	0.057 0	0.530 9	11.85	0.054 2	0.463 8
22	12.50	0.099 8	0.708 3	12.21	0.082 8	0.585 4	12.08	0.075 7	0.521 4	11.94	0.068 9	0.460 1
20	12.44	0.121 4	0.683 3	12.24	0.100 3	0.572 6	12.12	0.091 3	0.512 7	12.00	0.083 6	0.456 1
18	12.37	0.142 5	0.657 2	12.23	0.117 2	0.559 0	12.14	0.107 1	0.503 4	12.05	0.099 2	0.451 4
16	12.25	0.165 8	0.625 7	12.21	0.138 5	0.540 8	12.15	0.127 8	0.490 1	12.08	0.119 8	0.443 6
14	12.14	0.188 4	0.592 7	12.15	0.161 0	0.520 6	12.12	0.148 5	0.475 9	12.09	0.138 5	0.436 4
12	12.03	0.210 4	0.557 1	12.07	0.182 7	0.499 0	12.07	0.169 3	0.461 1	12.05	0.159 1	0.426 4
10	11.93	0.233 6	0.515 0	11.96	0.210 3	0.470 2	11.97	0.198 0	0.439 9	11.97	0.186 9	0.411 9
8	11.87	0.254 8	0.474 2	11.88	0.235 2	0.442 6	11.88	0.222 8	0.419 1	11.88	0.212 2	0.397 3
6	11.83	0.273 0	0.436 1	11.84	0.258 0	0.414 7	11.84	0.246 9	0.398 2	11.84	0.237 7	0.381 9
4	11.79	0.289 7	0.396 4	11.79	0.278 8	0.385 1	11.79	0.271 1	0.375 2	11.80	0.263 8	0.365 0
3	11.77	0.296 7	0.378 0	11.77	0.288 6	0.370 1	11.77	0.282 7	0.363 1	11.77	0.277 0	0.355 9
2	11.74	0.302 9	0.360 6	11.74	0.297 6	0.355 5	11.74	0.293 7	0.351 0	11.75	0.289 8	0.346 7
1	11.72	0.308 2	0.344 3	11.72	0.305 7	0.341 7	11.72	0.303 8	0.339 5	11.72	0.301 9	0.337 7
3/22	6.813	0.038 8	0.750 5	6.562	0.033 3	0.610 7	6.421	0.032 4	0.530 4	6.263	0.032 5	0.452 0
20	6.812	0.071 0	0.720 9	6.605	0.060 9	0.593 9	6.493	0.055 7	0.521 7	6.372	0.051 8	0.450 5
18	6.802	0.103 3	0.688 5	6.640	0.086 9	0.577 0	6.544	0.078 5	0.511 5	6.452	0.070 6	0.448 2
16	6.756	0.132 1	0.655 7	6.647	0.110 5	0.559 2	6.582	0.101 0	0.499 8	6.500	0.091 3	0.443 8
14	6.695	0.160 3	0.620 2	6.644	0.136 8	0.538 4	6.595	0.125 0	0.485 7	6.546	0.115 0	0.437 2
12	6.614	0.188 0	0.579 2	6.610	0.164 6	0.513 3	6.597	0.150 5	0.469 8	6.567	0.140 1	0.428 4
10	6.549	0.215 0	0.536 0	6.561	0.192 3	0.485 9	6.559	0.179 1	0.449 6	6.551	0.168 1	0.416 1
8	6.499	0.242 0	0.489 7	6.509	0.221 9	0.454 6	6.513	0.208 2	0.427 6	6.514	0.196 6	0.402 0
6	6.477	0.263 4	0.449 0	6.480	0.246 7	0.425 8	6.481	0.234 5	0.406 6	6.481	0.224 1	0.386 9
4	6.450	0.283 9	0.406 0	6.453	0.271 6	0.393 1	6.454	0.262 4	0.382 1	6.455	0.253 2	0.369 4
3	6.435	0.293 2	0.384 4	6.437	0.283 8	0.375 2	6.438	0.276 9	0.367 7	6.439	0.269 8	0.358 8
2	6.419	0.301 4	0.363 8	6.420	0.295 1	0.357 9	6.421	0.290 7	0.353 2	6.422	0.286 1	0.347 9
1	6.404	0.308 0	0.345 1	6.405	0.305 0	0.342 2	6.405	0.302 9	0.339 9	6.405	0.300 8	0.337 8
2/16	3.235	0.032 4	0.739 0	3.106	0.027 1	0.605 3	3.024	0.027 0	0.522 0	2.928	0.028 1	0.436 7
14	3.236	0.080 7	0.696 1	3.142	0.067 6	0.583 3	3.090	0.062 0	0.511 4	3.029	0.059 0	0.438 2
12	3.219	0.128 8	0.645 2	3.165	0.110 7	0.553 9	3.129	0.101 0	0.493 7	3.091	0.092 4	0.434 5
10	3.165	0.175 3	0.585 1	3.161	0.154 7	0.517 2	3.145	0.143 2	0.470 1	3.124	0.131 2	0.424 5
8	3.121	0.217 5	0.519 5	3.126	0.196 8	0.476 0	3.128	0.183 4	0.443 1	3.124	0.169 9	0.409 9
6	3.099	0.248 1	0.467 2	3.100	0.231 1	0.439 5	3.101	0.219 6	0.415 5	3.101	0.209 1	0.391 5
4	3.083	0.276 3	0.414 6	3.084	0.264 2	0.399 9	3.084	0.254 4	0.386 4	3.085	0.244 7	0.372 1
3	3.074	0.288 7	0.388 6	3.075	0.279 6	0.378 9	3.076	0.272 0	0.370 1	3.076	0.264 5	0.360 3
2	3.065	0.299 2	0.364 7	3.066	0.293 3	0.359 2	3.066	0.288 4	0.354 3	3.067	0.283 6	0.348 5
1	3.057	0.307 4	0.344 4	3.058	0.304 6	0.342 1	3.058	0.302 4	0.340 3	3.058	0.300 1	0.337 8
1/ 8	1.247	0.060 9	0.698 0	1.210	0.054 9	0.583 3	1.187	0.052 1	0.507 0	1.155	0.050 5	0.424 8
6	1.230	0.169 4	0.578 7	1.226	0.145 6	0.519 0	1.218	0.133 4	0.469 9	1.209	0.124 0	0.420 4
4	1.203	0.244 4	0.464 7	1.206	0.228 3	0.439 0	1.206	0.215 5	0.414 3	1.206	0.203 7	0.390 1
3	1.197	0.271 5	0.417 2	1.198	0.259 6	0.402 6	1.198	0.249 0	0.387 5	1.199	0.239 2	0.372 7
2	1.192	0.291 8	0.378 0	1.193	0.284 2	0.371 3	1.193	0.276 8	0.363 6	1.193	0.270 0	0.356 1
1	1.188	0.305 4	0.348 3	1.188	0.301 9	0.346 0	1.188	0.298 2	0.343 1	1.188	0.294 9	0.340 2

Annex Attached Table 1. (continued)

	2.5BG			5BG			7.5BG			10BG		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
9/10	77.11	0.238 6	0.372 4	77.08	0.230 6	0.356 4	77.05	0.222 1	0.338 7	—	—	—
8	77.14	0.251 7	0.366 0	77.12	0.244 6	0.353 3	77.08	0.237 1	0.338 2	—	—	—
6	77.19	0.266 4	0 358 2	77.15	0.261 2	0.348 8	77.10	0.255 7	0.337 1	77.06	0.251 6	0.327 0
4	77.05	0.282 2	0.349 2	77.05	0.278 5	0.343 1	77.05	0.274 6	0.335 3	77.06	0.271 9	0.328 5
3	76.96	0.289 5	0 344 9	76.96	0.286 8	0.340 2	76.96	0.283 9	0.334 0	76.97	0.282 5	0.329 3
2	76.87	0.296 8	0.340 3	76.87	0.295 2	0.336 9	76.87	0.293 3	0.332 6	76.87	0.293 0	0.329 7
1	76.76	0.304 5	0.335 2	76.77	0.303 8	0.333 3	76.78	0.303 0	0.331 0	76.78	0.303 2	0.329 9
8/18	58.62	0.175 6	0.396 1	—	—	—	—	—	—	—	—	—
16	58.56	0.191 2	0.391 3	58.57	0.181 2	0.363 6	58.60	0.172 0	0.335 7	—	—	—
14	58.48	0.205 6	0 385 6	58 48	0.195 8	0.361 0	58 49	0.186 9	0.336 0	58.52	0.178 9	0.311 9
12	58.38	0.219 8	0 379 9	58.37	0.210 4	0.358 3	58.38	0.201 4	0.336 1	58.40	0.194 1	0.315 3
10	58.26	0.235 7	0.372 9	58 26	0.227 0	0.354 7	58.26	0.219 1	0.336 1	58.27	0.212 7	0.319 0
8	58.15	0.250 8	0 365 6	58 14	0.242 8	0.351 0	58.14	0.236 2	0.335 6	58.15	0.231 3	0.322 1
6	58 02	0.265 9	0 357 9	58 02	0.260 1	0.346 9	58 02	0.253 9	0.335 0	58.02	0.250 4	0.325 1
4	57 89	0.280 7	0.349 5	57 89	0.276 9	0.342 2	57.89	0.273 6	0.334 5	57.89	0.270 5	0.327 6
3	57 83	0.288 3	0 345 1	57 82	0.285 3	0.339 6	57.82	0.282 9	0.333 5	57.83	0.281 0	0.328 4
2	57.75	0.296 1	0.340 4	57.75	0.294 1	0.336 5	57.75	0.292 2	0.332 1	57.76	0.291 7	0.329 1
1	57.67	0.304 3	0.335 2	57 68	0.303 1	0.333 2	57.68	0.302 1	0.330 6	57.69	0.302 3	0.329 4
7/22	43.49	0.133 8	0 406 1	—	—	—	—	—	—	—	—	—
20	43.40	0.148 9	0.403 6	43.45	0.138 0	0.362 1	—	—	—	—	—	—
18	43.28	0.162 3	0.399 7	43.34	0.151 3	0.362 5	43.40	0.142 4	0.329 1	—	—	—
16	43 07	0.178 5	0 393 9	43 13	0.167 3	0.360 6	43.19	0.158 2	0.330 8	43.26	0.148 5	0 297 5
14	42.85	0.193 0	0 388 2	42 86	0.183 7	0.358 0	42.88	0.175 1	0.332 0	42.82	0.167 0	0.301 7
12	42 59	0.210 2	0 380 9	42 59	0.199 8	0.355 4	42.58	0.191 6	0 332 2	42.59	0.184 3	0 306 4
10	42 50	0.226 7	0 374 2	42.50	0.216 8	0.352 9	42.50	0.209 9	0.333 2	42.49	0.204 1	0 312 2
8	42 41	0.244 6	0 366 7	42 40	0.236 2	0.349 5	42 40	0.230 1	0.333 8	42.40	0.224 5	0 317 4
6	42 30	0.261 9	0 358 2	42 30	0.255 5	0.345 5	42.30	0.250 4	0.333 9	42.30	0.246 2	0 322 2
4	42 20	0.278 0	0 349 9	42 21	0.272 8	0.341 5	42.21	0.268 8	0.333 6	42.21	0.266 0	0 325 6
3	42.15	0.286 2	0.345 4	42.15	0.282 2	0.339 1	42 15	0.279 2	0.333 0	42.15	0.277 3	0 327 0
2	42.09	0.294 8	0 340 6	42 10	0.291 9	0.336 3	42 10	0.290 0	0.332 1	42.10	0.289 2	0 328 2
1	42.03	0.303 6	0.335 2	42 04	0.302 1	0.333 1	42.04	0.301 3	0.330 9	42.04	0.301 1	0 329 0
6/22	30.61	0.111 9	0.407 3	—	—	—	—	—	—	—	—	—
20	30.57	0.126 4	0.404 9	30.55	0.116 3	0.356 0	—	—	—	—	—	—
18	30.49	0.142 1	0 401 4	30.50	0.131 7	0.357 1	30 50	0.123 9	0.320 3	30.49	0.117 1	0 278 4
16	30.33	0.159 3	0 396 5	30.37	0.148 4	0.356 6	30 39	0.140 0	0.323 7	30.40	0.132 7	0 286 4
14	30 12	0.177 4	0 390 2	30.16	0.165 7	0.355 0	30.16	0.158 0	0.325 8	30.13	0.151 2	0 292 8
12	29 89	0.195 2	0 383 1	29.91	0.184 3	0.352 6	29.90	0.176 1	0.326 8	29.82	0.169 7	0 298 0
10	29 70	0.215 0	0 375 5	29.69	0.204 0	0.350 1	29.69	0.196 4	0.328 1	29.69	0.191 3	0 305 0
8	29.63	0.233 7	0 368 5	29.62	0.224 3	0.347 5	29.62	0.217 8	0.330 2	29.62	0.212 4	0 311 3
6	29.55	0.253 5	0 360 3	29.55	0.245 2	0.344 6	29 55	0.239 6	0.331 1	29.55	0.234 8	0 317 1
4	29 48	0.271 6	0.351 6	29.47	0.266 3	0.341 0	29.47	0.262 0	0.331 8	29.47	0.259 5	0.322 6
3	29 43	0.281 8	0 346 3	29.43	0.277 7	0.338 6	29.43	0.274 4	0.331 6	29.43	0.272 6	0 325 1
2	29 38	0.292 2	0 340 6	29 38	0.289 3	0.335 8	29 38	0.287 1	0.331 2	29 38	0.285 9	0 327 2
1	29 33	0.302 7	0 334 8	29.34	0.301 1	0.332 7	29 34	0.299 9	0 330 4	29.34	0.299 4	0 328 7
5/24	19 81	0.073 0	0 403 4	—	—	—	—	—	—	—	—	—
22	19 87	0.085 2	0 401 7	19.69	0.077 0	0.337 6	—	—	—	—	—	—
20	19.94	0.099 4	0 400 7	19.76	0.089 4	0.339 7	—	—	—	—	—	—
18	19 98	0.115 3	0 399 0	19.84	0.103 4	0.342 6	19.70	0.097 0	0.298 5	—	—	—
16	19 97	0.133 6	0.396 1	19.91	0.122 9	0.346 5	19 83	0.115 2	0.306 9	19.70	0.109 2	0.265 4
14	19.89	0.154 9	0 391 6	19.87	0.143 7	0.348 2	19 84	0.135 2	0.313 2	19.80	0.129 4	0.277 1
12	19 79	0.172 8	0 386 7	19.78	0.160 7	0.347 9	19 76	0.153 0	0.317 1	19.73	0.147 7	0.284 8
10	19 62	0.197 8	0 378 7	19.62	0.184 9	0.346 3	19.61	0.177 5	0.321 2	19.57	0.171 5	0.293 3
8	19 52	0.220 8	0.370 5	19.51	0.210 4	0.344 9	19.51	0.203 5	0.325 0	19.51	0.197 5	0.302 6
6	19.45	0.245 6	0.361 0	19.45	0.237 0	0.342 9	19.45	0.230 2	0.328 4	19.45	0.224 5	0.311 0
4	19 40	0.267 2	0.351 8	19.39	0.260 6	0.339 6	19.39	0.256 5	0.330 0	19.39	0.252 8	0.319 0
3	19 36	0.278 6	0.346 5	19.36	0.273 1	0.337 4	19 36	0.269 7	0.330 2	19.36	0.267 1	0.322 4
2	19 33	0.290 0	0.340 9	19.33	0.286 2	0.335 0	19.33	0.283 3	0.330 2	19.33	0.281 8	0.325 2
1	19.30	0.301 4	0.335 1	19.30	0.299 4	0.332 3	19.30	0.297 6	0.329 8	19.30	0.296 9	0.327 6

Annex Attached Table 1. (continued)

	2.5BG			5BG			7.5BG			10BG		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
4/24	11.64	0.049 8	0.392 0	—	—	—	—	—	—	—	—	—
22	11.73	0.062 4	0.391 9	—	—	—	—	—	—	—	—	—
20	11.82	0.075 6	0.391 7	11.57	0.066 4	0.317 5	—	—	—	—	—	—
18	11.91	0.090 2	0.391 2	11.69	0.081 7	0.322 3	11.52	0.075 8	0.275 1	—	—	—
16	11.98	0.108 9	0.389 4	11.82	0.098 0	0.328 0	11.66	0.091 2	0.282 2	11.51	0.088 0	0.236 9
14	12.02	0.127 1	0.387 3	11.92	0.115 8	0.333 5	11.81	0.108 0	0.291 3	11.66	0.102 2	0.248 1
12	12.02	0.148 2	0.384 1	11.97	0.136 9	0.338 1	11.91	0.128 7	0.300 9	11.85	0.123 6	0.263 5
10	11.97	0.173 3	0.378 7	11.95	0.161 3	0.340 3	11.93	0.153 5	0.308 9	11.91	0.147 4	0.277 1
8	11.89	0.200 6	0.371 7	11.88	0.189 1	0.341 0	11.88	0.181 6	0.315 9	11.87	0.176 1	0.290 0
6	11.84	0.228 3	0.362 8	11.83	0.218 8	0.340 5	11.83	0.212 0	0.321 6	11.83	0.207 3	0.302 5
4	11.79	0.256 3	0.352 8	11.79	0.249 3	0.338 6	11.79	0.244 2	0.326 2	11.79	0.239 8	0.313 7
3	11.77	0.271 2	0.347 1	11.77	0.265 5	0.337 0	11.77	0.261 2	0.327 9	11.77	0.257 6	0.318 9
2	11.74	0.285 9	0.341 1	11.74	0.281 9	0.334 9	11.74	0.278 4	0.329 0	11.74	0.276 1	0.323 3
1	11.72	0.299 9	0.335 0	11.72	0.297 8	0.332 3	11.72	0.295 7	0.329 5	11.72	0.294 6	0.326 9
3/20	6.200	0.047 5	0.376 3	—	—	—	—	—	—	—	—	—
18	6.302	0.064 0	0.378 0	6.086	0.057 6	0.297 7	—	—	—	—	—	—
16	6.400	0.083 3	0.379 7	6.204	0.073 0	0.304 6	6.071	0.068 8	0.258 9	—	—	—
14	6.475	0.104 1	0.380 3	6.345	0.093 3	0.313 4	6.225	0.087 0	0.269 4	6.048	0.079 7	0.217 0
12	6.517	0.128 0	0.379 1	6.443	0.115 0	0.321 1	6.370	0.108 0	0.281 8	6.262	0.101 4	0.235 3
10	6.534	0.154 7	0.376 1	6.498	0.140 5	0.328 3	6.463	0.132 0	0.293 3	6.418	0.124 3	0.254 0
8	6.510	0.184 3	0.371 0	6.502	0.170 2	0.333 4	6.493	0.161 9	0.304 2	6.487	0.154 8	0.273 5
6	6.478	0.213 5	0.363 9	6.475	0.202 4	0.335 8	6.475	0.193 2	0.312 7	6.474	0.186 5	0.288 8
4	6.453	0.244 6	0.354 4	6.450	0.235 3	0.335 8	6.449	0.228 3	0.319 9	6.448	0.223 3	0.304 2
3	6.437	0.263 1	0.348 0	6.435	0.255 4	0.335 0	6.434	0.249 7	0.323 4	6.433	0.245 1	0.312 1
2	6.420	0.281 7	0.341 3	6.419	0.276 1	0.333 5	6.418	0.271 8	0.326 3	6.418	0.268 0	0.319 3
1	6.404	0.298 8	0.334 9	6.403	0.295 7	0.331 5	6.403	0.293 3	0.328 4	6.403	0.290 9	0.325 2
2/14	2.945	0.055 1	0.365 1	—	—	—	—	—	—	—	—	—
12	3.036	0.084 3	0.370 1	2.946	0.076 6	0.294 3	2.873	0.072 5	0.250 0	—	—	—
10	3.095	0.118 2	0.371 5	3.040	0.104 4	0.307 6	2.999	0.098 7	0.266 9	2.925	0.092 9	0.217 4
8	3.115	0.155 2	0.369 6	3.095	0.140 1	0.319 6	3.076	0.132 1	0.285 0	3.054	0.125 3	0.244 9
6	3.099	0.197 2	0.362 6	3.096	0.184 5	0.328 1	3.094	0.174 9	0.301 9	3.091	0.166 9	0.273 1
4	3.082	0.235 0	0.354 0	3.080	0.224 3	0.331 1	3.079	0.217 2	0.314 0	3.077	0.210 6	0.294 6
3	3.074	0.256 8	0.348 0	3.072	0.247 8	0.331 8	3.070	0.241 8	0.319 4	3.069	0.236 2	0.305 3
2	3.065	0.278 2	0.341 5	3.063	0.271 5	0.331 8	3.062	0.267 0	0.324 1	3.060	0.262 6	0.315 2
1	3.057	0.297 4	0.335 1	3.055	0.293 8	0.331 0	3.054	0.291 1	0.327 4	3.052	0.288 6	0.323 3
1/ 8	1.117	0.047 4	0.349 4	—	—	—	—	—	—	—	—	—
6	1.194	0.116 2	0.360 9	1.178	0.108 7	0.298 0	1.162	0.105 6	0.257 2	1.153	0.107 2	0.219 6
4	1.205	0.188 3	0.357 8	1.201	0.175 4	0.318 4	1.199	0.170 4	0.292 3	1.195	0.166 0	0.264 2
3	1.197	0.226 1	0.351 6	1.195	0.213 8	0.324 9	1.193	0.207 3	0.305 8	1.191	0.201 0	0.284 3
2	1.191	0.261 3	0.344 0	1.189	0.251 5	0.328 9	1.188	0.244 6	0.316 7	1.186	0.237 9	0.302 2
1	1.187	0.291 0	0.336 2	1.185	0.285 4	0.330 3	1.183	0.280 4	0.324 5	1.181	0.275 5	0.317 2

Annex Attached Table 1. (continued)

	2.5B			5B			7.5B			10B		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
9/ 4	77.04	0.270 0	0.321 8	76.99	0.269 6	0.314 9	76.94	0.270 9	0.310 4	76.91	0.273 5	0.306 5
3	76.94	0.282 1	0.324 2	76.91	0.282 8	0.319 9	76.88	0.284 7	0.316 9	76.85	0.286 6	0.314 6
2	76.85	0.293 3	0.326 3	76.83	0.294 4	0.323 9	76.80	0.296 2	0.322 3	76.79	0.297 5	0.321 2
1	76.77	0.303 6	0.328 0	76.76	0.304 4	0.327 1	76.74	0.305 7	0.326 5	76.73	0.306 3	0.326 1
8/12	58.46	0.188 0	0.292 9	—	—	—	—	—	—	—	—	—
10	58.28	0.207 4	0.300 6	—	—	—	—	—	—	—	—	—
8	58.13	0.227 6	0.308 0	58.12	0.225 0	0.291 7	58.14	0.226 6	0.282 4	58.19	0.230 9	0.274 3
6	58.01	0.247 8	0.315 2	57.97	0.247 4	0.303 8	57.94	0.249 1	0.296 9	57.88	0.253 3	0.290 5
4	57.88	0.268 7	0.321 2	57.85	0.269 2	0.314 2	57.82	0.271 0	0.309 9	57.78	0.274 2	0.305 2
3	57.81	0.280 5	0.323 9	57.79	0.281 4	0.319 1	57.76	0.283 1	0.316 0	57.73	0.285 4	0.312 9
2	57.74	0.292 1	0.326 2	57.72	0.293 3	0.323 3	57.70	0.294 7	0.321 4	57.69	0.296 1	0.319 8
1	57.68	0.303 1	0.328 1	57.66	0.304 0	0.326 9	57.65	0.304 9	0.326 0	57.65	0.305 5	0.325 5
7/16	43.35	0.143 0	0.267 7	—	—	—	—	—	—	—	—	—
14	42.79	0.162 2	0.276 0	43.03	0.161 3	0.248 9	—	—	—	—	—	—
12	42.58	0.179 9	0.284 1	42.55	0.178 0	0.259 2	42.64	0.182 2	0.246 6	42.76	0.188 8	0.236 7
10	42.48	0.200 1	0.293 9	42.45	0.199 4	0.273 8	42.40	0.202 6	0.262 0	42.34	0.209 1	0.253 1
8	42.38	0.221 9	0.302 9	42.35	0.221 7	0.288 4	42.31	0.224 0	0.278 3	42.26	0.229 4	0.270 7
6	42.29	0.243 3	0.311 3	42.26	0.242 7	0.300 5	42.23	0.245 5	0.293 5	42.19	0.249 9	0.287 3
4	42.19	0.264 8	0.318 4	42.17	0.265 3	0.311 7	42.15	0.267 3	0.307 1	42.12	0.270 8	0.302 8
3	42.14	0.276 8	0.321 9	42.12	0.277 6	0.316 9	42.11	0.279 3	0.313 6	42.08	0.282 2	0.310 4
2	42.09	0.289 0	0.324 9	42.08	0.289 9	0.321 6	42.06	0.291 3	0.319 5	42.05	0.293 4	0.317 5
1	42.04	0.301 1	0.327 5	42.03	0.301 8	0.325 9	42.02	0.302 6	0.324 9	42.01	0.303 8	0.324 0
6/16	30.42	0.128 2	0.255 3	30.39	0.129 6	0.224 0	30.20	0.136 4	0.205 2	30.02	0 144 4	0.193 5
14	30.11	0.147 3	0.265 0	29.96	0.148 9	0.236 6	29.75	0.155 2	0.219 7	29.69	0 162 7	0.209 4
12	29.76	0.165 8	0 273 2	29.72	0 168 5	0 250 1	29.68	0 173 6	0.235 8	29.63	0.180 8	0.226 2
10	29.68	0.188 3	0.284 8	29 65	0.188 8	0.264 7	29.61	0.194 2	0.252 8	29.56	0.201 1	0.244 7
8	29.61	0.208 9	0.295 0	29.58	0.209 9	0.279 2	29.55	0.214 5	0.268 9	29.51	0.220 4	0.261 6
6	29.54	0 232 6	0.305 4	29.51	0.233 5	0.294 1	29.49	0.236 9	0.285 7	29.45	0.241 9	0.279 6
4	29.46	0.258 9	0.315 6	29.44	0.259 9	0.308 4	29.42	0.262 3	0.302 5	29.40	0.266 0	0.298 2
3	29.42	0.272 4	0.319 9	29.40	0.273 3	0.314 7	29.39	0.275 1	0.310 3	29.37	0.277 9	0.306 8
2	29.38	0.285 8	0.323 7	29.37	0.286 6	0.320 2	29.36	0.287 9	0.317 5	29.35	0.289 7	0.314 9
1	29.34	0.299 3	0.326 8	29.33	0.299 9	0.325 1	29.33	0.300 5	0.324 0	29.32	0.301 4	0.322 4
5/18	—	—	—	—	—	—	—	—	—	19.47	0.118 4	0.161 8
16	19.60	0.107 4	0.230 8	19.54	0.111 5	0.199 1	19.58	0.121 1	0.184 8	19.60	0.131 1	0.176 9
14	19.75	0.126 8	0.246 8	19.69	0.130 5	0.218 3	19.62	0.139 3	0.202 9	19.57	0.148 5	0.194 1
12	19.69	0.145 2	0.258 2	19.61	0.149 8	0.233 5	19.55	0.158 1	0.219 5	19.52	0.166 6	0.211 0
10	19.56	0.169 6	0.271 7	19.53	0.173 0	0.250 7	19.50	0.179 6	0.238 3	19.47	0.186 7	0.229 6
8	19.50	0.195 3	0.285 0	19.48	0.196 6	0.267 7	19.45	0.201 7	0.257 0	19.43	0.208 0	0.249 2
6	19.44	0.222 2	0.298 0	19.43	0.222 8	0.285 5	19.41	0.226 3	0.276 2	19.38	0.231 7	0.269 4
4	19.39	0.250 9	0.310 3	19.38	0.251 2	0.302 7	19.36	0.253 1	0.295 4	19.34	0.256 9	0.290 0
3	19.36	0.266 0	0.316 0	19.35	0.266 3	0.310 2	19.34	0.267 7	0.304 9	19.32	0.270 6	0.300 3
2	19.33	0.281 3	0.321 1	19.32	0.281 7	0.317 2	19.31	0.282 7	0.313 9	19.30	0.284 6	0.310 4
1	19.30	0.297 0	0.325 7	19.29	0.297 3	0.323 5	19.29	0.297 9	0.322 2	19.29	0.298 9	0.320 1
4/16	11.41	0.089 3	0.202 3	—	—	—	—	—	—	11.43	0.114 4	0.147 4
14	11 55	0.101 8	0.213 6	11.52	0.108 7	0 186 2	11 62	0.119 0	0.175 2	11.75	0.129 7	0.169 3
12	11.81	0.123 4	0.235 0	11.81	0.128 7	0.209 8	11.84	0.138 3	0.197 5	11.88	0.148 0	0.190 1
10	11.89	0.145 6	0.251 6	11.88	0.150 7	0.230 5	11.87	0.159 8	0 217 9	11 84	0.168 2	0.209 9
8	11 87	0.173 8	0.269 0	11.85	0.176 1	0.250 4	11.83	0.182 6	0.238 4	11.81	0.190 1	0 230 6
6	11.82	0.205 7	0 286 8	11.81	0.207 0	0.272 7	11.80	0.211 5	0.262 1	11.78	0 217 2	0 255 3
4	11 78	0.237 5	0.302 4	11 78	0 238 0	0 293 2	11.77	0.240 7	0.285 1	11.75	0 245 0	0.279 2
3	11.76	0.255 9	0.310 4	11.76	0.255 8	0.303 5	11.75	0.257 6	0.297 1	11.74	0.260 9	0.292 0
2	11.74	0.274 9	0.318 0	11 74	0.274 5	0.313 3	11.73	0.275 7	0.308 7	11.73	0.277 8	0.304 9
1	11.72	0.294 0	0.324 4	11.72	0.293 7	0.322 1	11.71	0.294 2	0.319 6	11.71	0.295 2	0.317 5

Annex Attached Table 1. (continued)

	2.5B			5B			7.5B			10B		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
3/14	—	—	—	—	—	—	—	—	—	6.014	0.106 8	0.128 6
12	6.156	0.098 8	0.200 3	6.123	0.104 2	0.171 0	6.173	0.112 8	0.158 4	6.266	0.122 1	0.152 8
10	6.375	0.121 3	0.224 3	6.373	0.125 1	0.198 6	6.422	0.133 4	0.187 6	6.472	0.142 4	0.180 7
8	6.481	0.150 7	0.248 8	6.483	0.152 3	0.227 3	6.482	0.158 0	0.213 6	6.469	0.165 8	0.204 7
6	6.472	0.183 0	0.269 8	6.466	0.184 0	0.253 1	6.458	0.188 2	0.240 8	6.448	0.194 3	0.231 8
4	6.446	0.219 5	0.290 3	6.442	0.218 9	0.278 4	6.436	0.221 5	0.268 4	6.428	0.226 3	0.261 1
3	6.431	0.242 0	0.301 7	6.429	0.240 6	0.292 5	6.424	0.241 7	0.284 1	6.419	0.245 0	0.277 3
2	6.417	0.265 7	0.312 6	6.415	0.263 8	0.306 4	6.413	0.263 8	0.299 8	6.409	0.265 5	0.294 1
1	6.402	0.289 6	0.322 1	6.402	0.288 2	0.318 9	6.401	0.287 6	0.315 2	6.398	0.288 1	0.311 4
2/10	2.870	0.091 4	0.184 1	2.861	0.096 8	0.156 6	2.885	0.105 3	0.143 6	2.932	0.115 7	0.137 8
8	3.038	0.122 5	0.217 8	3.026	0.124 0	0.191 8	3.048	0.130 6	0.179 5	3.077	0.138 7	0.172 4
6	3.091	0.162 0	0.251 6	3.090	0.161 6	0.231 6	3.086	0.165 8	0.217 3	3.081	0.171 9	0.207 7
4	3.076	0.207 0	0.280 3	3.075	0.205 9	0.266 9	3.072	0.207 6	0.254 7	3.068	0.211 7	0.245 5
3	3.068	0.233 0	0.294 8	3.067	0.231 4	0.284 7	3.065	0.231 3	0.274 4	3.062	0.234 0	0.265 6
2	3.060	0.259 8	0.308 2	3.059	0.258 0	0.301 5	3.058	0.256 7	0.293 9	3.056	0.258 2	0.286 3
1	3.052	0.286 8	0.319 8	3.052	0.285 4	0.316 5	3.052	0.283 9	0.312 3	3.051	0.284 4	0.307 4
1/ 8	—	—	—	—	—	—	1.104	0.096 9	0.128 1	1.114	0.107 8	0.122 9
6	1.151	0.111 7	0.196 8	1.161	0.121 0	0.181 3	1.172	0.129 9	0.172 2	1.185	0.138 6	0.166 8
4	1.194	0.165 1	0.246 7	1.193	0.166 9	0.230 8	1.192	0.172 0	0.218 8	1.190	0.179 0	0.210 9
3	1.191	0.198 0	0.270 2	1.190	0.196 8	0.256 4	1.188	0.199 1	0.244 3	1.187	0.203 5	0.235 2
2	1.186	0.233 9	0.292 1	1.185	0.230 9	0.281 6	1.185	0.231 0	0.271 6	1.184	0.233 0	0.262 5
1	1.181	0.272 4	0.311 9	1.181	0.269 6	0.306 0	1.181	0.268 7	0.299 9	1.180	0.269 0	0.293 3

Annex Attached Table 1. (continued)

	2.5PB			5PB			7.5PB			10PB		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
9/ 4	—	—	—	—	—	—	—	—	—	76.69	0.294 0	0.298 2
3	—	—	—	—	—	—	—	—	—	77.77	0.301 4	0.281 2
2	76.75	0.300 2	0.319 7	76.73	0.301 9	0.319 0	76.71	0.304 3	0.318 4	76.70	0.306 7	0.318 5
1	76.72	0.306 5	0.324 6	76.71	0.307 4	0.324 2	76.71	0.308 6	0.323 9	76.70	0.310 6	0.325 0
8/ 8	—	—	—	—	—	—	—	—	—	57.87	0.270 6	0.257 9
6	57.79	0.258 6	0.285 1	57.72	0.264 0	0.280 8	57.65	0.273 1	0.278 3	57.60	0.282 3	0.278 0
4	57.73	0.278 4	0.301 8	57.68	0.282 5	0.299 8	57.64	0.288 5	0.298 0	57.61	0.294 1	0.298 0
3	57.69	0.288 8	0.310 3	57.66	0.291 8	0.308 9	57.63	0.296 2	0.307 7	57.61	0.300 2	0.307 8
2	57.66	0.298 4	0.318 2	57.65	0.300 2	0.317 2	57.63	0.303 1	0.316 6	57.62	0.305 6	0.316 6
1	57.64	0.306 7	0.324 8	57.63	0.307 4	0.324 2	57.62	0.308 9	0.324 0	57.62	0.310 0	0.323 9
7/12	—	—	—	—	—	—	—	—	—	42.05	0.249 4	0.218 3
10	42.23	0.217 8	0.245 2	42.13	0.227 4	0.240 4	42.02	0.243 6	0.235 4	41.95	0.259 4	0.236 6
8	42.17	0.237 2	0.264 1	42.10	0.245 0	0.259 6	42.01	0.257 4	0.255 1	41.96	0.270 2	0.255 4
6	42.12	0.256 1	0.281 9	42.07	0.262 2	0.278 1	42.01	0.271 6	0.274 6	41.97	0.280 8	0.274 3
4	42.07	0.275 5	0.298 7	42.04	0.280 0	0.296 5	42.00	0.286 2	0.294 3	41.98	0.291 7	0.293 3
3	42.05	0.285 8	0.307 6	42.02	0.289 2	0.305 7	42.00	0.293 8	0.304 1	41.98	0.297 6	0.303 4
2	42.03	0.295 9	0.316 0	42.01	0.298 0	0.314 5	41.99	0.301 1	0.313 5	41.99	0.303 4	0.313 1
1	42.00	0.305 1	0.323 5	42.00	0.306 0	0.322 5	41.99	0.307 5	0.322 0	41.99	0.308 6	0.321 9
6/16	—	—	—	—	—	—	—	—	—	29.25	0.229 1	0.177 9
14	29.57	0.175 7	0.200 5	29.46	0.188 2	0.195 1	29.32	0.213 8	0.191 8	29.24	0.238 1	0.195 3
12	29.52	0.192 2	0.217 8	29.43	0.204 0	0.213 2	29.32	0.226 4	0.209 9	29.25	0.247 0	0.211 7
10	29.48	0.211 0	0.236 7	29.40	0.221 6	0.232 4	29.32	0.240 4	0.229 7	29.26	0.257 2	0.229 9
8	29.44	0.229 3	0.254 8	29.38	0.238 3	0.250 2	29.31	0.253 3	0.247 8	29.27	0.266 9	0.247 9
6	29.40	0.248 7	0.274 1	29.36	0.255 8	0.269 6	29.31	0.266 7	0.266 4	29.28	0.277 2	0.266 2
4	29.36	0.270 9	0.294 3	29.33	0.276 1	0.291 5	29.31	0.282 8	0.288 6	29.29	0.289 4	0.287 8
3	29.35	0.281 7	0.303 8	29.32	0.285 8	0.301 5	29.30	0.290 7	0.299 2	29.29	0.295 7	0.298 6
2	29.33	0.292 4	0.312 6	29.32	0.295 1	0.311 2	29.30	0.298 4	0.309 5	29.29	0.301 8	0.309 2
1	29.31	0.302 7	0.321 2	29.31	0.304 1	0.320 4	29.30	0.305 8	0.319 5	29.30	0.307 6	0.319 4
5/22	—	—	—	—	—	—	—	—	—	18.99	0.210 0	0.129 8
20	—	—	—	—	—	—	19.15	0.179 8	0.132 5	19.17	0.214 5	0.141 9
18	19.49	0.134 8	0.152 8	19.39	0.151 0	0.147 4	19.28	0.187 2	0.146 5	19.19	0.219 9	0.154 0
16	19.50	0.148 7	0.168 6	19.41	0.163 6	0.164 0	19.28	0.195 8	0.161 8	19.20	0.225 1	0.165 6
14	19.47	0.164 1	0.186 1	19.39	0.177 8	0.181 4	19.28	0.205 9	0.177 5	19.21	0.232 7	0.180 6
12	19.43	0.179 8	0.203 1	19.37	0.192 8	0.198 8	19.28	0.217 8	0.195 0	19.22	0.241 4	0.197 1
10	19.40	0.197 9	0.221 8	19.35	0.209 6	0.217 4	19.28	0.230 9	0.214 5	19.23	0.251 0	0.214 9
8	19.37	0.217 3	0.241 9	19.33	0.227 6	0.237 5	19.28	0.244 4	0.233 3	19.24	0.260 4	0.233 5
6	19.35	0.238 6	0.263 0	19.31	0.247 1	0.258 6	19.28	0.259 2	0.254 9	19.25	0.271 9	0.253 9
4	19.32	0.262 5	0.286 0	19.30	0.268 9	0.282 4	19.27	0.276 9	0.279 9	19.26	0.285 3	0.278 9
3	19.31	0.274 8	0.297 0	19.29	0.280 0	0.294 1	19.27	0.285 8	0.292 0	19.26	0.292 1	0.291 1
2	19.29	0.287 4	0.307 8	19.28	0.291 0	0.305 7	19.27	0.294 8	0.304 0	19.26	0.298 9	0.303 5
1	19.28	0.300 0	0.318 5	19.27	0.302 0	0.317 4	19.27	0.303 8	0.316 4	19.27	0.305 8	0.316 2
4/30	—	—	—	—	—	—	—	—	—	11.04	0.196 2	0.079 8
28	—	—	—	—	—	—	—	—	—	11.16	0.198 3	0.086 9
26	—	—	—	—	—	—	11.19	0.165 9	0.085 7	11.24	0.200 9	0.094 2
24	—	—	—	—	—	—	11.31	0.168 6	0.094 2	11.35	0.203 7	0.103 3
22	—	—	—	—	—	—	11.41	0.171 9	0.103 4	11.42	0.206 8	0.112 1
20	—	—	—	11.35	0.127 6	0.107 6	11.50	0.175 0	0.112 2	11.49	0.209 8	0.120 6
18	11.38	0.120 6	0.126 1	11.58	0.138 3	0.124 5	11.62	0.180 7	0.126 7	11.58	0.214 5	0.133 0
16	11.66	0.132 4	0.144 2	11.70	0.149 8	0.141 6	11.70	0.187 1	0.141 3	11.64	0.219 6	0.146 4
14	11.81	0.146 5	0.163 3	11.78	0.162 5	0.159 5	11.70	0.195 5	0.157 3	11.65	0.224 7	0.160 1
12	11.82	0.163 3	0.182 9	11.77	0.177 8	0.178 2	11.70	0.205 4	0.174 1	11.66	0.232 7	0.176 4
10	11.80	0.181 1	0.202 4	11.76	0.193 6	0.197 1	11.70	0.217 9	0.192 9	11.67	0.241 9	0.194 9
8	11.78	0.200 7	0.223 3	11.74	0.212 0	0.218 2	11.70	0.232 9	0.214 7	11.68	0.252 9	0.215 6
6	11.75	0.225 4	0.248 4	11.73	0.234 7	0.243 5	11.70	0.249 9	0.239 5	11.68	0.265 1	0.238 7
4	11.74	0.251 0	0.273 7	11.72	0.258 9	0.269 6	11.70	0.268 7	0.266 0	11.69	0.279 2	0.265 0
3	11.73	0.265 5	0.287 3	11.71	0.271 4	0.283 3	11.70	0.278 6	0.280 0	11.69	0.286 5	0.278 6
2	11.72	0.280 9	0.301 3	11.71	0.284 4	0.297 6	11.70	0.289 1	0.295 1	11.69	0.294 3	0.293 3
1	11.71	0.296 7	0.315 4	11.70	0.298 2	0.312 9	11.70	0.300 4	0.311 4	11.70	0.303 0	0.310 0

Annex Attached Table 1. (continued)

	2.5PB			5PB			7.5PB			10PB		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
3/34	—	—	—	—	—	—	5.963	0.160 7	0.048 9	5.998	0.192 3	0.051 5
32	—	—	—	—	—	—	5.998	0.161 2	0.052 3	6.033	0.193 3	0.055 8
30	—	—	—	—	—	—	6.037	0.162 3	0.057 3	6.076	0.194 7	0.062 1
28	—	—	—	—	—	—	6.087	0.163 8	0.063 1	6.103	0.196 1	0.067 6
26	—	—	—	—	—	—	6.121	0.164 8	0.068 2	6.134	0.197 9	0.073 8
24	—	—	—	—	—	—	6.160	0.166 5	0.074 5	6.173	0.200 2	0.080 9
22	—	—	—	—	—	—	6.204	0.168 4	0.082 4	6.211	0.202 7	0.089 1
20	—	—	—	—	—	—	6.248	0.171 0	0.091 9	6.243	0.205 4	0.098 2
18	—	—	—	5.994	0.122 8	0.089 7	6.279	0.173 9	0.100 7	6.272	0.208 5	0.108 0
16	—	—	—	6.159	0.131 2	0.106 4	6.325	0.177 4	0.111 9	6.301	0.211 8	0.118 7
14	6.175	0.124 5	0.126 3	6.337	0.142 5	0.126 3	6.363	0.183 4	0.127 3	6.335	0.216 8	0.133 1
12	6.394	0.139 0	0.149 5	6.422	0.155 3	0.146 2	6.386	0.191 6	0.145 1	6.356	0.223 4	0.149 9
10	6.458	0.157 2	0.172 7	6.429	0.172 1	0.168 0	6.389	0.202 2	0.164 2	6.363	0.230 8	0.166 5
8	6.443	0.178 5	0.196 6	6.420	0.191 9	0.192 5	6.390	0.217 1	0.187 6	6.370	0.241 9	0.189 5
6	6.429	0.203 6	0.223 8	6.412	0.214 0	0.218 3	6.390	0.233 7	0.213 2	6.376	0.254 4	0.214 8
4	6.415	0.233 3	0.254 4	6.404	0.241 7	0.249 5	6.390	0.254 9	0.244 7	6.381	0.269 4	0.244 2
3	6.409	0.250 2	0.271 3	6.400	0.257 0	0.266 7	6.390	0.267 1	0.262 3	6.383	0.278 1	0.260 7
2	6.402	0.268 9	0.289 3	6.396	0.273 6	0.285 3	6.390	0.280 8	0.281 7	6.385	0.288 0	0.279 7
1	6.395	0.289 7	0.308 6	6.393	0.292 2	0.306 0	6.390	0.295 9	0.303 8	6.388	0.299 5	0.302 2
2/38	—	—	—	—	—	—	2.859	0.162 1	0.028 8	—	—	—
36	—	—	—	—	—	—	2.878	0.162 8	0.032 0	—	—	—
34	—	—	—	—	—	—	2.900	0.163 1	0.035 3	2.859	0.191 7	0.035 5
32	—	—	—	—	—	—	2.916	0.163 7	0.039 0	2.878	0.192 5	0.039 3
30	—	—	—	—	—	—	2.931	0.164 3	0.043 0	2.891	0.193 4	0.043 6
28	—	—	—	—	—	—	2.945	0.165 0	0.047 5	2.917	0.195 1	0.049 2
26	—	—	—	—	—	—	2.951	0.165 6	0.051 8	2.940	0.196 7	0.054 7
24	—	—	—	—	—	—	2.971	0.166 3	0.057 1	2.957	0.198 2	0.061 0
22	—	—	—	—	—	—	2.983	0.167 4	0.063 2	2.970	0.199 9	0.068 1
20	—	—	—	—	—	—	2.993	0.169 0	0.071 0	2.980	0.202 0	0.076 2
18	—	—	—	—	—	—	3.002	0.170 7	0.079 2	2.991	0.204 4	0.085 9
16	—	—	—	—	—	—	3.012	0.173 6	0.089 6	3.001	0.207 6	0.096 8
14	—	—	—	2.886	0.125 5	0.088 0	3.022	0.177 1	0.102 2	3.011	0.211 2	0.109 3
12	2.886	0.116 8	0.108 4	2.977	0.135 8	0.109 7	3.032	0.182 4	0.117 2	3.020	0.216 6	0.124 6
10	3.013	0.132 5	0.134 9	3.055	0.149 5	0.133 3	3.042	0.189 5	0.134 9	3.027	0.222 9	0.141 6
8	3.079	0.153 5	0.165 2	3.065	0.168 7	0.160 5	3.045	0.202 3	0.159 8	3.033	0.232 5	0.164 8
6	3.069	0.183 3	0.198 8	3.059	0.195 5	0.193 5	3.046	0.221 3	0.190 4	3.037	0.247 4	0.194 8
4	3.061	0.219 3	0.238 1	3.054	0.228 6	0.232 2	3.046	0.244 9	0.227 1	3.041	0.263 6	0.227 9
3	3.057	0.239 7	0.259 0	3.052	0.246 8	0.253 0	3.046	0.258 7	0.247 7	3.042	0.272 9	0.246 7
2	3.053	0.261 8	0.281 0	3.050	0.266 7	0.275 5	3.046	0.274 4	0.270 9	3.044	0.283 8	0.269 0
1	3.049	0.286 1	0.304 2	3.048	0.288 5	0.300 6	3.047	0.292 3	0.297 6	3.046	0.297 0	0.295 8
1/38	—	—	—	—	—	—	1.072	0.168 0	0.014 2	—	—	—
36	—	—	—	—	—	—	1.089	0.168 2	0.016 4	—	—	—
34	—	—	—	—	—	—	1.101	0.168 4	0.018 6	—	—	—
32	—	—	—	—	—	—	1.111	0.168 4	0.021 1	—	—	—
30	—	—	—	—	—	—	1.122	0.168 7	0.024 7	1.091	0.194 5	0.025 1
28	—	—	—	—	—	—	1.129	0.168 9	0.028 6	1.100	0.194 9	0.029 3
26	—	—	—	—	—	—	1.137	0.169 2	0.032 9	1.119	0.196 0	0.034 4
24	—	—	—	—	—	—	1.144	0.169 5	0.037 6	1.134	0.197 3	0.040 4
22	—	—	—	—	—	—	1.150	0.170 0	0.043 1	1.142	0.198 8	0.046 6
20	—	—	—	—	—	—	1.155	0.170 6	0.048 7	1.147	0.199 9	0.052 3
18	—	—	—	—	—	—	1.159	0.171 4	0.055 7	1.151	0.201 5	0.060 5
16	—	—	—	—	—	—	1.162	0.172 6	0.062 7	1.155	0.203 3	0.068 5
14	—	—	—	—	—	—	1.166	0.174 6	0.074 0	1.160	0.206 5	0.079 9
12	—	—	—	—	—	—	1.169	0.177 2	0.086 4	1.163	0.209 8	0.093 1
10	—	—	—	1.126	0.128 6	0.088 2	1.172	0.181 5	0.101 9	1.167	0.215 0	0.109 9
8	1.148	0.127 1	0.119 8	1.176	0.144 1	0.120 1	1.175	0.188 7	0.122 1	1.170	0.222 2	0.130 6
6	1.190	0.153 6	0.160 6	1.185	0.168 2	0.155 5	1.177	0.202 1	0.151 7	1.172	0.232 4	0.155 8
4	1.186	0.190 7	0.203 7	1.182	0.203 0	0.198 6	1.178	0.226 0	0.193 0	1.175	0.249 7	0.192 9
3	1.184	0.212 2	0.227 4	1.181	0.222 2	0.221 6	1.178	0.240 0	0.215 0	1.176	0.259 1	0.212 7
2	1.182	0.238 5	0.254 9	1.180	0.245 5	0.249 2	1.178	0.258 1	0.242 7	1.177	0.271 6	0.239 1
1	1.180	0.271 5	0.287 8	1.179	0.275 2	0.283 6	1.179	0.281 8	0.279 1	1.178	0.289 0	0.276 0

Annex Attached Table 1. (continued)

	2.5P			5P			7.5P			10P		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
9/ 6	—	—	—	—	—	—	76.44	0.315 7	0.290 7	76.03	0.325 7	0.295 3
4	76.66	0.299 4	0.299 5	76.64	0.303 5	0.299 9	76.58	0.315 0	0.305 3	76.51	0.321 0	0.308 9
3	76.68	0.304 1	0.309 8	76.66	0.306 9	0.310 6	76.64	0.314 3	0.313 6	76.62	0.318 2	0.316 0
2	76.69	0.307 9	0.318 1	76.68	0.309 6	0.319 0	76.67	0.313 6	0.321 0	76.66	0.315 7	0.322 2
1	76.70	0.310 8	0.324 6	76.70	0.311 6	0.325 2	76.69	0.313 1	0.326 6	76.69	0.313 8	0.326 9
8/14	—	—	—	—	—	—	—	—	—	56.29	0.340 2	0.242 4
12	—	—	—	—	—	—	57.31	0.316 3	0.247 8	56.72	0.336 5	0.255 9
10	—	—	—	57.91	0.290 6	0.251 0	57.39	0.315 9	0.261 1	57.01	0.333 0	0.268 3
8	57.71	0.283 3	0.261 8	57.64	0.295 0	0.266 1	57.45	0.315 6	0.274 5	57.24	0.329 3	0.281 0
6	57.56	0.291 4	0.280 0	57.53	0.299 8	0.283 1	57.49	0.315 0	0.290 8	57.46	0.325 0	0.295 0
4	57.59	0.299 4	0.298 0	57.57	0.304 4	0.299 7	57.54	0.314 7	0.304 1	57.53	0.320 9	0.307 9
3	57.60	0.303 7	0.307 9	57.59	0.307 0	0.309 0	57.57	0.314 2	0.312 2	57.56	0.318 5	0.314 8
2	57.61	0.307 7	0.317 0	57.60	0.309 4	0.317 7	57.59	0.313 7	0.319 9	57.59	0.316 1	0.321 2
1	57.62	0.310 9	0.324 5	57.62	0.311 4	0.324 8	57.61	0.313 1	0.325 9	57.61	0.314 1	0.326 2
7/22	—	—	—	—	—	—	—	—	—	40.96	0.350 6	0.194 7
20	—	—	—	—	—	—	—	—	—	41.09	0.348 2	0.205 9
18	—	—	—	—	—	—	41.51	0.315 1	0.205 0	41.22	0.345 9	0.216 6
16	—	—	—	—	—	—	41.61	0.315 4	0.217 0	41.35	0.343 1	0.227 7
14	—	—	—	42.03	0.284 1	0.218 4	41.68	0.315 2	0.229 4	41.49	0.339 8	0.240 1
12	42.05	0.269 8	0.225 0	41.94	0.287 3	0.231 5	41.76	0.315 1	0.242 9	41.61	0.336 6	0.252 4
10	41.89	0.276 5	0.241 1	41.85	0.291 2	0.246 2	41.80	0.315 2	0.255 6	41.72	0.333 5	0.264 0
8	41.92	0.283 4	0.258 4	41.89	0.295 6	0.262 7	41.84	0.315 0	0.270 2	41.81	0.329 9	0.276 9
6	41.94	0.290 7	0.276 1	41.92	0.299 6	0.278 9	41.88	0.314 9	0.285 2	41.86	0.326 0	0.290 5
4	41.96	0.298 2	0.293 9	41.94	0.304 2	0.295 9	41.92	0.314 5	0.300 5	41.91	0.321 6	0.304 3
3	41.97	0.302 2	0.303 6	41.96	0.306 6	0.305 0	41.94	0.314 3	0.308 7	41.93	0.319 1	0.311 4
2	41.98	0.306 1	0.313 0	41.97	0.308 9	0.313 9	41.96	0.313 9	0.316 5	41.96	0.316 9	0.318 1
1	41.99	0.309 6	0.321 7	41.98	0.311 1	0.322 2	41.98	0.313 5	0.323 5	41.98	0.314 7	0.324 1
6/26	—	—	—	—	—	—	—	—	—	28.72	0.354 0	0.167 0
24	—	—	—	—	—	—	28.71	0.312 9	0.161 2	28.74	0.352 0	0.176 7
22	—	—	—	—	—	—	28.79	0.313 0	0.171 0	28.78	0.350 3	0.185 7
20	—	—	—	28.99	0.274 8	0.170 7	28.87	0.313 3	0.182 5	28.84	0.348 2	0.196 0
18	29.15	0.253 8	0.175 7	29.04	0.277 6	0.183 1	28.95	0.313 5	0.195 8	28.90	0.345 6	0.207 9
16	29.16	0.258 4	0.187 2	29.09	0.280 6	0.195 2	29.01	0.313 6	0.207 0	28.95	0.343 3	0.218 5
14	29.17	0.263 1	0.201 9	29.13	0.283 8	0.208 6	29.06	0.313 6	0.219 6	29.01	0.340 7	0.229 9
12	29.20	0.268 4	0.216 7	29.16	0.287 2	0.223 3	29.11	0.313 9	0.232 9	29.07	0.337 4	0.243 2
10	29.22	0.274 0	0.232 3	29.19	0.290 3	0.237 6	29.14	0.313 8	0.246 2	29.11	0.334 2	0.255 8
8	29.24	0.280 6	0.249 5	29.21	0.294 4	0.254 1	29.18	0.314 1	0.261 8	29.16	0.330 3	0.269 7
6	29.26	0.287 7	0.267 6	29.24	0.298 7	0.270 9	29.21	0.314 0	0.277 0	29.19	0.326 6	0.283 3
4	29.27	0.296 5	0.288 8	29.26	0.303 5	0.290 5	29.25	0.314 2	0.295 5	29.24	0.321 7	0.299 3
3	29.28	0.300 6	0.298 9	29.27	0.305 9	0.300 0	29.26	0.314 1	0.303 9	29.25	0.319 8	0.306 9
2	29.29	0.304 6	0.309 0	29.28	0.308 1	0.309 6	29.27	0.313 8	0.312 0	29.27	0.317 8	0.314 4
1	29.29	0.308 7	0.319 1	29.29	0.310 4	0.319 2	29.29	0.313 5	0.320 3	29.28	0.315 5	0.321 8
5/30	—	—	—	—	—	—	18.85	0.308 5	0.122 4	18.98	0.358 8	0.137 7
28	—	—	—	18.65	0.267 1	0.118 0	18.85	0.309 1	0.131 1	18.95	0.356 9	0.145 4
26	18.67	0.238 1	0.118 9	18.76	0.268 6	0.127 9	18.86	0.309 3	0.139 2	18.94	0.355 5	0.152 6
24	18.82	0.240 6	0.128 4	18.84	0.270 2	0.136 6	18.89	0.309 8	0.148 8	18.93	0.353 3	0.162 3
22	18.94	0.243 7	0.138 7	18.93	0.272 2	0.146 9	18.92	0.310 4	0.157 0	18.94	0.351 6	0.171 5
20	19.07	0.247 6	0.150 3	19.01	0.274 3	0.158 0	18.97	0.310 5	0.168 3	18.96	0.349 7	0.181 0
18	19.12	0.251 5	0.162 4	19.08	0.276 6	0.169 3	19.02	0.311 1	0.179 5	18.98	0.347 0	0.192 0
16	19.14	0.255 4	0.174 2	19.10	0.279 1	0.181 3	19.06	0.311 7	0.192 1	19.02	0.344 7	0.203 7
14	19.16	0.259 9	0.187 8	19.13	0.282 1	0.194 8	19.09	0.312 2	0.204 7	19.05	0.342 1	0.215 8
12	19.18	0.264 6	0.202 2	19.15	0.285 1	0.208 3	19.12	0.312 3	0.218 2	19.09	0.339 2	0.228 4
10	19.20	0.270 3	0.219 0	19.18	0.288 8	0.224 9	19.15	0.312 8	0.233 8	19.12	0.336 0	0.243 1
8	19.22	0.276 5	0.236 0	19.20	0.292 6	0.241 2	19.17	0.313 2	0.248 7	19.15	0.332 8	0.257 3
6	19.23	0.284 2	0.256 8	19.22	0.297 0	0.260 8	19.20	0.313 4	0.267 3	19.19	0.328 6	0.274 5
4	19.25	0.293 2	0.279 4	19.24	0.302 1	0.282 4	19.22	0.313 7	0.287 2	19.22	0.323 6	0.292 7
3	19.25	0.298 1	0.291 7	19.25	0.304 9	0.293 9	19.24	0.313 7	0.297 8	19.23	0.320 8	0.302 0
2	19.26	0.303 1	0.304 1	19.25	0.307 7	0.305 6	19.25	0.313 5	0.308 5	19.25	0.318 0	0.311 1
1	19.26	0.308 0	0.316 7	19.26	0.310 4	0.317 4	19.26	0.313 3	0.319 1	19.26	0.315 4	0.320 2

Annex Attached Table 1. (continued)

	2.5P			5P			7.5P			10P		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
4/32	11.07	0.228 9	0 079 5	11.22	0.261 6	0.086 5	11.32	0.302 8	0.094 9	—	—	—
30	11.16	0.231 2	0 087 6	11.27	0.263 1	0.094 5	11.35	0.303 5	0.102 6	11.37	0.354 7	0.114 3
28	11.23	0.233 1	0.094 5	11.29	0.264 4	0.101 2	11.36	0.304 2	0.110 9	11.39	0.351 9	0.122 9
26	11.30	0.235 3	0.102 2	11.34	0.266 3	0.109 9	11.39	0.304 9	0.118 6	11.42	0.351 2	0.130 5
24	11.36	0.238 1	0 111 3	11.38	0.268 3	0.118 5	11.42	0.305 8	0.128 1	11.45	0.350 3	0.139 7
22	11.42	0.240 7	0 120 2	11.43	0.270 2	0.127 8	11.45	0.306 6	0.136 7	11.47	0.349 2	0.148 8
20	11.48	0.243 2	0.128 8	11.48	0.272 0	0.136 7	11.48	0.307 4	0.146 3	11.48	0.347 9	0.156 7
18	11.55	0.246 9	0.141 0	11.54	0.274 3	0.148 5	11.51	0.307 9	0.157 3	11.49	0.346 1	0.169 7
16	11.60	0.250 6	0.153 9	11.57	0.276 8	0.160 4	11.54	0.308 9	0.170 1	11.51	0.344 0	0.183 3
14	11.61	0.254 8	0.167 9	11.59	0.279 5	0.175 1	11.56	0.309 3	0.184 2	11.54	0.341 7	0.195 8
12	11.63	0.259 8	0 183 1	11.61	0.282 5	0.190 6	11.59	0.310 0	0.199 9	11.56	0.339 2	0.210 4
10	11.64	0.265 8	0.201 1	11.63	0.285 9	0.207 2	11.61	0.310 8	0.216 1	11.59	0.336 3	0.225 9
8	11.66	0.272 3	0.220 3	11.64	0.289 8	0.226 1	11.63	0.311 4	0.233 5	11.61	0.333 2	0.242 2
6	11.67	0.280 0	0.242 0	11.66	0.294 4	0.246 4	11.65	0.312 0	0.253 0	11.63	0.329 5	0.260 3
4	11.68	0.289 1	0.265 6	11.67	0.299 6	0.268 7	11.66	0.312 4	0.274 1	11.66	0.325 1	0.280 2
3	11.68	0.294 0	0.278 7	11.68	0.302 4	0.281 2	11.67	0.312 6	0.285 6	11.67	0.322 5	0.290 9
2	11.69	0.299 5	0.293 5	11.69	0.305 6	0 295 1	11.68	0.312 7	0.298 3	11.68	0.319 7	0.302 4
1	11.69	0.305 6	0.310 1	11.69	0.309 0	0.310 9	11.69	0.312 8	0.312 6	11.69	0.316 4	0.315 1
3/34	6.022	0.224 7	0.055 9	—	—	—	—	—	—	—	—	—
32	6.055	0.226 1	0.060 7	6 036	0.259 2	0.065 4	—	—	—	—	—	—
30	6.082	0.227 2	0.066 2	6.067	0.260 2	0.071 7	6.034	0.298 8	0.078 6	—	—	—
28	6.107	0.228 9	0 072 6	6 094	0.261 3	0.078 0	6.065	0 298 5	0.084 6	—	—	—
26	6.140	0.231 1	0 079 8	6 132	0.262 7	0.085 7	6.104	0 298 9	0 092 8	6.066	0.342 8	0.102 5
24	6.172	0.233 5	0 087 1	6 166	0.264 3	0 093 1	6.144	0 299 7	0 100 8	6.114	0.341 3	0.110 0
22	6.209	0 236 4	0 095 7	6 206	0.266 6	0.102 5	6.187	0.301 0	0 110 5	6.164	0.341 2	0.119 6
20	6 244	0 239 2	0 105 7	6 240	0.268 9	0 112 9	6.232	0.302 4	0 120 7	6.207	0.340 6	0.129 5
18	6.269	0.242 0	0 115 5	6.263	0.270 8	0.122 4	6.254	0.303 3	0.130 0	6.240	0.340 6	0.139 3
16	6.292	0 245 0	0 126 7	6.284	0.273 2	0.134 0	6.275	0.304 5	0 142 4	6.266	0.339 6	0.152 3
14	6.316	0 249 0	0.140 3	6.302	0.275 9	0 147 3	6.288	0.305 5	0 154 8	6.279	0.338 2	0.164 3
12	6 334	0 253 9	0.156 8	6 318	0.278 9	0.162 3	6.303	0 306 3	0.169 8	6.288	0.337 0	0.179 1
10	6 345	0.258 9	0.173 4	6.332	0.282 1	0 179 9	6.320	0 307 6	0 188 3	6.308	0.335 0	0.197 4
8	6 356	0 265 5	0 194 9	6.345	0.286 6	0 201 1	6 335	0 309 0	0 207 8	6.326	0.332 7	0.216 9
6	6.366	0 273 0	0.218 5	6.357	0.291 4	0 224 4	6 350	0.310 5	0.231 4	6.343	0.329 5	0.239 6
4	6 374	0.283 0	0.246 2	6 368	0.296 9	0.250 2	6 363	0 311 5	0 256 1	6.358	0.325 9	0.262 8
3	6 378	0.288 8	0.262 0	6.373	0.299 9	0.265 0	6 369	0 312 1	0.270 0	6.365	0.323 7	0.275 8
2	6 382	0.295 7	0.280 5	6.379	0.303 3	0.282 3	6 375	0 312 5	0 286 0	6.373	0.320 8	0.290 8
1	6 386	0.303 6	0.302 5	6.384	0.307 6	0 303 3	6 383	0 312 8	0 305 4	6.382	0.317 2	0.308 3
2/30	2 843	0.225 2	0 044 8	—	—	—	—	—	—	—	—	—
28	2.868	0.226 3	0 050 9	2.827	0.261 0	0 055 1	—	—	—	—	—	—
26	2.896	0.228 2	0.057 8	2 854	0.260 5	0.061 8	—	—	—	—	—	—
24	2 922	0.230 4	0 065 0	2 884	0.261 7	0.069 6	2 851	0.293 3	0 074 8	—	—	—
22	2 950	0.233 2	0 073 3	2 916	0.263 6	0 078 4	2 881	0.293 7	0 083 1	2.850	0.330 2	0.089 9
20	2 970	0.235 8	0 082 4	2 948	0.265 9	0.088 1	2 919	0.295 3	0.094 0	2.885	0.329 1	0.100 0
18	2 983	0.238 5	0.092 5	2 971	0.268 5	0.098 6	2 950	0 297 0	0 104 3	2.921	0.329 6	0.110 8
16	2 993	0.241 3	0 103 9	2.985	0.270 6	0.110 4	2 974	0 298 6	0.116 3	2.957	0.330 6	0.123 6
14	3 001	0.244 7	0.116 6	2 994	0.273 0	0.122 8	2 988	0.300 3	0.130 0	2.981	0.330 9	0.138 1
12	3 009	0.249 1	0.131 9	3 002	0.276 2	0 139 2	2 997	0 302 0	0 146 4	2.993	0.330 6	0 154 7
10	3 017	0.254 3	0.150 5	3.010	0.280 0	0 158 0	3 004	0.303 9	0.164 6	2.999	0.329 8	0.173 4
8	3 024	0.261 2	0.172 8	3 019	0.284 1	0.179 7	3 014	0 305 6	0.186 8	3.009	0.328 1	0.194 6
6	3 032	0.270 2	0.202 6	3 027	0.289 7	0.209 4	3 024	0 307 6	0.215 7	3.020	0.326 2	0.222 8
4	3 037	0.279 8	0.232 1	3 034	0.295 2	0.237 1	3.031	0 309 4	0.242 9	3.029	0.323 7	0.249 5
3	3 039	0.285 7	0.249 4	3 037	0.298 3	0 253 3	3 035	0 310 2	0 258 0	3 033	0.322 3	0 263 6
2	3 042	0.292 9	0.270 3	3 040	0.302 2	0.273 0	3 039	0.311 1	0.276 2	3.037	0.320 2	0.280 4
1	3 044	0.301 9	0.296 2	3 044	0.307 0	0.297 5	3 043	0.312 0	0.299 2	3.042	0.317 1	0.301 6

Annex Attached Table 1. (continued)

	2.5P			5P			7.5P			10P		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
1/26	1.090	0.228 7	0.037 2	—	—	—	—	—	—	—	—	—
24	1.098	0.229 6	0.043 7	—	—	—	—	—	—	—	—	—
22	1.113	0.231 3	0.049 8	1.094	0.263 2	0.052 9	—	—	—	—	—	—
20	1.131	0.233 5	0.057 5	1.103	0.264 5	0.061 2	1.093	0.288 5	0.065 1	—	—	—
18	1.143	0.235 7	0.066 0	1.122	0.266 1	0.070 2	1.105	0.289 5	0.073 8	1.094	0.312 5	0.077 6
16	1.149	0.237 7	0.074 4	1.136	0.268 1	0.079 0	1.122	0.291 1	0.083 0	1.110	0.313 8	0.087 5
14	1.154	0.240 8	0.086 6	1.148	0.270 5	0.091 8	1.140	0.293 5	0.095 5	1.129	0.315 2	0.100 0
12	1.158	0.244 1	0.100 3	1.155	0.273 1	0.107 0	1.151	0.295 4	0.112 2	1.147	0.316 9	0.117 1
10	1.162	0.248 8	0.118 3	1.159	0.276 0	0.124 9	1.157	0.297 3	0.130 0	1.155	0.317 6	0.135 1
8	1.165	0.254 2	0.138 0	1.162	0.279 8	0.145 1	1.161	0.299 6	0.150 4	1.159	0.318 4	0.155 5
6	1.169	0.261 6	0.164 4	1.166	0.284 7	0.170 9	1.165	0.301 9	0.176 1	1.163	0.318 9	0.181 3
4	1.172	0.271 3	0.197 1	1.170	0.290 4	0.202 0	1.169	0.304 5	0.206 4	1.168	0.318 9	0.212 0
3	1.174	0.277 0	0.215 3	1.172	0.293 6	0.219 3	1.171	0.305 9	0.223 1	1.170	0.318 7	0.228 2
2	1.175	0.285 0	0.240 3	1.174	0.298 1	0.243 4	1.173	0.307 7	0.246 2	1.173	0.318 0	0.250 3
1	1.177	0.296 7	0.276 3	1.177	0.304 4	0.278 0	1.176	0.310 0	0.279 6	1.176	0.316 3	0.282 0

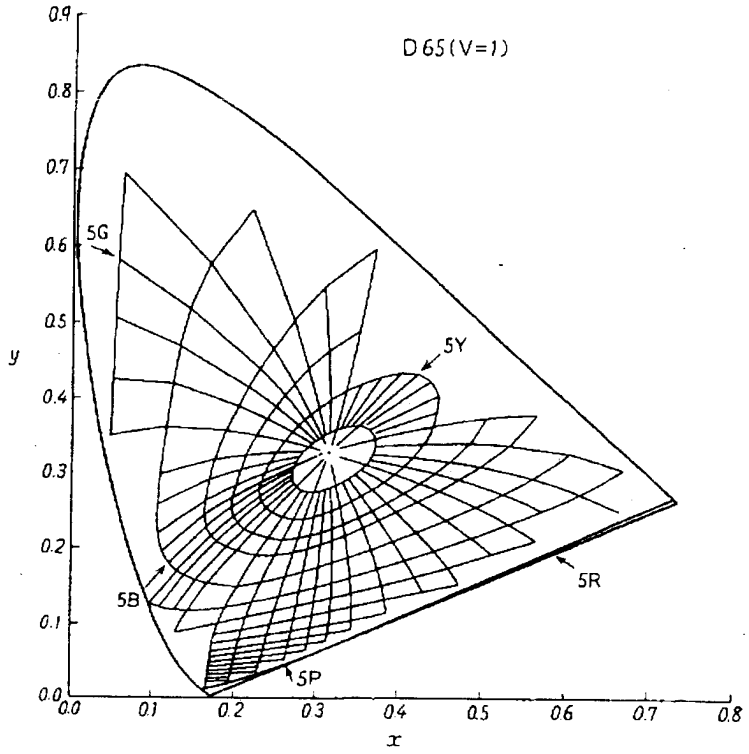
Annex Attached Table 1. (continued)

	2.5RP			5RP			7.5RP			10RP		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
9/ 6	75.87	0.336 6	0.301 3	75.90	0.347 6	0.309 1	75.86	0.355 8	0.315 4	75.94	0.363 4	0.322 1
4	76.47	0.326 8	0.313 0	76.45	0.333 5	0.317 9	76.45	0.338 4	0.321 7	76.43	0.343 4	0.325 6
3	76.61	0.322 0	0.318 7	76.59	0.326 4	0.321 9	76.58	0.329 6	0.324 5	76.56	0.332 8	0.327 0
2	76.65	0.317 9	0.323 5	76.63	0.320 1	0.325 3	76.62	0.322 0	0.326 7	76.60	0.323 5	0.328 0
1	76.68	0.314 6	0.327 2	76.66	0.315 4	0.327 8	76.65	0.316 0	0.328 3	76.64	0.316 4	0.328 8
8/14	56.21	0.368 6	0.256 8	—	—	—	—	—	—	—	—	—
12	56.50	0.361 1	0.267 6	56.32	0.388 2	0.281 6	56.23	0.406 9	0.293 2	—	—	—
10	56.83	0.353 1	0.279 2	56.80	0.373 8	0.291 8	56.66	0.388 5	0.301 3	56.57	0.403 9	0.312 8
8	57.13	0.345 1	0.289 8	57.10	0.361 5	0.300 1	57.10	0.372 7	0.308 2	57.11	0.384 3	0.317 9
6	57.44	0.336 5	0.301 6	57.43	0.347 7	0.309 3	57.41	0.355 8	0.315 5	57.39	0.363 5	0.322 2
4	57.51	0.327 3	0.312 3	57.50	0.334 1	0.317 3	57.48	0.339 3	0.321 1	57.47	0.344 5	0.325 2
3	57.55	0.322 6	0.317 7	57.53	0.327 2	0.321 2	57.52	0.330 7	0.323 7	57.51	0.334 2	0.326 5
2	57.58	0.318 4	0.322 7	57.56	0.321 0	0.324 6	57.55	0.323 0	0.326 1	57.54	0.324 8	0.327 6
1	57.60	0.315 0	0.326 7	57.59	0.316 0	0.327 4	57.58	0.316 8	0.328 0	57.57	0.317 4	0.328 5
7/20	41.03	0.389 1	0.221 5	—	—	—	—	—	—	—	—	—
18	41.17	0.382 5	0.231 6	41.06	0.427 1	0.253 5	—	—	—	—	—	—
16	41.30	0.375 6	0.242 4	41.20	0.414 8	0.261 5	41.13	0.442 7	0.276 6	41.06	0.473 2	0.295 1
14	41.43	0.368 1	0.253 7	41.40	0.402 1	0.271 1	41.32	0.426 0	0.284 0	41.24	0.452 2	0.300 2
12	41.56	0.361 0	0.264 2	41.54	0.389 6	0.280 2	41.53	0.409 4	0.292 2	41.51	0.431 0	0.306 2
10	41.70	0.353 5	0.275 4	41.70	0.376 0	0.290 0	41.69	0.391 6	0.300 4	41.68	0.408 2	0.312 3
8	41.79	0.346 0	0.285 7	41.77	0.364 6	0.297 7	41.76	0.376 3	0.306 8	41.75	0.389 0	0.316 8
6	41.85	0.337 7	0.297 1	41.83	0.350 8	0.306 3	41.82	0.360 0	0.313 3	41.81	0.368 4	0.320 6
4	41.90	0.328 9	0.309 3	41.89	0.336 6	0.315 1	41.88	0.342 3	0.319 7	41.87	0.347 9	0.324 1
3	41.93	0.324 4	0.314 9	41.92	0.329 9	0.319 2	41.91	0.334 0	0.322 4	41.89	0 338 1	0 325 6
2	41.95	0.320 1	0.320 2	41.94	0.323 7	0.322 9	41.93	0.326 3	0.324 9	41.92	0.328 8	0.327 1
1	41.97	0.316 2	0.325 0	41.96	0.317 9	0.326 2	41.95	0.319 2	0.327 1	41.94	0.320 4	0.328 3
6/24	28.79	0.401 9	0.196 7	—	—	—	—	—	—	—	—	—
22	28.81	0.396 1	0.205 2	28.81	0.454 5	0.229 6	—	—	—	—	—	—
20	28.84	0.391 3	0.213 2	28.84	0.445 3	0.235 6	28.84	0.482 6	0.254 0	—	—	—
18	28.90	0.384 7	0.224 0	28.89	0.431 9	0.245 8	28.88	0.465 3	0.261 9	28.88	0.503 7	0.282 0
16	28.94	0.378 6	0.233 8	28.93	0.420 4	0.254 8	28.92	0.451 2	0.269 7	28.91	0.483 9	0.287 8
14	29.00	0.371 3	0.244 8	28.98	0.408 3	0.263 9	28.97	0.434 2	0.278 6	28.96	0.460 3	0.295 5
12	29.06	0.363 7	0.256 1	29.04	0.395 4	0.274 0	29.03	0.417 7	0.287 2	29.01	0.440 7	0.301 8
10	29.11	0.355 9	0.268 3	29.09	0.381 8	0.283 8	29.08	0.400 7	0.295 5	29.06	0.419 4	0.307 8
8	29.15	0.348 2	0.279 8	29.13	0.369 3	0.292 5	29.12	0.383 4	0.303 1	29.11	0.397 1	0.313 5
6	29.18	0.340 3	0.291 4	29.17	0.356 1	0.301 5	29.16	0.367 5	0.309 5	29.15	0.377 8	0.317 9
4	29.23	0.330 8	0.304 9	29.22	0.340 7	0.311 9	29.21	0.347 4	0.317 1	29.20	0.354 3	0.322 5
3	29.24	0.326 4	0.311 1	29.24	0.333 4	0.316 5	29.23	0.338 1	0.320 5	29.22	0.343 0	0.324 4
2	29.26	0.322 0	0.317 3	29.26	0.326 4	0.320 8	29.25	0.329 2	0.323 5	29.24	0.332 3	0.326 2
1	29.28	0.317 5	0.323 3	29.27	0.319 6	0.325 0	29.27	0.320 9	0.326 5	29.26	0.322 3	0.327 8
5/26	19.01	0.411 8	0.172 9	—	—	—	—	—	—	—	—	—
24	19.00	0.406 2	0.181 0	19.04	0.480 4	0.206 2	—	—	—	—	—	—
22	18.98	0.401 5	0.188 6	19.02	0.467 8	0 213 9	19.04	0.514 1	0.231 8	—	—	—
20	18.96	0.395 5	0 198 2	18.99	0.457 1	0.221 8	19.02	0.499 9	0.239 3	19.04	0.547 9	0.259 8
18	18.97	0.389 6	0.208 4	18.95	0 444 9	0.231 0	18.94	0.483 3	0.248 2	18.97	0.525 2	0.267 3
16	19.00	0.383 3	0 219 0	18 98	0.433 2	0 240 5	18.97	0.468 4	0.257 3	18.96	0.504 5	0 275 2
14	19.04	0.376 8	0.229 8	19.02	0.420 8	0.250 8	19.01	0.451 6	0.267 0	19.00	0.482 2	0 284 2
12	19.08	0.369 5	0.241 8	19.06	0.408 2	0.260 9	19.05	0 436 0	0 275 5	19.04	0 463 1	0 291 4
10	19.11	0.361 5	0.255 2	19.10	0.393 5	0.272 3	19.09	0.416 0	0.286 1	19.08	0.438 0	0 300 0
8	19.14	0.354 0	0.267 5	19.13	0.379 7	0.282 9	19.12	0.397 9	0.294 7	19 12	0.414 9	0 307 0
6	19 16	0 344 0	0 283 0	19 17	0 362 8	0 294 9	19.16	0.376 8	0.304 5	19.15	0.389 1	0 313 9
4	19.21	0.333 6	0.298 7	19.20	0.345 9	0.306 9	19.20	0.355 2	0.313 6	19.19	0.363 0	0 319 9
3	19 23	0.328 4	0.306 5	19 22	0.337 3	0.312 8	19.21	0 344 0	0.317 8	19.21	0.349 5	0 322 6
2	19.24	0.323 2	0.314 2	19.23	0.328 8	0.318 7	19.23	0.332 8	0.321 9	19.22	0.336 4	0.325 0
1	19.25	0.318 0	0.321 8	19.25	0.320 7	0.324 1	19.24	0.322 4	0 325 6	19 24	0.324 0	0.327 2

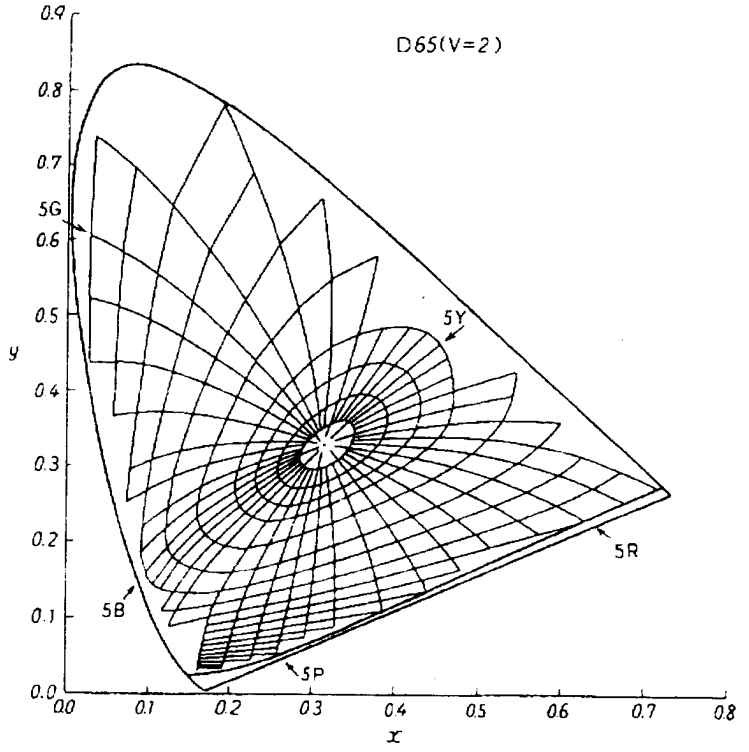
Annex Attached Table 1. (continued)

	2.5RP			5RP			7.5RP			10RP		
	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D	Y_D	x_D	y_D
4/26	11.42	0.418 1	0.150 8	—	—	—	—	—	—	—	—	—
24	11.46	0.412 0	0.157 4	—	—	—	—	—	—	—	—	—
22	11.49	0.406 8	0.166 3	11.46	0.477 3	0.189 5	—	—	—	—	—	—
20	11.51	0.402 2	0.174 9	11.51	0.467 3	0.197 5	11.49	0.523 1	0.216 7	11.47	0.576 9	0.238 0
18	11.51	0.395 2	0.187 4	11.53	0.454 8	0.209 1	11.53	0.505 4	0.228 0	11.54	0.554 3	0.247 8
16	11.51	0.388 5	0.199 6	11.51	0.442 2	0.220 7	11.53	0.488 0	0.239 1	11.54	0.530 5	0.258 4
14	11.53	0.382 0	0.211 8	11.52	0.429 9	0.232 1	11.51	0.469 9	0.250 1	11.50	0.508 3	0.267 8
12	11.56	0.374 9	0.224 8	11.54	0.417 1	0.244 0	11.54	0.451 4	0.261 3	11.53	0.484 7	0.278 1
10	11.58	0.366 8	0.239 4	11.57	0.402 1	0.257 6	11.56	0.431 7	0.273 2	11.56	0.458 1	0.288 4
8	11.60	0.358 8	0.253 7	11.60	0.388 8	0.269 4	11.59	0.412 4	0.283 8	11.58	0.433 1	0.297 3
6	11.63	0.349 0	0.270 2	11.62	0.371 9	0.283 5	11.62	0.389 6	0.295 7	11.61	0.404 3	0.306 5
4	11.65	0.338 2	0.288 4	11.65	0.353 2	0.298 2	11.64	0.365 2	0.307 0	11.64	0.375 4	0.314 6
3	11.66	0.332 5	0.297 5	11.66	0.344 0	0.305 4	11.65	0.353 2	0.312 4	11.65	0.360 5	0.318 4
2	11.67	0.326 6	0.307 2	11.67	0.334 5	0.312 9	11.67	0.340 6	0.317 8	11.66	0.345 1	0.322 1
1	11.69	0.320 2	0.317 6	11.68	0.324 3	0.320 7	11.68	0.327 3	0.323 3	11.67	0.329 4	0.325 6
3/22	6.081	0.411 1	0.135 4	—	—	—	—	—	—	—	—	—
20	6.151	0.405 0	0.146 4	6.101	0.467 9	0.164 9	—	—	—	—	—	—
18	6.205	0.401 2	0.156 3	6.175	0.459 3	0.175 1	6.114	0.522 4	0.194 6	—	—	—
16	6.253	0.396 1	0.169 3	6.240	0.450 8	0.187 0	6.208	0.507 4	0.206 5	6.165	0.569 8	0.228 5
14	6.279	0.390 1	0.182 7	6.278	0.440 1	0.201 1	6.267	0.491 4	0.219 9	6.256	0.545 0	0.241 8
12	6.286	0.383 1	0.197 1	6.286	0.427 9	0.215 8	6.287	0.473 3	0.233 6	6.287	0.520 9	0.254 2
10	6.302	0.375 1	0.213 5	6.297	0.414 5	0.231 1	6.293	0.451 4	0.248 8	6.286	0.491 4	0.267 7
8	6.321	0.366 0	0.232 3	6.316	0.399 3	0.248 0	6.311	0.429 6	0.263 4	6.306	0.460 9	0.281 1
6	6.339	0.355 5	0.252 4	6.334	0.382 0	0 266 3	6.330	0.404 3	0.279 7	6.326	0.426 8	0.294 7
4	6.354	0.344 7	0.273 1	6.351	0.363 3	0.284 5	6.347	0.378 5	0.295 0	6.344	0.393 3	0.306 4
3	6.362	0.338 3	0.284 8	6.359	0.352 7	0.294 6	6.356	0.364 3	0.303 0	6.352	0.375 5	0.312 1
2	6.371	0.331 0	0.297 7	6.368	0 340 8	0.305 4	6.365	0.348 8	0.311 2	6.361	0.356 3	0.317 7
1	6.379	0.322 6	0.312 3	6.376	0.327 6	0.316 7	6.374	0.331 8	0.319 8	6.371	0.335 7	0.323 2
2/20	2.851	0.383 9	0.109 8	—	—	—	—	—	—	—	—	—
18	2.879	0.385 3	0.123 1	2.853	0.437 7	0.135 9	—	—	—	—	—	—
16	2.921	0.382 1	0.135 9	2.888	0.434 7	0.150 0	2.863	0.482 9	0.163 9	—	—	—
14	2.965	0.379 2	0.151 0	2.941	0.425 9	0.165 3	2.918	0.469 8	0.178 5	2.894	0.519 9	0.193 0
12	2.989	0.375 0	0.168 7	2.983	0.416 4	0.183 0	2.972	0.456 2	0.196 3	2.959	0.498 5	0.211 3
10	2.998	0.369 3	0.187 4	2.997	0.405 1	0.201 0	2.995	0.440 1	0.214 9	2.992	0.475 4	0.229 8
8	3.006	0.362 3	0.208 4	3.004	0.392 9	0.221 7	3.002	0.420 8	0.234 8	3.000	0.449 7	0.248 5
6	3.018	0.352 9	0.235 1	3.016	0.376 8	0.246 8	3.013	0.397 8	0.257 4	3.011	0.419 8	0.268 7
4	3.027	0.343 2	0.259 8	3.024	0.360 9	0.269 5	3.022	0.375 3	0.277 8	3.020	0.390 1	0.286 8
3	3.031	0.338 2	0.272 0	3.028	0.352 6	0.280 9	3.026	0.363 6	0.288 3	3.024	0.374 7	0.296 2
2	3.035	0.332 1	0.286 4	3.033	0.342 5	0 293 7	3.031	0.350 1	0.299 8	3.029	0.357 4	0.306 0
1	3.040	0.323 9	0.304 8	3.038	0.329 8	0.309 2	3.036	0.333 7	0.312 9	3 034	0.337 3	0.316 7
1/16	1.093	0.342 1	0.092 9	—	—	—	—	—	—	—	—	—
14	1.117	0.343 5	0.106 2	1.097	0.387 2	0.117 1	—	—	—	—	—	—
12	1.140	0.343 9	0.124 0	1.125	0.384 7	0.133 3	—	—	—	—	—	—
10	1.152	0.343 4	0.142 0	1 146	0.381 1	0.152 4	1.109	0.431 2	0.144 2	1 093	0.472 6	0.154 4
8	1.159	0.341 8	0.162 6	1.157	0.374 1	0.173 5	1.137	0.421 4	0.164 0	1.129	0.459 8	0.176 3
6	1.162	0.338 9	0.188 6	1.161	0.366 1	0.199 4	1.154	0.408 8	0.186 3	1.150	0.443 9	0.198 7
4	1.167	0.335 0	0.218 0	1.165	0.356 7	0 227 8	1.160	0.394 1	0.210 7	1.158	0.422 7	0.223 7
3	1.169	0.332 8	0.234 1	1.167	0.351 2	0.243 4	1.164	0.377 1	0.237 7	1.162	0.398 7	0.249 5
2	1.171	0.329 0	0.255 5	1.170	0.343 0	0.263 4	1.166	0.367 6	0.252 4	1.164	0.385 4	0.263 2
1	1 174	0.322 9	0.285 4	1.172	0.331 0	0.290 4	1.168	0.355 2	0 270 6	1 166	0.368 4	0.279 5
							1.171	0.337 8	0 294 7	1.169	0.345 3	0.300 0

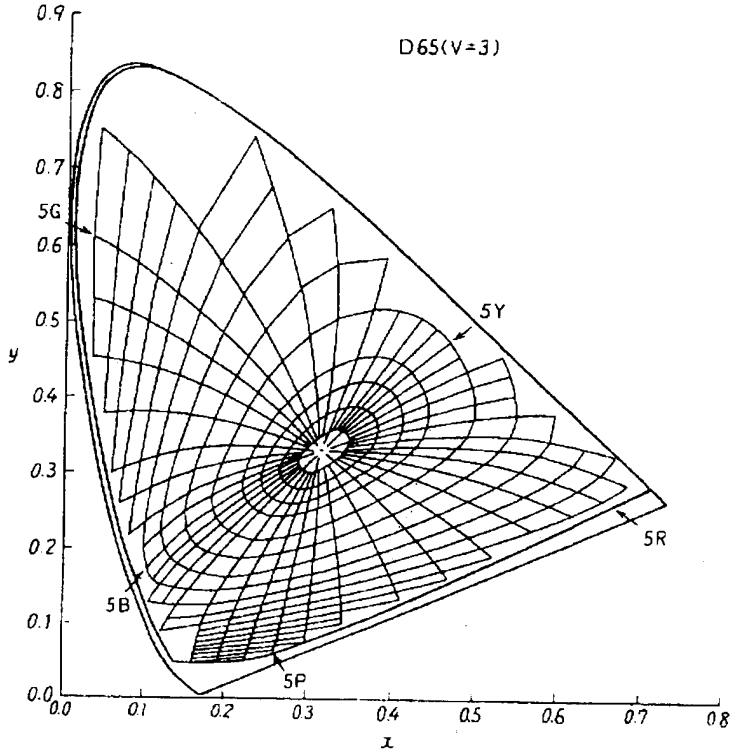
Annex Attached Fig. 1



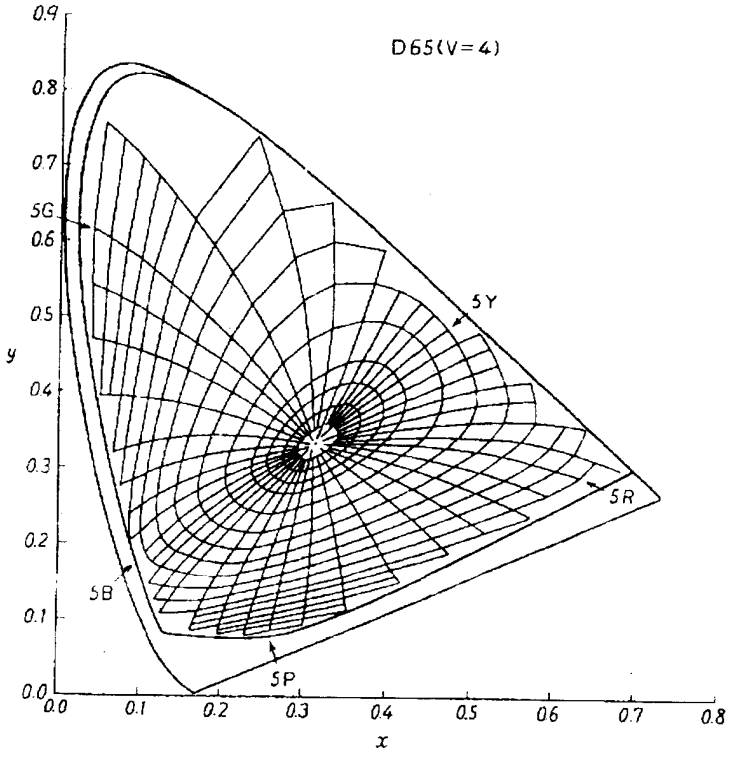
Annex Attached Fig. 2



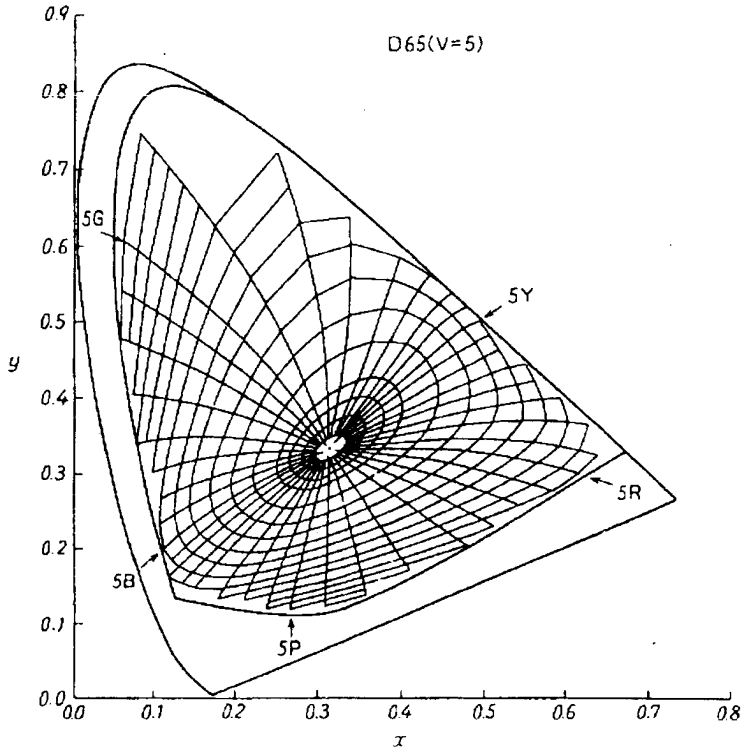
Annex Attached Fig. 3



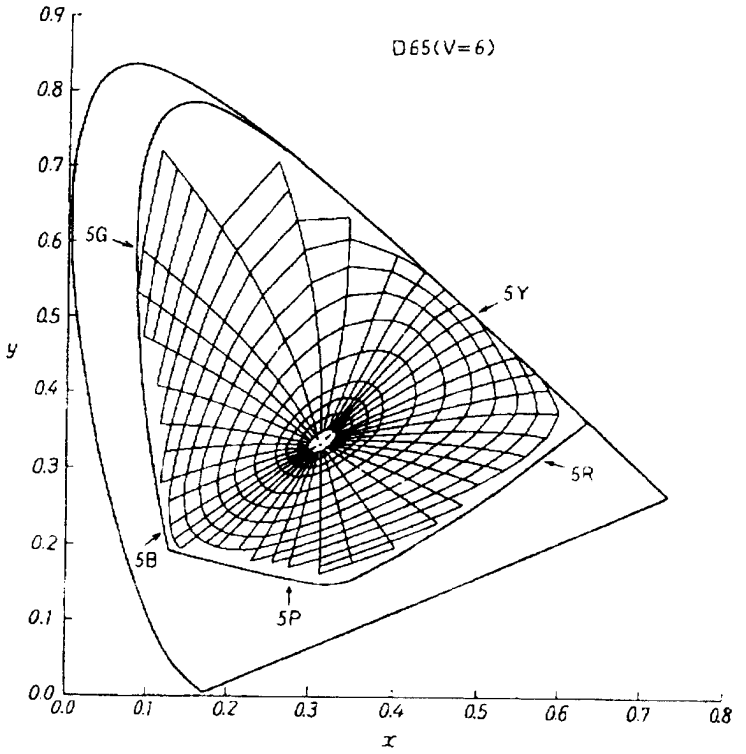
Annex Attached Fig. 4



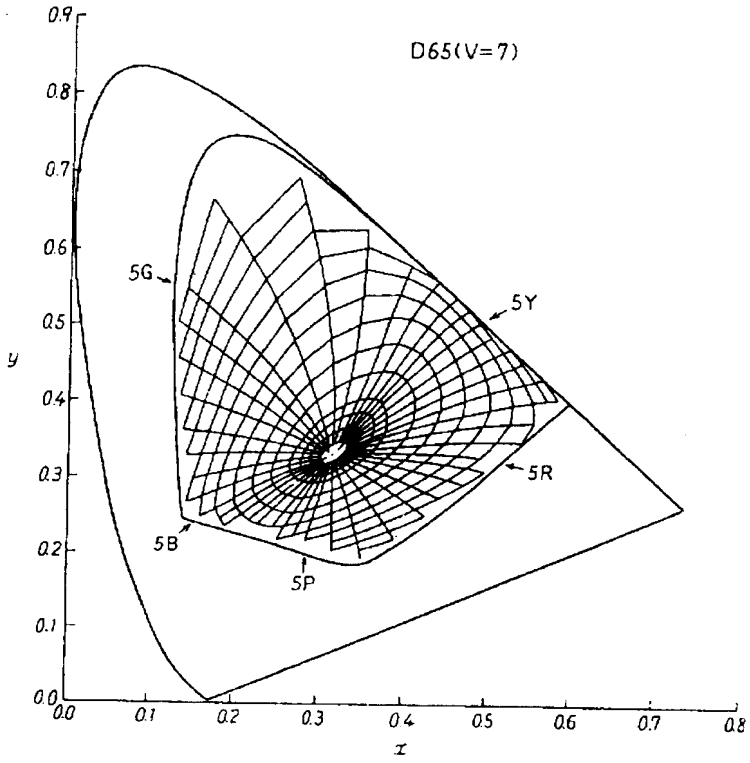
Annex Attached Fig. 5



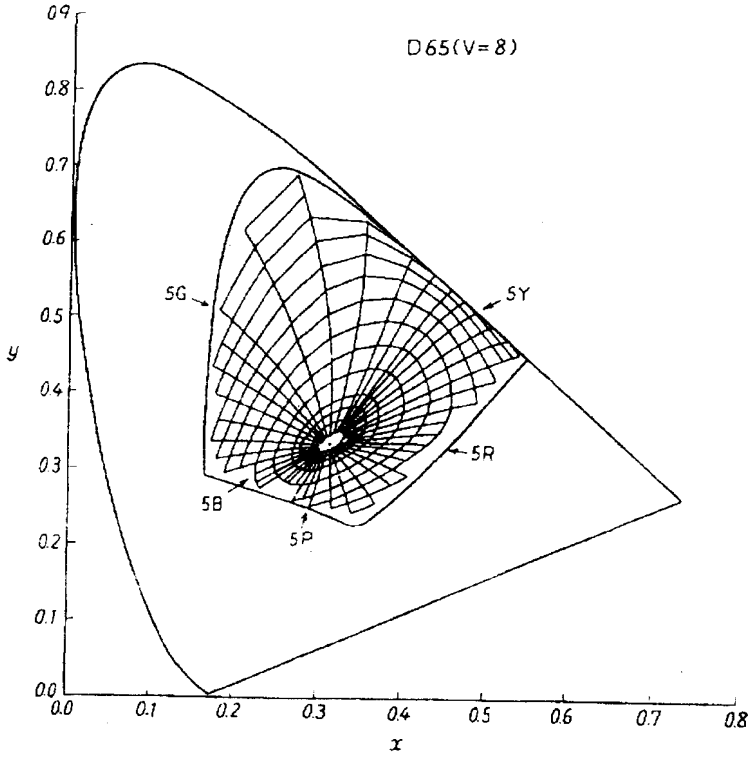
Annex Attached Fig. 6



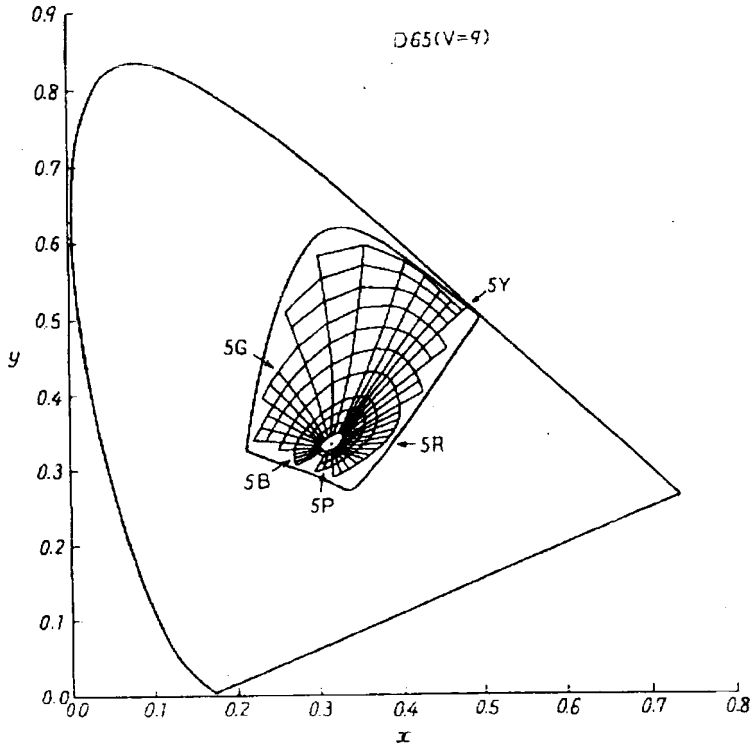
Annex Attached Fig. 7



Annex Attached Fig. 8



Annex Attached Fig. 9



Informative reference 1. Determination of notation for colour specification under standard illuminant C

Preface This Informative reference is to describe examples of methods to obtain the notation for colour specification H_C, V_C and C_C (hereafter the suffixes are omitted) from the luminance factor Y_C and chromaticity coordinates x_C, y_C (hereafter the suffixes are omitted) by using the Attached Table 1 and Attached Table 2 of this Standard and does not form a part of the standard.

The examples shown below are described about the search of the chromaticity coordinates in Attached Table 1 composing a quadrangle which surrounds the chromaticity coordinates x, y of the sample colour and about the subroutine subprogram in accordance with JIS X 3003 to obtain the hue H and chroma C of the sample colour from the values of its coordinates by the linear interporation. The notation for colour specification can be determined by citing this subroutine by means of GOSUB sentence after calculating the chromaticity coordinates and the value V by the main program or another subprogram.

Besides, the value V of the sample colour to be used shall be the value obtained by calculating directly by using the formula in the remarks of Attached Table 1 from luminance factor Y of the sample colour.

1. Method for searching chromaticity coordinates forming a quadrangle which surrounds chromaticity coordinates x, y of sample colour As the methods for searching chromaticity coordinates forming a quadrangle which surrounds chromaticity coordinates x, y (hereafter referred to as chromaticity coordinates. See Informative reference 1 Fig. 1), the method by vector product, the method by interior division ratio, the method by polar coordinates, etc. are known. An example of searching by the use of vector is shown here.

The chromaticity coordinates exist on two integer value planes adjacent to the value V of sample colour (in accordance with Attached Table 1), so that the search of chromaticity coordinates is necessary to be carried out respectively on both planes of high value side and low value side adjacent to each other.

2. Method for obtaining hue H and chroma C of sample colour The hue H and the chroma C of sample colour can be determined by an interpolation method from the searched chromaticity coordinates. As for the interpolation method, some methods are proposed according to the degree of the interpolation or the interpolation space. An example of utilizing the linear interporation based on the interior division ratio m and n in x y plane is shown here.

The hue H and the chroma C of the sample colour are determined from the value V of the sample colour by interpolating, by the following formula, H and C obtained by the interpolation from the chromativity coordinates of the value plane adjacent to the value V of the sample colour:

$$H = H_i + k(H_h - H_i) \quad \cdots\cdots (1)$$

$$C = C_i + k(C_h - C_i) \quad \cdots\cdots (2)$$

$$k = (V - V_i)/(V_h - V_i) \quad \cdots\cdots (3)$$

where, H : hue of the sample colour

C : chroma of the sample colour

V : value of the sample colour

H_h, C_h : hue and chroma obtained by interpolation from chromaticity coordinates of the integer value plane on high value side adjacent to value of the sample colour.

H_l, C_l : hue and chroma obtained by interpolation from chromaticity coordinates of value plane on low value side adjacent to value of the sample colour

3. Subroutine subprogram The numerical values in Attached Table 1 are read in the main program in compliance with the value V of the sample colour by an appropriate method and transferred to this subroutine.

In this subroutine, the relation between the name of variable that appears as dummy argument and the symbols in Informative reference 1 Attached Fig. 1 is as follows:

SX, SY : chromaticity coordinates of sample colour P

$X1$, X2, $X3$, $X4$: values of x in chromaticity coordinates x, y of points A, B, C, D

$Y1$, $Y2$, $Y3$, $Y4$: values of y in chromaticity coordinates x, y of points A, B, C, D

$H1$, $H2$: straight line AB and straight line CD indicating constant hue line

when giving hue number so as to be in sequence from 10RP = 0 to 7.5RP = 39, $H1 < H2$

$C1$, $C2$: straight line AC and straight line BD indicating constant chroma line

chroma of $C1$ and $C2$, $C1 < C2$

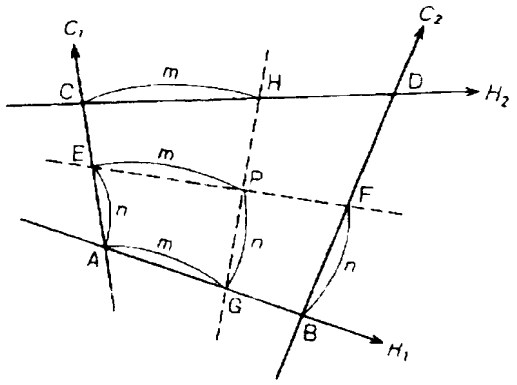
M : interior division ratio used for interpolation of chroma

N : interior division ratio used for interpolation of hue

```
10000 REM *** search ***
10010 REM *** zero correction ***
10020 DEF FNZC(XX)=XX-(XX=0)*1E-10
10030 REM *** comparison of P (SX, SY) with C2 ***
10040 LET XD=X2-X4
10050 LET XD=FNZC(XD)
10060 LET A1=(Y2-Y4)/XD
10070 LET B1=(X2*Y4-X4*Y2)/XD
10080 LET YD=SY-(A1*SY+B1)
10090 IF XD*YD>0 THEN 10110
10100 IF XD*YD<=0 THEN 10130
10110 LET F1=0
10120 GOTO 10140
10130 LET F1=1
10140 REM *** comparison of P(SX, SY) with H2 ***
10150 LET XD=X3-X4
10160 LET XD=FNZC(XD)
10170 LET A3=(Y3-Y4)/XD
10180 LET B3=(X3*Y4-X4*Y3)/XD
10190 LET YD=SY-(A3*SX+B3)
10200 IF XD*YD<0 THEN 10220
10210 IF XD*YD>=0 THEN 10240
10220 LET F2=0
10230 GOTO 10250
10240 LET F2=1
10250 REM *** decision ***
10260 IF F1=1 AND F2=1 THEN 10280
10270 IF F1<>1 OR F2<>1 THEN 10300
10280 PRINT "CONTAINED"
10290 GOTO 10310
10300 PRINT "NOT CONTAINED"
10310 RETURN
20000 REM *** calculation of interior division ratio m, n ***
```

```
20010 REM * * * calculation of interior division ratio m * * *
20020 LET E1=X1-SX
20030 LET E2=X2-X1
20040 LET E3=X3-X1
20050 LET E4=X4-X3-X2+X1
20060 LET E5=Y1-SY
20070 LET E6=Y2-Y1
20080 LET E7=Y3-Y1
20090 LET E8=Y4-Y3-Y2+Y1
20100 LET BB1=E2*E8-E4*E6
20110 LET BB1=FNZC(BB1)
20120 LET BB2=E1*E8+E2*E7-E3*E6-E4*E5
20130 LET BB3=E1*E7-E3*E5
20140 LET D=BB2*BB2-4*BB1*BB3
20150 LET M=INT((-BB2+D^0.5)/2/BB1*10000+0.5)/10000
20160 REM * * * calculation of interior division ratio n * * *
20170 LET BB1=E3+M*E4
20180 LET BB1=FNZC(BB1)
20190 LET N=INT(-(E1+M*E2)/BB1*10000+0.5)/10000
20200 REM * * * interpolation of hue * * *
20210 LET HH=H1+1.0*N
20220 REM * * * interpolation of chroma * * *
20230 LET CC=C1+2.0*M
20240 RETURN
```

Informative reference 1 Fig. 1.
Relation between locations of chromaticity coordinates



Informative reference 2.
Determination of notation for colour specification under standard illuminant D_{65}

Preface This Informative reference is to describe the examples of methods to obtain the notation for colour specification H_D, V_D and C_D from the luminance factor Y_D and chromaticity coordinates x_D, y_D by using Annex Attached Table 1 of this Standard and does not form a part of the standard.

In the bases of the colour system under the standard illuminant D_{65}, the luminance factor Y_D may differ when the hue H_D or the chroma V_D differs, even if the value C_D is the same. There are both cases where the variation of luminance factor Y_D maybe ignored and shall be taken into account and in the latter case, the interpolation method cannot be applied as it is under the illuminant C.

An example of determination of the symbol for colour specification taking into account the variation of luminance factor Y_D on the constant value plane is shown below:

1. Method for obtaining hue H_D and chroma C_D of sample colour The method for obtaining hue H_D and chroma C_D is composed of search and interpolation as under the illuminant C. In the search, the variation of luminance factor Y_D is ignored and the judgment is given to the chromaticity coordinates x_D, y_D by the method shown in Informative reference 1.

Besides, the interpolation for hue H_D and chroma C_D is carried out in the same way.

2. Method for obtaining value V_D of sample colour As for the lightness function for obtaining the value V_D from the luminance factor Y_D, the CIE 1976 lightness function is applied by defining its parameters divisionally in compliance with each part of lightness as shown below.

$$V_D = a\left(\frac{Y_D}{Y_n}\right)^{\frac{1}{3}} - b \quad \cdots\cdots\cdots\cdots\cdots\cdots\cdots\cdots\cdots\cdots \quad (1)$$

where, $a = \dfrac{(V_h - V_l)}{(A_h - A_l)}$

$$b = \frac{(V_h A_l - V_l A_h)}{(A_h - A_l)}$$

$$A_l = \left(\frac{Y_l}{Y_n}\right)^{\frac{1}{3}}$$

$$A_h = \left(\frac{Y_h}{Y_n}\right)^{\frac{1}{3}}$$

In the case $\frac{Y_D}{Y_n}$ is not more than 0.008856, the formula (2) is used instead of the formula(1).

$$V_D = a\left(\frac{Y}{Y_n}\right) - b \qquad \cdots\cdots (2)$$

where,

$$a = \frac{(V_h - V_l)}{(A_h - A_l)}$$

$$b = \frac{(V_h A_l - V_l A_h)}{(A_h - A_l)}$$

$$A_l = \frac{Y_l}{Y_n}$$

$$A_h = \frac{Y_h}{Y_n}$$

In this case, Y_n is the luminance factor Y_D of the perfect refrecting diffuser.

Here, V_l, V_h and Y_l, Y_h are the values, of two values V_D on the lower and higher levels between which the sample colour is put, and of luminance factor Y_D corresponding to them.

V_l and V_h are obtained by the following formula (3).

$$V_l = \mathrm{INT}\,(V') \qquad \cdots\cdots (3)$$

$$V_h = V_l + 1$$

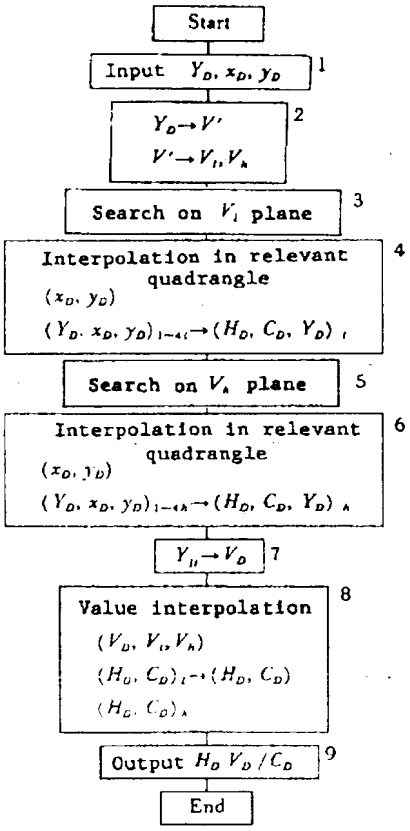
where,

$$V' = 11.6\left(\frac{Y_D}{Y_n}\right)^{\frac{1}{3}} - 1.6$$

In this case, INT (V') gives only integer part of V'.

3. Example of program A flow chart for obtaining the symbol specification is shown in Informative reference 2 Fig. 1.

Informative reference 2 Fig. 1.
A flow chart for obtaining the symbol specification



When luminance factor Y_D and chromaticity coordinates x_D and y_D of the sample colour are given (step 1) after the basis value data of colour system are read in, the two values of V_i and V_k between which the sample colour is put, (step 2) shall be at first determined by using the formula (3). Then, search on the value V_i plane (step 3) and do the interpolation in the relevant quadrangle (step 4).

It shall be noted that not only the interpolated values H_i and C_i of the hue and chroma corresponding to the sample colour on the value V_i plane are obtained but also the interporated value of Y_i of luminance factor is obtained by using the same interpolation ratio.

Repeat the above steps as well with respect to the value V_k plane (steps 5 and 6).

Substitute V_i, V_k and Y_i, Y_k thus obtained for the relevant values in the formula (1) or (2) to determine the lightness function and convert Y_D of luminance factor of sample colour to the value V_D (step 7). Carry out the value interpolation for the hue H_i and H_k and the chroma C_i and C_k on the value V_i and V_k planes, by using the value of this value V_D [formulas (1), (2) and (3) in Informative reference 1] and obtain the final hue H_D and chroma C_D (step 8).

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